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METHODS OF MEASURING TEMPERATURE.

BY

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PRINCIPAL ASSISTANT IN THE PHYSICS DEPT. OF THE NATIONAL PHYSICAL LABORATORY

WITH AN INTRODUCTION

BY

PRINCIPAL E. H. GRIFFITHS, F.R.S.

SECOND EDITION, REVISED.

With Illustrations.



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PREFACE TO SECOND EDITION.

THE first edition of this book was exhausted very quickly and for four years it has been unprocurable, as the author was too occupied to make the necessary revision. For this second edition, in addition to the correction of certain errata, the changes are mainly in connection with the treatment of Optical Pyrometry. The patience of the publishers in respect to delay on the Author's part is gratefully acknowledged.

E. G.

October, 1925.

PREFACE.

THE present volume is written for those concerned with the measurement of temperature, whether in scientific investigations or in the control of industrial operations.

Attention has been devoted chiefly to the experimental basis of the methods in general use, the calibration of the instruments, and the precautions which must be observed in practice.

While the volume is complete in itself, it is assumed that the reader is conversant with the fundamental principles of physics, and the aim has been to extend the general treatment given in standard text-books, such as those of Poynting and Thomson.

It was not deemed desirable to devote much space to descriptions of the constructional details of pyrometers, since the information is readily accessible in the catalogues of the manufacturers.

A connected account is given of the classical researches with the gas thermometer, which have established, in a concrete form, the absolute scale of temperature over the range 200° to 1,550° C. And it is well to remember that although the electrical and radiation methods enable "relative" measurements to be made with a high degree of precision, they are dependent on the gas thermometer work for their evaluation in terms of the fundamental scale of temperature.

In subsequent chapters the various types of pyrometers are dealt with individually, the theory underlying the method and the calibration of the instrument.

An attempt has been made to set out clearly the errors to which pyrometric observations are liable, when the conditions of use do not comply with those postulated by the theory upon which the design is based; particularly in the case of instruments of the "radiation" type.

The illustrations have been prepared by Mr. Edgar A. Griffiths, and the writer wishes to acknowledge his indebtedness to his brother for his contributions to the work.

The descriptions of the apparatus in use at the National Physical Laboratory have been inserted with the kind permission of the Director, Sir Richard Glazebrook.

E. G

TEDDINGTON, MIDDLESEX,
December, 1917.

INTRODUCTION.

THE need of a monograph on the measurement of temperature must, I think, have been evident to every physicist, and it was a great pleasure to me to know that the difficult task of supplying this need was to be discharged by one so capable as Dr. Ezer Griffiths.

A perusal of Dr. Griffiths's book has made me realise how rapid our progress has been in recent times in this essential and hitherto somewhat neglected branch of physical measurement. Accurate measurement of temperature is the basis of nearly all accurate measurements in physics, and it is sad to reflect on the amount of valuable work which has had to be "scrapped" owing to lack of attention to this important matter. That unreliable instrument the mercury thermometer has in the past been used with little knowledge of its imperfections. We can best judge of the advances that have been made by recalling the conditions under which an observer had to work some thirty years ago. About 1888 I had the privilege of being called into consultation by Messrs. Heycock and Neville, who were engaged in an enquiry into the freezing-point of various metals as a basis for their investigations into the nature of certain alloys. We made a careful study of what we then regarded as the standard determinations of temperatures above the boiling-point of water. The discrepancies between the various observers were most startling. For example, the freezing-point of zinc ranged from 342° to 450°, that of antimony varied by 100°; and at higher temperatures the data were unreliable. We ultimately decided for the purposes of standardisation to accept the following as authentic:

The boiling-point of aniline	[at 760 mm.]	184·41°	by Ramsay.
,, ,, naphthalene	,,	218·06°	by Crafts.
,, ,, benzophenone	,,	306·08°	by Crafts.
,, ,, mercury	,,	358·2°	by Ramsay.
,, ,, sulphur	,,	448·38°	by Regnault.

As is shown by Table VII., *infra*, we were fortunate in our selection, for, with the exception of sulphur, later determinations have led to but small modifications of the above numbers.

In 1891 I published* the results of the standardisation of platinum thermometers based on the above data. At the time when the observations were taken I was unacquainted with the admirable investigation by Professor Callendar † into the relation between platinum and the air scales of

* *Phil. Trans. R.S.*, vol. 182. † *Phil. Trans.*, A. 1887.

temperature. In the autumn of 1889 I for the first time became acquainted with this work. I then found that the upper portion of the curves obtained by me departed materially from the parabolic formula given by Callendar, although up to a temperature of something like 350° we were in fair agreement. Consultation with Callendar led to the conclusion that either his formula did not hold with platinum thermometers constructed like mine, or that the value given by Regnault for the boiling-point of sulphur was too high. We, in consequence, joined forces and conducted under stringent conditions an enquiry into the true boiling-point of sulphur, the result being stated as follows: "the temperature by the normal air thermometer, at constant pressure, of the saturated vapour of sulphur boiling under standard pressure is 444·5°." Not only was the accuracy of Professor Callendar's conclusions thus established, but the results of both his and my own determinations were brought into close agreement. As shown by Table II. in Dr. Griffiths's work, various observers, both here and in the United States, have since redetermined the boiling-point of sulphur under varied conditions, and their investigations have but the more firmly established the conclusions we arrived at. Many of the discrepancies between previous observers at higher temperatures are thus explained, for they were obtained by extrapolation from the value of sulphur obtained by Regnault, and as this was about 4° too high, and as this error became rapidly magnified by extrapolation, it was evident that little value could be attached to the then accepted numbers at temperatures exceeding 500°.

Messrs. Heycock and Neville determined the freezing-point of such substances as gold, copper, silver, by means of thermometers standardised by the assumption of the parabolic formula and the above-determined boiling-point of sulphur; and when it is remembered that this meant the extrapolation over something like 600°, the agreement of their results (see Tables VII. and X., *infra*) with those obtained by subsequent observers is a convincing proof of the validity both of the parabolic formula up to a temperature of about 1,100° C. and of the sulphur boiling-point. I venture to say that the recent increase in the accuracy of measurement of high temperatures is in no small degree due to the investigations of Callendar and the confirmation of his conclusions, during the period 1887-1893, by the observers above referred to.

The chapters on the Thermocouple and Radiation pyrometers indicate how rapid has been the subsequent advance and also its importance for the purposes of industry.

If we consider the melting-point of palladium (1,549° C.) as satisfactorily determined, we may regard our methods of observation and our knowledge of the temperature scale about 1,600° C. as comparable both in facility and accuracy with our measurements some thirty years ago in the neighbourhood of 600° C.

E. H. GRIFFITHS.

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METHODS OF MEASURING TEMPERATURE.

CHAPTER I.

THE FUNDAMENTAL SCALE OF TEMPERATURE.

The Scale of Temperature.—In the early development of the science of temperature measurement the mercury in glass thermometer held undisputed sway as the fundamental standard; in time it was realised that a temperature scale based on the expansion of mercury relative to glass had serious limitations. The composition of the glass had a considerable influence on the resulting scale, and, moreover, the range of such instruments was extremely limited. These considerations led experimentalists like Regnault to prefer the scale of the gas thermometer as the standard of reference, with the mercury thermometer as a working standard, calibrated by reference to the gas scale.

Later the thermodynamical researches of Lord Kelvin showed that it was possible to formulate a scale of temperature which would be independent of the intrinsic properties of any particular substance and that it would be identical with the scale given by a "perfect gas."

A "perfect gas" may be described as one which obeys Boyle's and Gay Lussac's laws, and one in which a free expansion, with no external work, would cause no change in temperature.

Although none of the known gases are perfect in the sense contemplated by the above definition, the departure of such gases as hydrogen, helium, argon, oxygen, and nitrogen, under the conditions obtaining in gas thermometry, is small and, moreover, is amenable to calculation.

In passing, it may be remarked that the computed value of the correction increases with the temperature, and is of the order of about 1° at 1,100° C. for air and nitrogen.

The gas thermometer is never used directly in practical work for the measurement of temperatures, owing to the complications that would be involved. Consequently to realise the gas scale for practical work it is necessary to transfer the scale to auxiliary standards.

Such secondary standards may be mercury thermometers, thermocouples, or the melting points or boiling points of pure substances.

The Scale from 0° to 100° C.—In 1884 Chappuis, at the Bureau International des Poids et Mesures, commenced an experimental investigation of the divergence of the scale of some "Verre Dur" mercury thermometers from that of the constant-volume hydrogen gas thermometer.

A careful comparative study was made of eight mercury thermometers by methods which are described in Chapter II., and the various corrections ascertained.

The accuracy of work was such that when the thermometers were directly

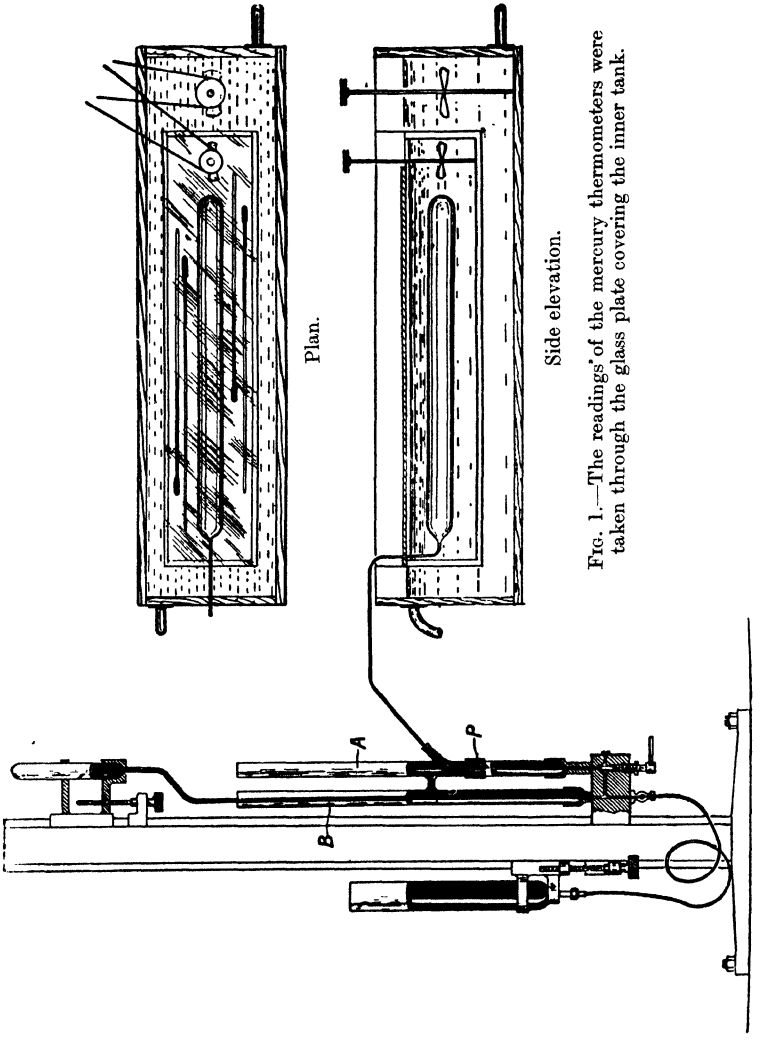


FIG. 1.—The readings of the mercury thermometers were taken through the glass plate covering the inner tank.

compared in the same bath their observations agreed to 0·002° after the application of the corrections.

The next step was the determination of the divergence of this "Verre Dur" mercury thermometer scale from that of the gas thermometer.

The general features of the apparatus are shown in Fig. 1.

The bulb of the gas thermometer was of platinum-iridium alloy, 110 cms. long by 3·6 cms. in diameter, the bulb being connected to the manometer by a platinum capillary 1 metre in length and 0·7 mm. in diameter. The end of the capillary was soldered to the plug (P), which was connected to the closed end of the manometer.

The barometer was inserted into the open limb and permitted the total pressure on the gas to be obtained from a single reading. The mercury in the tube A was in communication with that in B by way of the cross-tube. The function of the tube A was to enable the barometric height to be determined from observations of the difference in level in the same vertical line: the barometric height being required when standardising the instrument in steam.

The ice-point was obtained by surrounding the bulb with powdered ice, while the steam-point was determined with a horizontal type of hypsometer.

The apparatus employed in the comparison with the mercury thermometers is shown on the right in the diagram: the thermometers being laid alongside the gas thermometer bulb in a well-stirred water bath.

The coefficient of cubical expansion of the bulb was calculated from the value of the linear expansion, this being directly determined by measuring the length of the bulb at four temperatures.

Experiments were also made with the gases nitrogen and carbon dioxide, the initial pressure in each case being 1,000 mms. of mercury.

Taking the hydrogen scale as standard of comparison, the divergences of the various scales from it are shown in Table I.

TABLE I.

t_H °C.	$t_N - t_H$ °C.	$t_{CO_2} - t_H$ °C.	$t_{Hg} - t_H$ °C.
0	0	0	0
10	+0·006	+0·025	+0·052
20	+0·010	+0·043	+0·085
30	+0·011	+0·054	+0·102
40	+0·011	+0·059	+0·107
50	+0·009	+0·059	+0·103
60	+0·005	+0·053	+0·090
70	+0·001	+0·044	+0·072
80	−0·002	+0·031	+0·050
90	−0·003	+0·016	+0·026
100	0	0	0

The negative values for $t_N - t_H$ at 80° and 90° are within the limits of experimental error, since an error of 0·01 mm. in the pressure reading at 100° would suffice to account for them.

It will be observed that the maximum divergence in the case of the mercury "Verre Dur" thermometer is about 0·107° at 40° C.; for the nitrogen gas thermometer 0·011°; and for the carbon dioxide thermometer 0·060° at about 45° C.

Calculation shows that the corrections necessary to convert readings on the hydrogen scale in the range 0° to 100° to the absolute thermo-dynamic scale are of the same order as the probable error of experiment in gas thermometer work.

The Scale from 100° to 600° C.—Numerous investigations have been made concerning the gas scale over this range. At the present day it is generally accepted that the platinum resistance thermometer (standardised in ice, steam, and sulphur vapour) will give a scale identical with that of the gas thermometer, to the same order of accuracy as that attainable in intercomparisons with the gas thermometer.

This important conclusion was arrived at by Callendar, who in 1887 made a direct determination of the resistance of a particular specimen of platinum wire at various temperatures up to 600° C. The platinum spiral was sealed into the bulb of the air thermometer by means of which the temperature was obtained.

By this device, Callendar avoided one of the greatest experimental difficulties of that time in gas thermometry—viz., the maintenance by gas heating of a large enclosure at a constant and uniform temperature.

The apparatus is shown diagrammatically in Fig. 2. The gas thermometer was designed for both constant volume and constant pressure work.

Instead of the customary practice of confining the gas by a column of mercury a sulphuric acid gauge was employed, which increased the sensitivity seven-fold, and also eliminated capillary errors entailed by the use of small-bore tube.

This gauge is denoted by the letters F G H J K in the diagram. When the three-way tap T_1 was turned in the middle of the acid column it prevented movement, whatever the variations of pressure.

The scale F G was adjusted so that when the end of the acid column stood at zero the pressure was the same in both limbs (F and K) of the gauge. To determine the pressure in terms of mercury corresponding to each reading of the scale F G, the way A M N was cleared by drawing the mercury into Q; the tap T_3 turned off, T_2 set in the position (T), and P_2 was connected to the open air through drying tubes, so that atmospheric pressure was communicated to the F limb of the U gauge F G by way of P_2. Readings of the manometer and of the U gauge were taken at various adjustments, from which the probable error of a single pressure observation and the pressure corrections were easily deduced; capillary effects being thus eliminated. In addition to the U gauge, there is another connection between the bulb capillary C and the manometer W by way of the bulbs A M N. These were filled with pure dry mercury, and were used for (1) work at constant pressure, (2) calibrating the bulb on the principle of the volumenometer, (3) as an open way through which the bulb could be filled with dry air.

Mercury could be withdrawn or added by means of the adjustable reservoir Q, or in weighed quantities by the tubes P_2, P_3 dipping into weighed beakers.

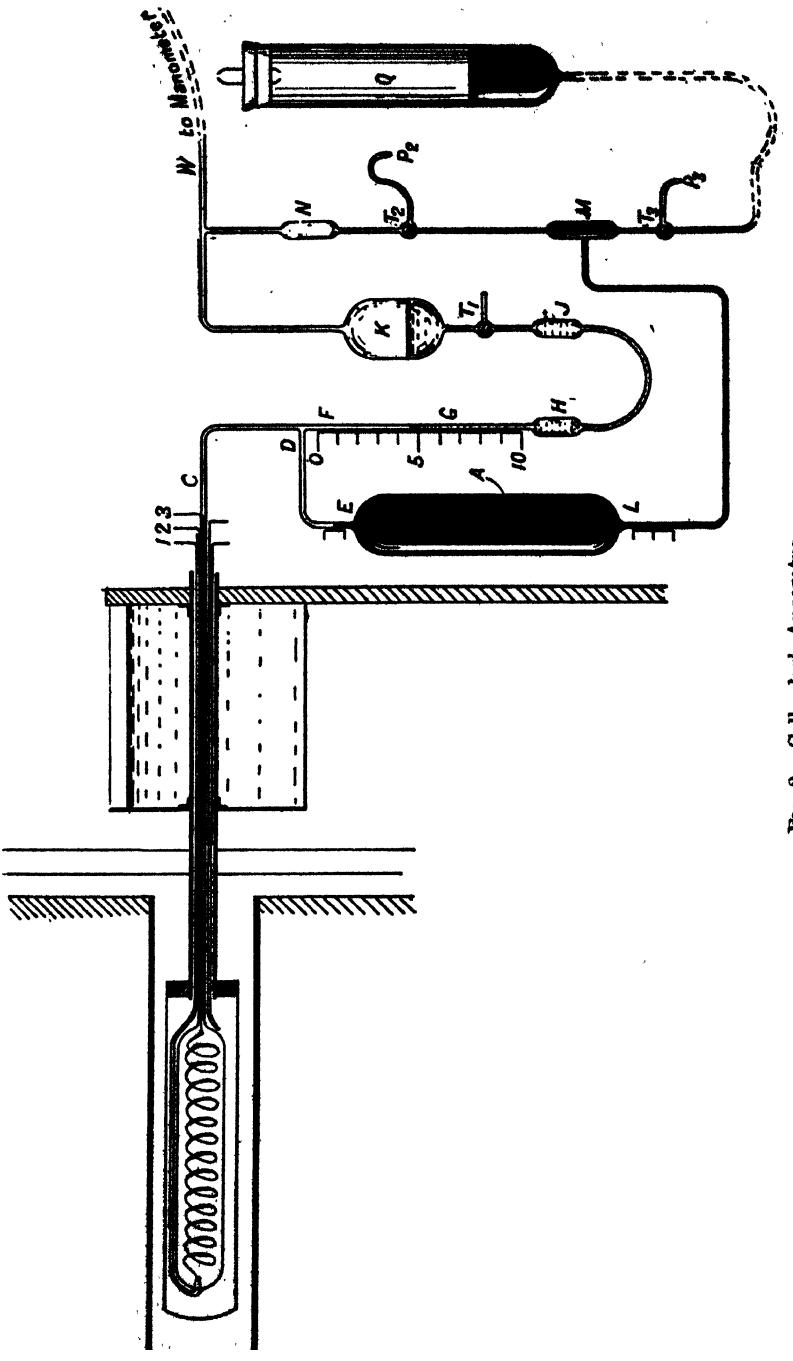


Fig. 2.—Callendar's Apparatus.

The bulb was dried and heated to a temperature of 400° to 500° C. W was connected to an exhaust pump and P_2 with the dry air supply; then, by means of T_2, the bulb could be connected alternately with either. After a series of such operations, mercury was re-admitted to fill A, and the operation was then complete.

When using the instrument as a constant-pressure thermometer, mercury was allowed to run from A into weighed beakers at P_3, until the sulphuric acid gauge indicated that the pressure in the bulb was at its original value. The scale F G gave the small variation of pressure, and the weight of mercury the expansion.

During each series of observations, the temperature of the bulb was maintained as steadily as possible.

The thermometer bulb was made from a piece of hard glass tubing; the coefficient of cubical expansion being deduced from observations on a length of the same tubing as that from which the bulb was made. It was observed that the expansion was irregular, on account of the structural and hysteresis changes in the glass.

The Resistance Coil.—The platinum wire was 2 metres long by 0·013 cm. diameter, wound in the form of a spiral. The resistance at room temperature was approximately 20 ohms. By the arrangement of double electrodes (shown in the diagram) the resistance of the lead wire outside the uniformly heated region could be allowed for.

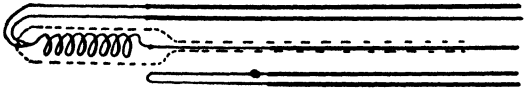


FIG. 3.

One end of the coil was led out through the capillary connecting the bulb to the manometer (Fig. 3). A double lead of the same wire, and which was coated with the same hard glass to imitate it exactly, was laid alongside. The other double lead consisted of 10 cms. of fine platinum wire, to the mid-point of which the other end of the spiral was fused. The fine wires were bent double and fused through the glass, while the projecting ends were fused on to thick (0·096 cm.) platinum wires coated with hard glass and laid alongside the others.

The resistance of the leads was determined on each occasion, and the correction amounted to about 3 per cent. of the total resistance.

The experiments showed that to the degree of accuracy attainable in the observations (about 1°), the variation of resistance of platinum with temperature could be represented by a parabolic formula.

The subsequent investigations of Callendar and Griffiths showed that this was generally true for wires of varying degree of purity, when the appropriate values of the coefficients were inserted in the parabolic formula.

In a direct determination of the boiling-point of sulphur with the gas thermometer, they obtained the 444·53° C., which was about 4° lower than that previously obtained by Regnault.

Harker and Chappuis (1899), and later Holborn and Henning (1911), submitted the parabolic formula to a rigorous examination. Employing a liquid bath to obtain uniformity of temperature, they made a direct comparison of a number of platinum thermometers with the gas thermometer at various temperatures between 100° and 500° C., and found no divergence greater than the probable error of experiment.

While these researches proved conclusively the validity of the parabolic formula for the representation of the variation with temperature of the resistance of platinum, there still remained very considerable discrepancies between the various values ascribed to the boiling-point of sulphur on the gas scale.

This is a fixed point of importance in practical thermometry on account of its use in the standardisation of resistance thermometers. Since a determination of the resistance value in melting ice, steam, and the vapour of boiling sulphur under standard pressure is sufficient to determine the constants of the parabolic formula.

Determinations of the Boiling-point of Sulphur.—The value 448·38° C. obtained by Regnault was found later to be nearly 4° too high, doubtless on account of the superheating of the vapour in his form of apparatus.

In the course of their comparison of the resistance thermometer with the gas thermometer, Harker and Chappuis, and Holborn and Henning, made some determinations of the boiling-point of sulphur on the gas scale, employing the resistance thermometer as intermediary. Their values are indirect in so much that the gas thermometer was not directly employed to determine the temperature of the sulphur vapour, but are entitled to full weight, since the resistance thermometer was directly compared with the gas thermometer in salt baths at temperatures in the vicinity of the sulphur boiling-point.

Day and Sosman (1912) made a direct determination of the sulphur point, using a nitrogen-filled thermometer, whose bulb was of platinum-rhodium alloy. It was of 205 c.cs. capacity, and the nitrogen was under an initial pressure of 500 mms. of mercury.

Great precautions were taken to eliminate systematic errors. An aluminium shield surrounded the bulb in the sulphur tube, to prevent the condensed sulphur from lowering its temperature below the true boiling-point, and also to eliminate radiation loss to the walls of the tube.

The sulphur bath was electrically heated, and it was found that 35 per cent. variations in the current produced no variation in the observed boiling-point.

To ascertain whether the temperature of the walls of the tube had any influence in some of the experiments, the external jacket was heated until the temperature of the air gap was as high as that of the sulphur vapour within the tube. Provided the tube was full of vapour this produced no apparent change in the value obtained.

A direct comparison of the temperature given by this form of apparatus with that obtained in the Meyer tube form of sulphur boiling apparatus

(Fig. 33) devised by Callendar and Griffiths, showed a systematic difference of but 0·04°.

The probable source of the divergences in the results obtained by various observers since the time of Regnault is uncertainty in the coefficient of cubical expansion of the bulb material.

Fused quartz has the smallest coefficient of the materials available for the construction of the bulb of gas thermometers. Values obtained by Eumorfopoulos with a constant-pressure thermometer constructed of fused silica are given in Table II. below.

TABLE II.—Gas Thermometer Determinations of the Boiling-point of Sulphur since 1890.

Date.	Author.	Thermometer.	Gas	Pressure, mms.	Original figure.	Thermodynamic scale.
1890	Callendar & Griffiths	Constant pressure	Air	760	444·53 C.	444·91 C.
1902	Chappuis & Harker	Constant volume	Nitrogen	530	444·70 C.	444·80 C.
1908	Eumorfopoulos	Constant pressure	Air	760	444·55 C.	444·93 C.
1911	Holborn & Henning	Constant volume	Hydrogen Helium	623 612	444·51 C.	444·51 C.
			Nitrogen	625	444·39 C.	
1912	Day & Sosman	Constant volume	Nitrogen	502	444·45 C.	444·55 C.

The value 444·6° C. is, at the present time, the generally accepted value for the boiling-point of sulphur on the thermodynamic scale.

The Scale from 500° to 1,500° C.—Numerous investigations with the gas thermometer have been carried to high temperatures. The difficulties the early pioneers had to face were of a very real character, as a study of the memoirs of Princeps, Pouillet and Barus will show. Electric furnaces, homogeneous platinum alloy thermo-elements, and other refinements of the present day were unknown.

Amongst the earlier observers to make gas thermometer comparisons above 1,100° C. were Holborn and Wien, who, in 1895, carried the air thermometer scale to 1,450° C. They employed a very refractory porcelain bulb, and the thermocouple was enclosed within the bulb.

The melting-point of nickel, as determined by the calibrated thermo-element, was found to be 1,484° C., a value exceeding that accepted at the present day by 32°.

In 1906 Holborn and Valentiner made gas thermometer comparisons up to 1,680° C. The bulb was made of pure iridium, and was only 50 c.cs. in capacity. The greatest difficulty was the lack of uniformity in the temperature over the bulb, and variations amounting to 60° occurred along its length.

The iridium, being volatile at these temperatures, had a very destructive effect on the thermocouples used as intermediary for transferring the scale.

The melting-point of palladium was found to be 1,575° C., a value 25° higher than Day and Sosman's recent value.

In 1911 Day and Sosman published an account of an investigation which had been going on for seven years at the Carnegie Institution. Reference must be made to the original paper for a detailed account of the apparatus; here it will suffice to refer to the salient features.

The thermometer was of the constant-volume type filled with nitrogen, the bulb being of about 200 c.cs. capacity. Both bulb and capillary tube

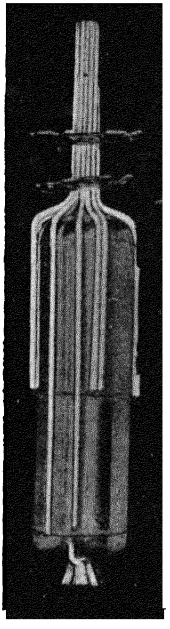


FIG. 4.—Day and Sosman's gas thermometer bulb with thermo-elements in position.

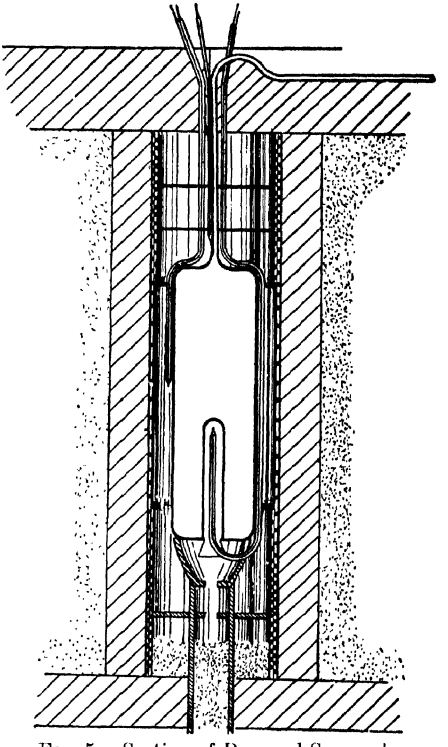


FIG. 5.—Section of Day and Sosman's furnace and gas thermometer bulb.

were made of a platinum-rhodium alloy, the choice of which was determined by considerations of rigidity at high temperatures and possible contamination of the thermocouples exposed with the bulb in the furnace.

The expansion-coefficient of the bulb was deduced from experiments on the linear expansion of a bar of the same composition.

To diminish the danger of deformation of the bulb at high temperatures, the furnace was enclosed in a gas-tight shell, in which the pressure was adjusted at each temperature until equal to that within the bulb.

A section of the furnace and internal arrangement is given in Fig. 5.

For the highest temperatures the heating coil was made in three sections, internally wound.

The current through each coil was separately adjusted, so as to produce as uniform a temperature distribution as possible over the space occupied by the thermometer.

Internal windings * have disadvantages from the point of view of uniformity, but are inevitable where temperatures up to 1,550° C. are required with platinum windings.

The distribution of temperature over the bulb was obtained by binding a number of pure platinum wires to different points of the bulb and insulating by means of Marquardt capillary tubing. The platinum-rhodium walls of the bulb formed the other element of each couple.

A number of independent platinum-platinum 10 per cent. rhodium couples were also inserted in the furnace, one of which was placed in the re-entrant † tube of the bulb as illustrated in Fig. 5.

Owing to the impossibility of insulating the thermo-elements completely from the heating circuit at high temperatures, alternating current had to be employed for heating.

The results of the work are embodied in the following melting- and freezing-point determinations of metals and salts of stated purity :—

TABLE III.

Metal.	Temperature °C.
Cadmium,	320·2°
Zinc,	418·2
Antimony,	629·2
Silver,	960·0
Gold,	1,062·4
Copper,	1,082·6
Nickel,	1,452·3
Cobalt,	1,489·8
Palladium,	1,549·2
Diopside (melting-point). ($MgSiO_3$, $CaSiO_3$)	1,391·2
Lithium silicate, (Li_2SiO_3)	1,200·9°
Anorthite, (Al_2SiO_5, $CaSiO_3$)	1,549·5°

NOTE.—The salt melting-points are reproducible to probably 1°.

* For the same conditions of insulation, etc., an internal temperature 200° higher can be obtained with the heating coil within instead of over the outside of the porcelain tube.

† The re-entrant tube for bringing the couple to the centre of the bulb was first employed by Barus in 1889, when using a rotating gas muffle around the thermometer to produce uniform temperature conditions.

Although the investigation was carried out with great thoroughness, the low temperature portion of the scale, as represented by the freezing-points of cadmium and zinc, is inconsistent with the work of several observers on the sulphur-point. The difference is considerably greater than the probable error of experiment in this region, and is of the order of 1°.

This fact led Day and Sosman to repeat some of their work at various temperatures up to 600° C., employing the same gas thermometer immersed in a well-stirred salt bath. The revision confirmed the fact that their previous values were too low by about 1°, and this they explain by stating that an integration of the temperature over the bulb in an electric furnace gives a slightly higher value for the mean temperature than the true value, as obtained in a well-stirred salt bath. They further point out that their apparatus was primarily designed for high temperature work, where the use of a salt bath is not at present a practicable proposition.

Since the values at higher temperatures obtained by various observers differ by several degrees, it is impossible to ascertain whether the above error is systematic throughout the range.

Range 0° to − 200° C.—Holborn and Wien in 1901 extended their previous comparison between the gas and platinum thermometers between 0° and 500° C., by making comparisons at − 78° C. and − 190° C., temperatures obtainable by the use of solid CO_2 and liquid air. The coil of the platinum thermometer was enclosed within the bulb of the gas thermometer, so as to minimise the error due to the slowly varying temperature. They found that the parabolic formula obtained by standardising in ice, steam, and sulphur vapour represented the gas scale between − 78° and 500° C., but below − 78° C., deviated ; the divergence amounting to 2·3° at − 190° C., the platinum thermometer reading too low.

Travers and Gwyer, in 1905, made comparisons at the same two temperatures with improved apparatus of greater sensitivity. They found the departure of the platinum at − 190° C. to be 2·23°, a value in close agreement with that of Holborn and Wien.

Henning, in 1913, carried out a detailed investigation over the range 0° to − 200° C. The comparison was effected between the hydrogen gas thermometer and a number of platinum thermometers constructed of wire of varying degrees of purity. The lowest temperatures were obtained by means of liquid air baths, while the intermediate points were obtained in a bath of alcohol or petroleum ether cooled by liquid air.

His experiments showed that the parabolic formula was not valid below − 40° C., and, moreover, that platinum thermometers constructed of wires of varying purity were not consistent, but gave results differing by as much as half a degree when immersed in the same bath.

He found, however, that the scales of two different thermometers could be connected over this range by a formula involving only one constant, and that the constant could be determined by a comparison of the thermometers at a single temperature.

Thus, if platinum temperatures* pt' and pt are deduced from observations with two thermometers compared at the same temperature, the following empirical relationship holds good :—

$$pt' - pt = c\ pt\ (pt - 100)$$

The constant c may be obtained by a comparison of the two thermometers at one low temperature, as, for example, in a liquid air bath.

Although the above formula would appear to require for its evaluation the use of a standard platinum thermometer, whose scale has been directly compared with the gas thermometer, it is possible to utilise Henning's data by making the assumption that his gas thermometer would give the accepted value $-182{\cdot}9_5°$ C. for the boiling-point of oxygen.

The curve in Fig. 6 is plotted from data given by Henning for his standard thermometer, having $\alpha = 0{\cdot}0039150$ and $\delta = 1{\cdot}484$.

Hence, if a platinum thermometer has to be calibrated down to low temperatures, it is only necessary to determine the resistance in ice, steam, sulphur vapour, and boiling oxygen.

The departure of the scale at the oxygen-point can then be compared with Henning's value at $t = -182{\cdot}9_5°$ C.

In Table IV. the values of α, δ, and c are given for the various platinum thermometers tested, and it will be observed that there is no obvious connection between c and the δ of the parabolic formula (see Chap. III.).

TABLE IV.

100α.	δ.	$c \times 10^5$.
0·38624	1·510	−0·68
0·38874	1·492	+0·09
0·39131	1·491	+0·06
0·39132	1·491	+0·11
0·39150	1·484	0
0·39134	1·486	−0·10
0·39143	1·482	+0·10

Choice of Gas for Use in Gas Thermometers, and the Relation between the Practical Gas Scale and the Absolute Thermodynamic Scale of Temperature.—Since the thermodynamic scale of temperature is the ultimate standard of reference, it is desirable to choose as gas to be employed in the thermometer that one which approaches nearest the " ideal gas."

In practice it has not always been possible to do this. Hydrogen, which has a very small correction to bring its scale to the thermodynamic, has been found to be entirely satisfactory up to temperatures of about 400° C. At higher temperatures the ready diffusivity of hydrogen through platinum and its alloys has necessitated recourse being made to nitrogen, which has been employed up to 1,600° C.

* See Chapter III.

The discovery of the monatomic gases, helium, argon, and neon, with no chemical affinity, has placed at the disposal of gas thermometer workers elements which approach the " ideal gas " nearer than hydrogen or nitrogen. Helium also possesses the very valuable characteristic of an extremely low liquefaction-point, and for work at low temperatures it is now coming

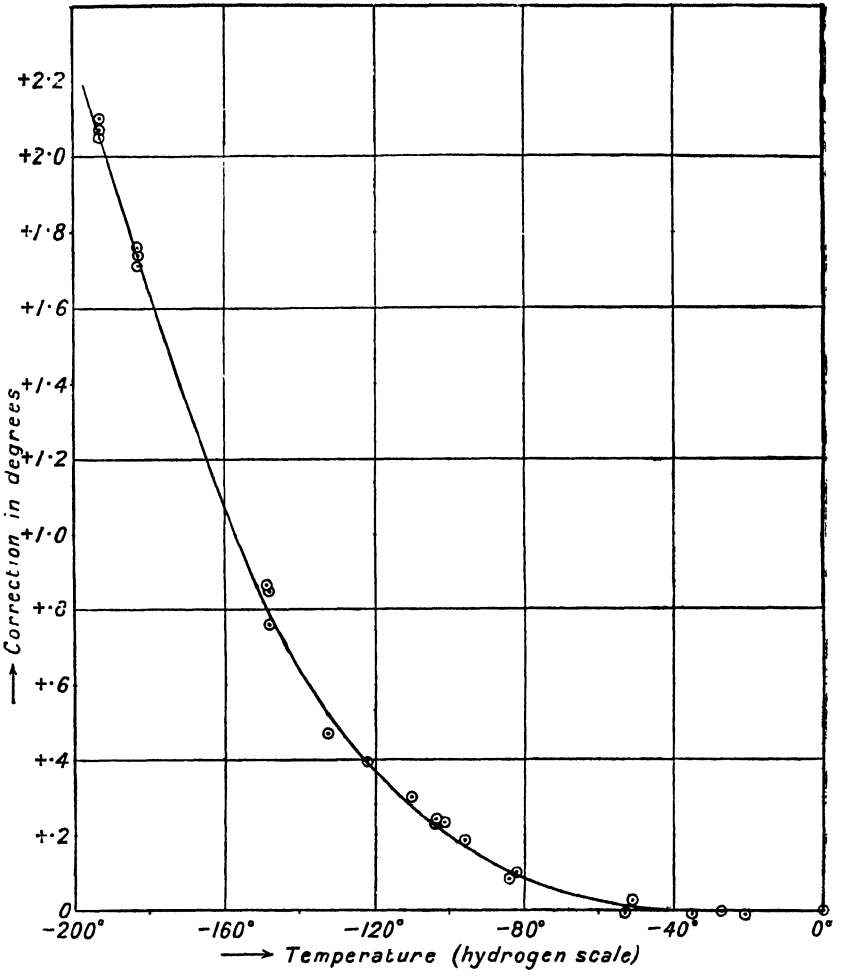


FIG. 6.—Curve plotted from Henning's data for his standard thermometer.

into general use. At higher temperatures it readily diffuses through quartz and glass, consequently argon will probably be employed for this part of the range in future.

Corrections to Thermodynamic Scale.—Hydrogen, nitrogen, and air

approximate fairly closely to the " ideal gas " over the range in which they obey Boyle's law.

The corrections necessary to convert the practical gas scale to the thermodynamic scale can be calculated from certain physical properties of the gas. The method of calculation is complicated by the necessity of employing indirect methods, owing to the lack of the requisite data.

To determine the departure of a real gas from the ideal state a knowledge of two quantities is necessary: (1) the departure of the product $p\,v$ from a constant value under isothermal conditions of change; (2) the value of λ, the amount of heat that must be added to unit mass of gas during a free expansion, in which its volume is increased by unity, to keep its temperature constant.

Both these quantities are small and difficult to measure directly with the necessary degree of accuracy.

Kelvin first realised the need of experimental data to permit of the calculation of the corrections to the practical gas scale, in order that it might be expressed in terms of the thermodynamic scale.

In collaboration with Joule he devised in 1850 the " porous plug " experiments. In these experiments a gas is caused to flow steadily through a porous plug, and the change in temperature is measured. The difference in temperature obtained depends upon both of the quantities referred to above, and consequently the reduction of the observations to give the desired corrections is a matter of some difficulty.

The problem has been attacked from different standpoints by Kelvin, Rose-Innes, Callendar, Berthelot, and Buckingham.

The order of agreement between the results will be seen by a study of Table V.

TABLE V.—Corrections to the Constant Pressure ($p = 1{,}000$ mms.) Hydrogen Scale between 0° and 100° C.: the Values to be Subtracted from the Observed Temperatures.

I.	II.	III.	IV.	V.	VI.	VII.
$t°$ C.	Rose Innes (1901).	Callendar (1903).		D. Berthelot.	Buckingham.	
20	0·0024	0·0025	0·0013	0·0008	0·0026	0·0023
40	0·0033	0·0035	0·0018	0·0010	0·0037	0·0032
60	0·0031	0·0033	0·0016	0·0009	0·0037	0·0032
80	0·0019	0·0020	0·0010	0·0005	0·0024	0·0022

The data in columns II., III., VI., and VII. have been obtained by calculation based on the value of the Joule-Kelvin effect and are in agreement. On the other hand, data in columns IV. and V. have been obtained by general consideration of the equation of state of the gas, without the

use of the Joule-Kelvin effect. The latter values are apparently only $\frac{1}{2}$ or $\frac{1}{4}$ the mean of the others, and are not so reliable.

Outside the range 0° to 100° C., extrapolation of data determined within this range has to be resorted to.

Table VI. summarises the corrections to the gas scales which are in use at the present day.

TABLE VI.—Corrections to Thermodynamic Scale $\theta_0 = 273{\cdot}10°$ C.

Temp. Centigrade.	Constant pressure = 76 cms.			Constant volume $p_0 = 100$ cms.		
	Helium.	Hydrogen.	Nitrogen.	Helium.	Hydrogen.	Nitrogen.
− 250	—	—	—	+0·02	—	—
− 200	+0·10	+0·26	—	+0·01	+0·06	—
− 100	+0·03	+0·03	+0·33	0·000	+0·014	+0·07
− 50	+0·009	+0·004	+0·09	0·000	+0·004	+0·02
+ 25	−0·002	−0·002	−0·013	0·000	0·000	−0·006
+ 50	−0·002	−0·003	−0·017	0·000	0·000	−0·006
+ 75	−0·002	−0·002	−0·012	0·000	0·000	−0·004
+ 150	+0·005	+0·003	+0·04	0·000	+0·001	+0·01
+ 200	+0·01	+0·01	+0·10	0·000	+0·002	+0·04
+ 450	+0·07	+0·04	+0·50	0·00	+0·01	+0·15
+1000	+0·24	+0·01	+1·7	—	+0·04	+0·70
+1500	—	—	+3·0	—	—	+1·3

Standard Temperatures in the Range covered by Gas Thermometer Experiments.—The vast amount of labour expended on gas thermometer observations, briefly sketched in the preceding pages, has resulted in the fixing, with some degree of certainty, of a series of standard temperatures which may form the basis of a common scale of temperature.

Table VII. summarises the most probable values of a series of standard temperatures, according to recent research.

Most of the substances are easily obtained of the requisite purity. But in the case of benzophenone and oxygen special attention must be given to the purity of the samples employed.

The appropriate method of utilising these fixed points for the calibration of auxiliary standards is given with the description of these particular instruments.

TABLE VII.—Standard Temperatures.

(Thermodynamic scale.)

Temperature Centigrade.	Substance.	Uncertainty.	Reproducibility	Atmosphere.	Crucible Material.
−252·7	Hydrogen,	0·2	0·05		
−182·9$_5$	Oxygen,	0·1	0·03		
−78·5	Solid CO_2 in petrol, (sublimation)	0·1	0·03		
−38·88	Mercury,	0·1	0·05		
32·383	$Na_2SO_4 + 10H_2O$.	0·002	0·001		
		(Transformation to anhydrous salt).			
217·9$_3$	Naphthalene,	0·02	0·01		
231·84	Tin,	0·1	0·05	Reducing	Graphite
302	Diphenylamine,	0·3	0·05		
305·90	Benzophenone,	0·05	0·02		
320·9	Cadmium,	0·1	0·03	Air	,,
327·4	Lead,	0·1	0·05		,,
419·4	Zinc,	0·1	0·15	Air	
444·6	Sulphur,	0·1	0·03		
630	Antimony,	0·5	0·3	Reducing	,,
738	Cu_4Sn, (68·2 % Cu : 31·8 % Sn)				,,
779	Ag_4Cu_2,	1·0	1·0	Reducing	
801	Salt (NaCl).	2·0	1·0		
852	Sodium carbonate,				
883	Sodium sulphate.				
961·7	Silver,	1·0	0·5	,,	
1,064	Gold,	2·0	1·0	Air or reducing	
1,066	Potassium sulphate,				
1,083	Copper.	2·0	1·0	Reducing	
1,201	Lithium silicate,				
1,452	Nickel,			H_2 or N_2	Refractory
1,490	Cobalt.			,,	clay, borax
1,553	Palladium,		3	Air	over metal
1,391	Diopside (pure).			Air	Platinum.
1,549	Anorthite (pure),				

The estimates of the limits of the uncertainty in the absolute values and of the reproducibility are due to Burgess.

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CHAPTER II.

THE MERCURIAL THERMOMETER.

THE simplicity of the mercury in glass thermometer and the convenience of a direct reading temperature scale have led to the very general use of this type of pyrometer, and the peculiarities of the instrument have received much study during the past half-century.

The result of this accumulation of experience has been to show that, where extreme accuracy is desired, the simplicity of the instrument is more apparent than real, and that a well-designed resistance thermometer outfit easily surpasses it in sensitivity, besides being free from " zero depression," * which is the inherent failing of the mercury in glass thermometer.

The Range 0° to 100° C. with the Mercury Thermometer.—In the fundamental interval 0° to 100° C. the mercury thermometer received very careful study at the International Bureau of Weights and Measures at Sévres, and it was shown that by adopting suitable precautions it was possible to reproduce the temperature scale to better than 0·005° in this interval. The standard thermometers of the Bureau were of " Verre dur " glass, since this glass had the smallest zero depression of the then known glasses. This thermal hysteresis manifests itself in troublesome changes of the zero after exposure to higher temperatures and in slowness in settling to equilibrium when maintained at a definite temperature.

The mercury thermometer was graduated to give a temperature scale of its own; the degree being defined as one-hundredth of the volume of the stem contained between the readings, at the melting-point of ice, and the steam-point of water under standard conditions.

The object of Chappuis' work, previously described, was to obtain the relation between this scale and that of the international hydrogen scale in which the degree Centigrade is defined as one-hundredth part of the change in pressure of a constant volume of hydrogen gas, when its temperature is changed between that of melting pure ice and that of steam from boiling pure water at normal pressure, the initial pressure of the gas at 0° being 1,000 mms. of mercury.

Sources of Error in Mercury Thermometers.—Since it is impossible to construct a thermometer to comply with the ideal conditions contemplated above, it is necessary to calibrate each mercury thermometer and determine corrections for the following :—

1. The variations in the calibre of the capillary bore.
2. The variation in the fundamental interval from 100° C.

* The difference in the ice-point reading taken after a long time at 0° C. and that immediately after exposure to a temperature of 100° C.

3. The influence of the variations in the external pressure on the bulb from standard atmospheric pressure.

4. Effect of the internal pressure on the volume of the bulb due to the height of the column of mercury above the centre of the bulb.

5. Changes in the zero or " ice-point " reading.

It is the standard practice in work of the highest precision to determine the reading in melting ice immediately after each observation taken by the thermometer.

When the above corrections have been ascertained, it is then possible to express its readings in terms of the international gas scale.

The Bureau of Weights and Measures has supplied to the various national laboratories standards whose corrections have been determined, and which have also been compared with the four " Verre dur " thermometers by which the normal hydrogen scale is preserved at the Bureau. So that it is now possible to obtain the corrections necessary to reduce the readings of any thermometer to the international hydrogen scale by a direct comparison with one of these. This procedure is to be recommended, as it is questionable whether the calibration method of obtaining the corrections of a thermometer is defensible on the score of precision or of economy of time. The determination of the absolute corrections of a thermometer at a large number of points by direct comparison in a well-stirred bath requires less time than the determination of the relative corrections by calibration at a few points. Moreover, the user is at the mercy of the thermometer-maker as to whether the composition of the glass is identical with that of " Verre dur " or other standard glass.

The Calibration of a Standard Mercury Thermometer.—The procedure followed in the work of calibrating a primary standard is of interest in the light it throws on the peculiarities of mercury thermometers and in showing the care and attention which must be bestowed on the instrument if readings of great accuracy are desired.

The preliminary step is to remove all strains set up in the glass during manufacture by a thorough annealing. This is effected by a prolonged exposure to a temperature higher than that to which it is proposed to submit the thermometer in actual use.

One result of this annealing is to produce a very considerable rise in the zero-point.

1. **Calibration of the Bore.**—The graduations on the stem are supposed to be equidistant. The standard practice is to break off mercury columns approximately 10°, 20°, . . . 90° in length and measure the excess length of these columns over the corresponding spaces at successive points along the scale.

The method of reducing the data to obtain the bore corrections need not be described here.*

* The arithmetical artifices employed in the reduction of the observations by the method of least squares is described in *Traité Practique de la Thermometrie de Precision*, Guillaume. Also in a paper entitled *An Example in Thermometry*, by A. S. Cole and E. L. Durgan. Minor contributions, *Physical Review*, vol. iv., p. 207 (1897).

2. **Determination of the Fundamental Interval.** (*a*) **Steam-point.**—The type of hypsometer employed at the International Bureau is shown in Fig. 7. The steam jacket is capable of rotation from the horizontal to the vertical position, so that readings may be taken in both positions.

The thermometer is inserted in the hypsometer with a few tenths of a degree projecting for reading. A thin rubber disc is better than a cork for closing the mouth, since it permits of the steam heating practically the whole of the mercury column.

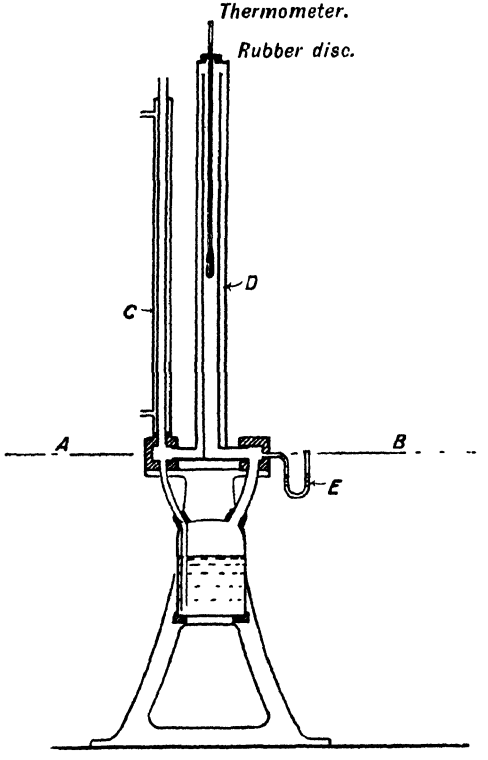


FIG. 7.—Hypsometer employed at the International Bureau.
A, B, axis of rotation; C, condenser; D, steam jacket; E, water manometer.

A U-tube water manometer is fixed to the steam jacket, so that the excess pressure within the apparatus may be added to that of the barometric pressure.*

Alternate barometer and thermometer readings are taken.

Even at temperatures as low as 100° C., a slight distillation of the mercury will take place from the top of the column to the cooler region above; some observers have eliminated this by mounting a small glass bell jar over the hypsometer, so that the thermometer is entirely enclosed in the steam.

* *The boiling-point of water at various pressures is given in* Table XLV. (Appendix).

Others have overcome this difficulty by passing hot air over the emergent end.

Readings are taken with the hypsometer in both the vertical and the horizontal positions, as this determines the internal pressure coefficient.

The observations are taken first in the horizontal position, then in the vertical; this sequence avoids the possibility of distilled mercury joining with the column, since the reading is lower in the vertical than in the horizontal position.

This procedure, however, has one disadvantage, in so much as the meniscus in the vertical position is a falling one.*

The difficulty may be overcome by withdrawing the thermometer a few centimetres, so as to slightly cool the stem; on replacement the meniscus will be a rising one.

(*b*) **Ice-point.**—A convenient form of ice-point apparatus is shown in Fig. 8.

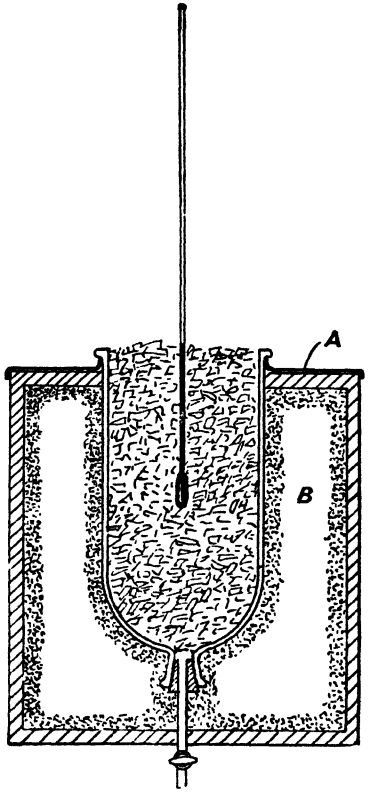


FIG. 8.—Ice-point apparatus.
A, lead sheet; B, cork dust.

Finely powdered ice is employed, saturated with distilled water, the water being drawn off until the surface whitens. The ice-point is determined as soon as possible after withdrawal from the hypsometer. Usually a period of two or three minutes must elapse before the thermometer can be safely inserted into the ice. Since the zero begins to rise after its temporary depression, at the rate of about 0·001° per minute, it is necessary in work of the highest precision to allow the same interval of time to elapse between the withdrawal from the higher temperature bath and the determination of the ice-point.

In order to obtain a rising meniscus at the ice-point, a super cooler has been proposed, consisting of a test-tube containing mercury inserted into a freezing mixture. By this means it would be possible to cool the bulb a few degrees below 0° before inserting into the ice bath.

The temporary depression of the zero after heating to higher temperatures has been exhaustively studied by several observers for "Verre dur" thermometers.

* Readings with a receding column are not reliable owing to "stiction."

The heating is effected by a number of resistance units of the type shown in Fig. 10, which illustrates the internal construction of a double unit wound ready for insertion into an envelope of thin sheet copper.

Two plain sheets of mica (not shown) are fastened over the faces of the unit to insulate it from the metal walls of its container.

The copper envelopes are soldered to a brass plate closing the end of the limb containing the stirrer and project up into the stream of water.

The units are designed for working off the 100 volt supply circuit, and are each of 400 watts capacity.

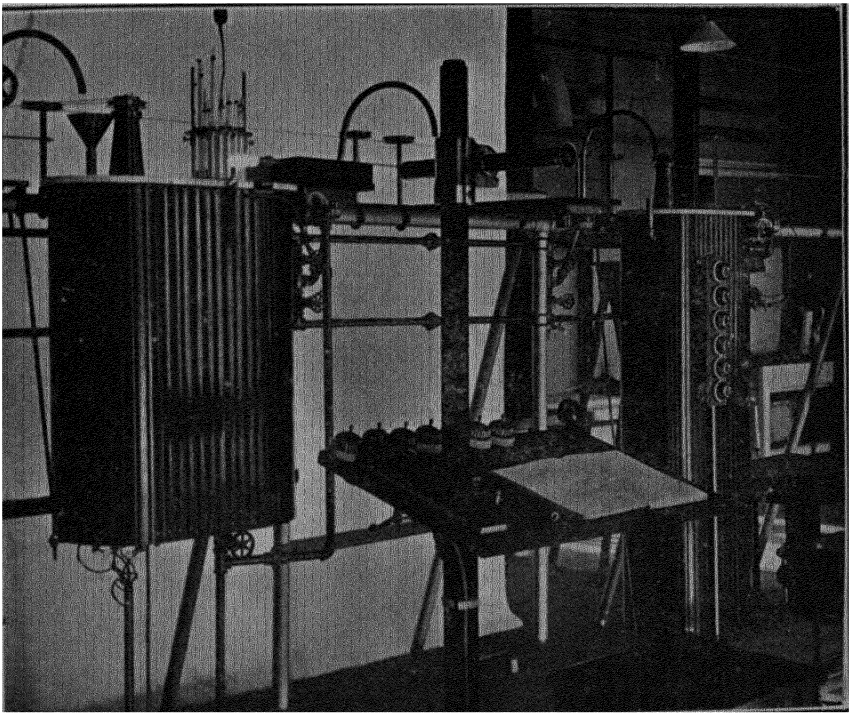


FIG. 9.—Water bath for the comparison of mercury thermometers.
The electrical connection to the heater units will be observed in the bottom left-hand corner.

Generally six units are provided for each bath and are contained in three separate pockets. Variations in the energy supply are obtained by means of seven two-way lamp switches with an intermediate "off" position.

The six resistance units are connected in series, and from them are led seven connections to the neutral points of the switches. The upper and lower contacts of each switch are connected respectively to the

positive and negative poles of the 100-volt supply circuit.

By this arrangement, permitting series and parallel combination of the units, the energy can be varied from 60 to 2,400 watts without the use of any series resistance. To obtain still smaller heating energies a sliding resistance of 100 ohms is connected in series with the first unit.

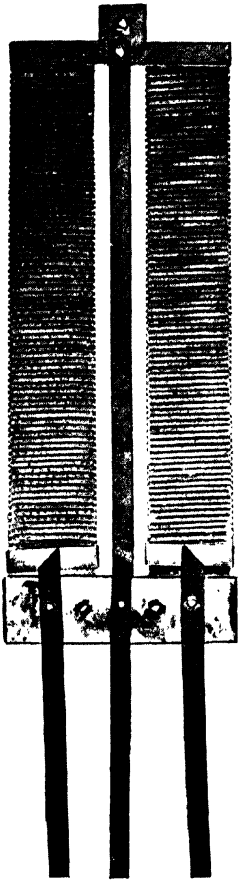


FIG. 10.—Heater element for water bath.

It might be remarked that the life of a suitably proportioned unit has been found to be about 500 kilowatt hours.

High Temperature Mercurial Thermometers.—By employing a hard glass and filling the upper part of the stem with gas under sufficient pressure to prevent distillation, or boiling of the mercury, it is possible to measure temperatures as high as 500° C. But to determine temperatures absolutely to within 1° at 450° C. demands considerable care to eliminate the various sources of error to which these instruments are subject.

Borosilicate glass 59''' is generally employed for the construction of high-range thermometers with the divisions engraved directly on the stem. Generally there is an auxiliary bulb, or reservoir, at the top, which is "large" in proportion to the volume of the bore of the stem itself; its volume usually being 20 times that of the internal volume above 0°.

This bulb is filled with gas—nitrogen or carbon dioxide—under sufficient pressure to prevent boiling of the mercury at the highest temperature at which the thermometer is intended to be used.

The pressures necessary are—

2	atmospheres	for a maximum	temperature of	400° C.
20	,,	,,	,,	550° C.
60	,,	,,	,,	750° C.

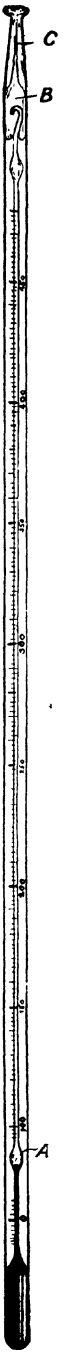


FIG. 11.—High-range thermometer.

A, bulb to take expansion from 0° to 100°; B, auxiliary bulb; C, narrow bore tube filled with shellac or fusible metal.

To seal off the thermometer under pressure a little shellac or fusible metal is placed in the narrow bore tube above the auxiliary bulb, and before sealing off this is heated until it flows down, sealing up the tube while still under pressure. The external pressure may then be removed and the glass tube sealed off above in the usual way.

Occasionally high-range thermometers are made by fusing off the capillary containing gas at atmospheric pressure with the mercury standing at some low point.

Evidently, if the length of the capillary is properly chosen, the mercury, on rising, will compress the contained gas, increasing the pressure sufficiently to prevent boiling at all temperatures on the scale. This method is not so satisfactory as the previous one, since the internal pressure increases rapidly as the temperature rises, depressing the readings of the thermometer. This depression of the zero is not constant for different instruments, owing to the difficulty of duplicating the conditions.

The scale of high-range thermometers generally has about 30° divisions engraved at the ice-point, 10° below and 20° above, the same at the 100° point, the two points being separated by a small reservoir to shorten the length of the stem. Then the graduation proceeds in single degrees over the higher portion of the range.

In others the reservoir takes up the expansion from 0° to 200° C.

The graduations at 0° are essential for keeping a check on the behaviour of the instrument by frequent ice-point readings.

If the scale of a borosilicate glass thermometer were obtained by extrapolation of the hundred degrees between ice and steam, it would differ considerably from the gas scale, as the data in Table VIII. show :—

TABLE VIII.

Gas thermometer scale. °C.	Mercury thermometer borosilicate glass scale. °C.	Gas thermometer scale. °C.	Mercury thermometer borosilicate glass scale. °C.
0	0	375	385·4
100	100	400	412·3
200	200·7	425	440·7
300	304·1	450	469·1
325	330·9	475	498·0
350	358·1	500	527·8

It is interesting to note that under similar conditions a thermometer of Jena 16''' glass would read 301·96° C. for a gas thermometer temperature of 300° C., so that the scale of the mercury "Verre dur" glass thermometer approximates more nearly to that of the gas thermometer than that of borosilicate glass. This, however, is of no importance, since at the present day the scales are never obtained by extrapolation.

Salt Baths for Comparisons at Higher Temperatures.—Generally the scales of instruments which are to serve as standards are pointed off by comparing the thermometer with a resistance thermometer in oil and nitrate baths.

Fig. 12 illustrates a form of salt bath suitable for comparisons between 200° and 600° C.

The salt mixture consists of about equal proportions of sodium and potassium nitrates. It is important not to expose any joints or brazing to the action of the molten nitrate; the only satisfactory mode of construction is to employ castings or oxy-acetylene welded steel parts.

Fig. 13 is a photograph of a cast-iron container for a molten salt bath.

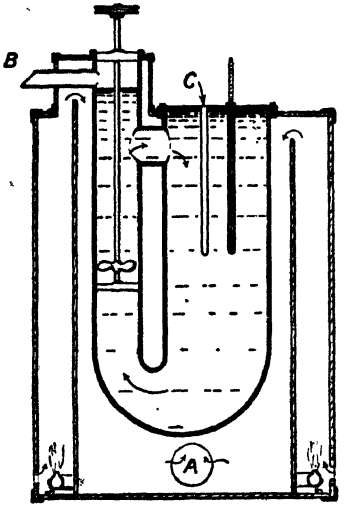


FIG. 12.—Salt bath for comparisons of thermometers between 200° and 600° C.

A, flue pipe; B, overflow and filler tube; C, steel tube (thin-walled) screwed into top of bath.

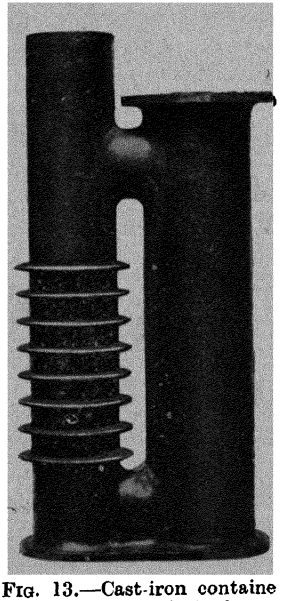


FIG. 13.—Cast-iron containe for molten salt bath.

The hot gases should be so directed as to come in contact with the upper part of the bath first. This ensures that the frozen salt melts from the top downwards, and thus avoid the severe strains which would be set up should the bottom be first heated.

Changes in High-range Thermometers.—When a thermometer is new and has not been submitted to any annealing, considerable changes of zero take place, due to the strains set up in the glass in manufacture and to thermal hysteresis. A high-range thermometer is, of course, subject to the same changes as a low-range one, only they appear in a more aggravated form.

(1) **Permanent Changes.**—There occurs a permanent contraction of the bulb and stem, rendering all the readings higher than the original values. This contraction takes place more rapidly if the temperature is raised. In the case of a thermometer maintained at room temperature the changes will extend over years. They can, however, be brought speedily to conclusion by subjecting the thermometer for a period of 4 to 10 days to a temperature higher than that which it will be required to measure in practice and by following this treatment with a slow cooling extending over a period of 3 to 6 days. The result of this annealing, or artificial ageing, is to produce a rise of the zero of the order of 30° when the thermometer has been subjected to a maximum temperature of about 450° C.

(2) **Temporary Changes.**—All thermometers, when heated, show changes which are temporary in character and the magnitude of the changes depend on the temperature and the composition of the glass.

If the zero of a thermometer is determined immediately after it has been exposed to high temperature, it will be found to be depressed below the value obtained, when the thermometer has been at room temperature for a long period. For a top temperature of 400° to 500° C. the depression of the zero may amount to 1°. Consequently, in work of precision, it is the custom to determine the zero as frequently as possible by ice-bath operations.

While an absolute accuracy of 1° at high temperatures is about the best obtainable with mercury thermometers, to secure this it is necessary to observe some additional precautions to those already described in connection with low-range thermometers.

Some Additional Precautions.—1. Prolonged exposure of the thermometer to high temperatures should be avoided. Distillation of the mercury from the top of the column to the colder portion of the stem invariably occurs to some extent, and it is impossible to join up the minute globules. The effect of such distillation can be observed on the zero point reading.

2. The thermometer should be immersed in the hot region to as near the top of the column as the conditions permit. Emergent stem corrections are, at the best, but makeshifts, and at high temperatures their magnitude is apt to become serious even with a small emergence. For example, a thermometer was tested at a temperature of 450° C., with about 14° of the column (corresponding to the length of 11 mms.) emergent; the reading was 1° low in consequence.

The emergent stem correction is usually calculated by the formula—

$$\text{Correction} = 0{\cdot}00016(T - t)n$$

where T = temperature of bath,
t = ,, air,
n = number of degrees exposed.

Where the conditions of the experiment necessitate an emergent column, it is advisable to calibrate the thermometer under precisely similar conditions.

Thermometer Glass.—The composition of the glass is a matter of considerable importance in thermometer construction. Unsatisfactory glasses show thermal hysteresis of large magnitude.

Weber, as far back as 1883, proved that the best results were obtained with a pure potassium glass containing large percentages of silicon and calcium, and that the presence of both K_2O and Na_2O together was objectionable.

The glass selected by the International Bureau is known as "Verre dur"; it is a lead-free glass, containing about 11 per cent. of the oxide of sodium (Na_2O) and only a trace of K_2O (0·3 to 0·4 per cent.); the chief constituents being silica 72 per cent. and lime 14 per cent. At that time "Verre dur" was probably the best obtainable, but in recent years glasses surpassing "Verre dur" have been introduced, and the better-class thermometers nowadays are made of Jena 16''' glass.

For high-temperature work borosilicate glass 59''' is in general use, since this glass does not soften until quite high temperatures are attained.

Its chemical composition is given in the table below :—

TABLE IX.

Composition of 59''' Glass.

SiO_2	72 per cent.
Al_2O_3	5 ,,
Na_2O	11 ,,
B_2O_3	12 ,,
Mn_2O_3	0·05 ,,

Sometimes K_2O is present to the extent of about $1\frac{1}{2}$ per cent. Such glass is, of course, inferior in properties to one free from both Na_2O and K_2O together.

The zero depressions after heating to 100° C. are quite small.

For "Verre dur" about 0·10°.

Jena 16''' ,, 0·08.

Borosilicate 59''' 0·03.

Although it was originally stipulated that "Verre dur" should be free from lead, this requirement has not always been complied with. Glasses of broken "Verre dur" thermometers analysed at the N. P. L. were found to contain quite appreciable amounts of lead.*

Apart from the difficulty of obtaining glasses of the correct chemical composition, it has been observed that thermometers made out of the same ingot of glass will differ in behaviour due to slight differences of chemical composition in various parts of the ingot and even the working of the bulbs in the blowpipe slightly affects the composition of the glass.

* From 2 to 6 per cent.

Unless the thermometer receives the most thorough annealing, the strains set up during the construction will exert a noticeable influence on the temperature scale obtained.

Fused silica possesses most of the qualities desired in a thermometer envelope, except for the practical difficulty of obtaining capillary with approximately uniform bore.

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CHAPTER III.

THE RESISTANCE THERMOMETER.

The Resistance Thermometer.—The foundation of a method for the measurement of temperature based on the change of resistance of platinum is due to Sir William Siemens, who in 1871 constructed a practical form of pyrometer on this principle. He also devised an ingenious form of resistance bridge, with the object of eliminating uncertainties due to change in the resistance of the leads, consequent on variations in the depths of immersion of the pyrometer stem in the hot region.

The constructional details of the early Siemens pyrometers were unsatisfactory. The platinum wire was wound on a pipeclay cylinder and enclosed in a tube of wrought iron.

A committee of the British Association, appointed in 1872-3 to test these pyrometers, made an unfavourable report on their permanency, and for some years this method of temperature measurement fell into disuse. Prof. A. W. Williamson, chairman of the B.A. committee, suggested that the changes in the resistance of the platinum were due to the reducing atmosphere produced by the highly heated iron casing, which would cause the platinum to combine with a trace of the reduced silicon taken from the pipeclay cylinder.

Analysis proved the truth of this theory and pointed to the desirability of an oxidising or neutral atmosphere around the platinum wire.

Siemens showed that a sheath of platinum eliminated this trouble, and Fig. 14 illustrates his improved type of pyrometer.

His method of calibrating the pyrometer for high temperature work is open to criticism in the light of present-day knowledge.

Up to 350° C. he calibrated it against an (unstudied) mercury thermometer, and at higher temperatures employed a calorimetric method. The relation between the resistance and temperature was expressed by the formula $r = aT^{\frac{1}{2}} + \beta T + \gamma$, where a, β, γ are constants.

Siemens arrived at this general formula from considerations of a mechanical model of the atom, in which he assumed that "the resistance a metallic body offers to the passage of an electric impulse from atom to atom is directly proportional to the velocity of the vibrations which represent its heat."

The work of Callendar in 1887 has already been referred to in Chap. I.

To the joint work of Callendar and Griffiths we owe the modern resistance thermometer and bridge, an instrument unequalled among pyrometric devices for precision and reliability. Callendar introduced nomenclature which has since come into general use.

The platinum temperature $p\,t$ is defined as

$$p\,t = \frac{R_t - R_0}{R_{100} - R_0} \times 100$$

where R_0 is the resistance at 0° C.
R_{100} „ „ 100° C.
R_t „ „ t° C.

The quantity $R_{100} - R_0$ is generally referred to as the "Fundamental Interval" (F.I.) of the thermometer.

He showed that the difference between the true temperature (t), as measured by the air thermometer, and the platinum temperature $p\,t$ was represented by a parabolic formula—

$$t - p\,t \equiv d = \delta\left\{\left(\frac{t}{100}\right)^2 - \frac{t}{100}\right\}$$

where δ is the coefficient for that particular sample of wire and whose numerical value is about 1·5.

The subsequent work of Callendar and Griffiths proved that the parabolic formula, with appropriate values of the coefficients, held generally for the representation of the variation of resistance of platinum with temperature over the range 0° to 600° C.

The type of thermometer finally adopted by them had a platinum coil wound on a mica rack with leads of heavy platinum wire.

A similar pair of wires to the leads, in the form of a loop, were laid alongside. This loop was connected in the opposite arm of the bridge so as to

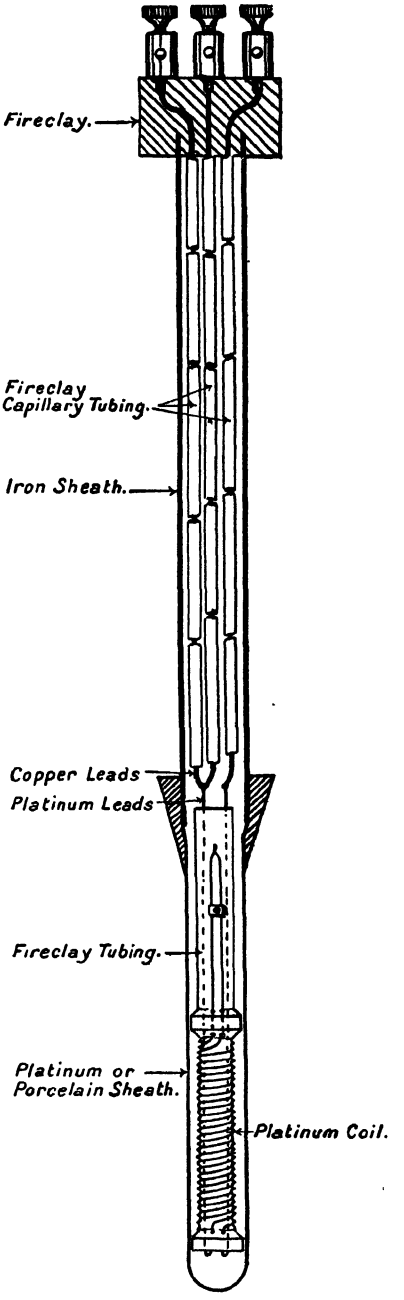


FIG. 14.—Siemens' improved pyrometer.

compensate for the resistance of the leads to the coil at all temperatures.

Fig. 16 illustrates the connections of the bridge.

Extrapolation of the Scale of the Platinum Thermometer for the Determination of High Temperature Melting-points.—The work of Heycock and Neville immediately followed that of their colleagues Callendar and Griffiths, and was primarily directed towards the determination of the freezing-points of metals and their alloys.

To measure temperatures in the vicinity of 1,000° C., it was necessary to extrapolate the parabolic formula over a range of 400° C., since at that time there were no reliable determinations of the melting-points of metals in terms of the gas scale.

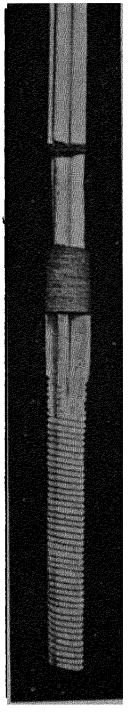


FIG. 15.—Complete platinum resistance thermometer coil.

For example, gold, a metal obtainable in a state of high purity, had, according to Barus, a freezing-point value of 1,093° C. This was determined by means of a platinum *vs.* platinum-iridium couple calibrated in terms of a gas thermometer. Holborn and Wien, at the same time (1892), and employing an almost identical method, obtained the value 1,072° C., a discrepancy of 21°.

Heycock and Neville investigated the freezing-point of gold among those of other metals, and their

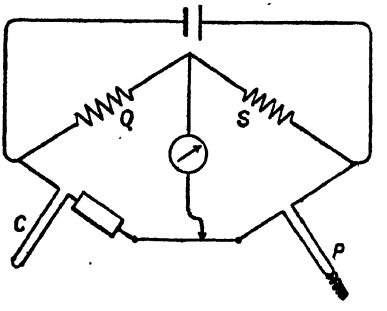


FIG. 16.—Diagram of bridge connections.

Q, S, equal ratio arms. C, compensatory loop, the lower end is joined by fine wire to produce same conducting effect as in the leads to coil. P, platinum coil and leads.

work showed that it gave a sharp well-defined transition point which renders it an excellent "fixed point" for calibration purposes.

Employing thermometers constructed of wire of various degrees of purity and reducing the observations by the parabolic formula, they obtained the values given in Table X.

TABLE X.—Freezing Point of Gold. Purity 99·95 per cent.

Thermometer number.	Platinum, Temperature °C.	δ	$d = t - pt$ °C.	$t°$ C.
13	908·7	1·500	153·2	1,061·9
15	852·9	2·040	208·3	1,061·2
18	900·7	1·574	180·7	1,061·4
13A	903·3	1·553	158·6	1,061·9
14	907·7	1·511	154·3	1,062·0

Weighted mean 1,061·7°

This value for the freezing-point of gold is in close agreement with the recent determination, 1,064° C.

A comparison of the most reliable recent determinations of the freezing-points of the metals, expressed on the gas thermometer scale, with those obtained previously by Heycock and Neville proves conclusively that the resistance thermometer standardised at 0°, 100°, and 444·6° C., will give temperatures identical with the gas scale up to 1,080° C., within the limits of experimental error to which the gas thermometer scale is known.

This is further confirmed by several direct comparisons between the resistance thermometer and the gas thermometer over the same range.

Influence of the Purity of the Platinum.—A fairly accurate idea of the purity of the platinum wire may be formed from a consideration of its coefficients of resistance. The purest specimens give values of α (the mean coefficient between 0° and 100° C.) as high as 0·00389 and δ about 1·50 or slightly less. Impure wire on the other hand may give values of α only 60 per cent. of the above and of δ's up to 1·6.

The parabolic formula has been found to hold rigorously when the purity does not vary far from the first-named values. When a thermometer is constructed of impure wire it is generally found that the zero will not remain constant after exposure to high temperatures and consequently the reliability of the instrument is impaired.

Since only a small quantity of the material is required it is advisable to wind the coil of the purest platinum obtainable. The heavy wire leads may be of commercially pure wire.

For work up to temperatures of 500° C. silver leads are quite satisfactory, provided an intermediate piece of platinum is introduced between the fine wires and the silver, so as to avoid the risk of contamination in the autogenous welding.

Above 600° C. the volatilisation of the silver causes contamination of the platinum coil and also deterioration of the insulation of the mica rack.

Construction of Platinum Thermometers.—Fig. 14 represents the original type of high temperature resistance thermometer.

Fig. 17 illustrates an hermetically sealed type of thermometer designed by Dr. E. H. Griffiths for laboratory work of high precision. By sealing

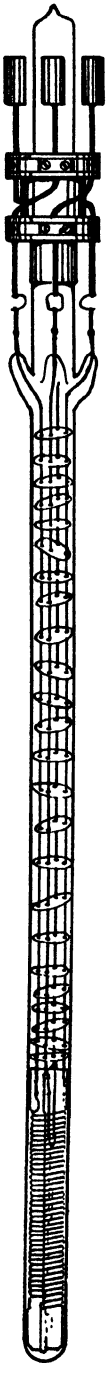


FIG. 17.—Hermetically sealed thermometer for high precision work.

the sheath it is possible to eliminate any possibility of moisture condensing on the mica and impairing the insulation. Insulation troubles are frequent in high resistance thermometers unless precautions are taken to prevent access of moist air.

Other types of heads are shown on the thermometers in Figs. 32 and 34.

Of the various insulating materials hitherto investigated for the high temperature work, good quality mica has proved to be the most satisfactory for thermometer construction.

Exposure to a temperature of about 1,000° C. causes dehydration of the mica, which in consequence becomes silvery white and brittle. If reasonable care is taken it is quite satisfactory in this condition.

Resistance Thermometers for Calorimetric Work.—For calorimetric work it is desirable to have a sensitive thermometer of small lag, so that its indications at any instant are a true measure of the temperature of the liquid.

Thermometers of the type illustrated in Fig. 17 are satisfactory provided the coil is made as light as possible and the sheath of very thin glass.

With the object of reducing the thermometer lag to a minimum, Dickinson and Mueller have developed the type of thermometer illustrated in Figs. 18 and 19.

The mode of construction is described by them as follows :—

Coil.—The coil is of the purest platinum wire 0·1 mm. in diameter, a length of about 2·2 metres being wound in a flat bifilar coil about 8 cms. long and 7 mms. broad, on one end of a mica strip, which is about 18 cms. long and 0·2 mm. thick. The turns of wire are held in place by notches in the sides of the mica strip and are spaced about 14 turns to the centimetre. The coil is insulated from the surrounding sheath by strips of mica somewhat wider and thinner than that on which the coil is wound.

Before winding, the wire is annealed by heating to a high temperature, 1,000° to 1,200° C. by passing an electric current through it. After winding and attaching the leads —*i.e.*, after the coil is so far completed as not to require further handling, it is carefully washed in distilled water to remove all traces of hygroscopic salts, and is then heated to a bright red by means of an electric current to drive off all traces of hygroscopic salts, volatile matter, and to reanneal the wire.

Leads.—The leads are made of thin strips of copper 0·13 mm. thick by 2 to 3 mms. wide. If the thermometer

is of the compensating lead type the compensating loop is closed by a piece of the 0·1 mm. platinum wire about 3 or 4 cms. long. All platinum joints are made by fusing with an arc, using a pure graphite electrode, while the copper platinum joints are made either by welding or with silver, using borax as a flux. The flat copper strips extend to just beyond the mica strips, where they are silver soldered to No. 20 copper wires, which are threaded through glass tubes. If suitable rolls are available, it is preferable to roll down the wires at the ends to take the place of the copper strips.

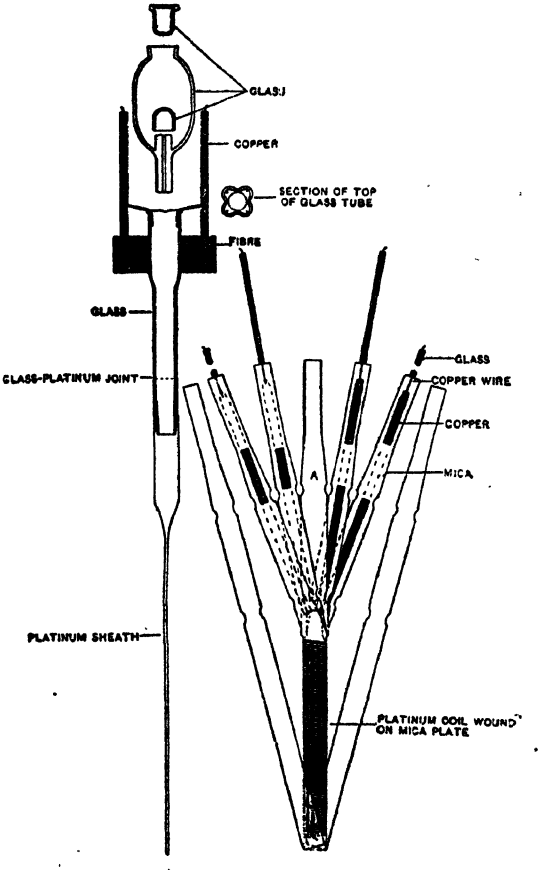


FIG. 18.—Diagrammatic sketch of parts of thermometer, separated to show construction.

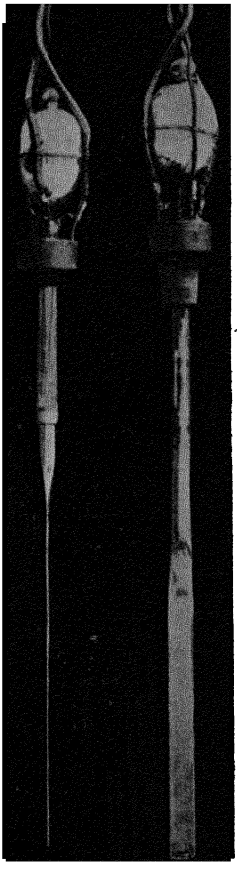


FIG. 19.—Dickinson and Mueller's type of calorimetric resistance thermometer.

Sheath.—The sheaths are made of thin-drawn silver or (preferably) platinum tubes 7 mms. in diameter, 15 to 18 cms. long, and of about 0·12 mm. wall thickness for the platinum and up to 0·2 mm. for the silver. These tubes are partially flattened, as shown in Fig. 19, and after the coil is inserted

are closed at the ends by fusing with an arc, and pressed down on to the coil.

Heads.—The heads are made entirely of glass and consist of four pieces, as shown in Fig. 18—the stem, drying capsule, and two small caps. The stems are usually attached to the metal cases by platinising the glass, which is just large enough to slip into the metal tube, and then soldering the glass and metal together with ordinary soft solder. As this solder melts at about 190° C., thermometers to be used above this temperature have the case made of platinum, which is fused directly to the glass. This method requires a rather large joint between the glass and platinum. The glass must be of special composition and the work carefully done to avoid breaking at this point.

The upper part of this tube is shaped to provide grooves for the lead wires, which are brought out between the tube and the stem of the drying capsule.

The drying capsule is sealed in with Khotinski cement, the wires passing out through this cement.

The drying capsule is about half-filled with asbestos wool, the small inside cap serving to prevent loose particles from dropping into the tube below. The rest of the capsule is filled with phosphorus pentoxide. When the small upper cap is cemented on, the thermometer is kept warm to prevent the internal pressure becoming larger than one atmosphere when the thermometer is subsequently used at the higher temperatures.

Outside Leads.—The coil leads are soldered to pins or small copper tubes held in a fibre collar which is cemented to the glass stem. To these pins or tubes the flexible leads are attached.

These leads should be as nearly as possible alike, both as to length and total resistance.

The copper flexibles must be protected at the soldered joints to prevent sharp bending. This may be accomplished by threading the wires through the copper tubes and making the soldered joint at the lower end.

Test of Insulation Resistance.—The presence of moisture in the thermometer, due to a leak or to exhaustion of the drying material, may occur. The resulting phenomena are very characteristic and easily recognised. If the bridge, with the thermometer in circuit and galvanometer circuit closed and a key in the battery circuit, is balanced by adjusting resistance with the battery key closed, then on opening the battery circuit there will be a large deflection of the galvanometer, which gradually diminishes, and on closing it again another large deflection in the opposite direction. The latter slowly diminishes if the circuit is kept closed. This phenomenon is readily distinguished from that due to the use of an excessive measuring current, by the absence of the galvanometer deflection in the latter case when the battery circuit is opened.

The presence of moisture also reduces the insulation resistance between the coil and sheath. This insulation resistance is easily tested and should exceed 200 megohms.

Resistance Bridges adopted for Thermometric Work.—The requirements of platinum thermometry differ in many respects from those of ordinary resistance comparison work.

Compensation for the resistance of the leads necessitates the use of a bridge with equal ratio arms. Another requirement is that it should be capable of measuring changes in resistance to a high order of accuracy. For example, a thermometer constructed with a resistance coil of 2·56 ohms at 0° will have an increase in resistance of 1 ohm when heated to 100° C. Hence to measure temperatures to $\frac{1}{100}$° demands resistance measurements to $\frac{1}{10000}$th of an ohm.

In practice this presents little difficulty, since balance to the nearest 0·05 is obtained by the set of coils, and final balance obtained by means of a bridge wire or set of shunted coils.

In resistance thermometry we are only concerned with changes of resistance; the absolute value of the unit employed is of little consequence, provided the relative values of the coils are accurately known.

Methods of calibrating the bridge coils and wire are described later.

Types of Resistance Bridges—(*a*) **Siemens' Three-lead Bridge.**—This bridge is primarily of historical interest as representing the first attempt to eliminate lead resistance in platinum thermometry work.

Fig. 20 shows the connections.

The coils Q and S are the equal ratio arms. The thermometer coil P has three leads connected in the manner shown in diagram.

The lead L_2 is adjusted in the construction of the thermometer equal to L_3. When R is adjusted equal to P the bridge is balanced and the lead resistance completely eliminated.

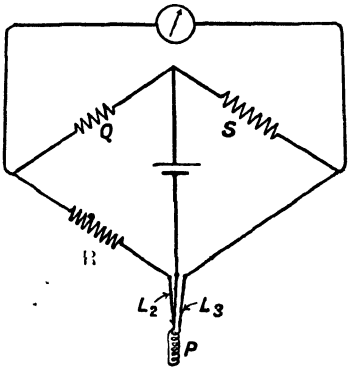


Fig. 20.—Siemens' three-lead bridge. Q and S, ratio arms; P, thermometer coil; L_2 and L_3, equal leads.

The defect of this form of bridge is that a slide wire cannot be used in connection with R to measure minute changes of resistance.

This difficulty can, however, be surmounted by the use of a set of shunt coils of the type described later in connection with shunted coil bridges. One setting would then determine the resistance and hence the temperature.

Siemens' procedure was to shunt one of the ratio arms and calibrate empirically.

(*b*) **The Callendar and Griffiths Bridge.**—The connections on this bridge are shown in Fig. 16, p. 32. It was evolved for use with the compensating leads type of thermometer.

In a later type of bridge manufactured by the Cambridge Instrument Co., mercury contacts of the form shown in Fig. 21 replace the usual plugs.

The ends of the coil are soldered to brass posts terminating in mercury cups. A ∩-shaped bar is carried by a light spring, which is depressed when the weighted plug D is inserted into the hole G.

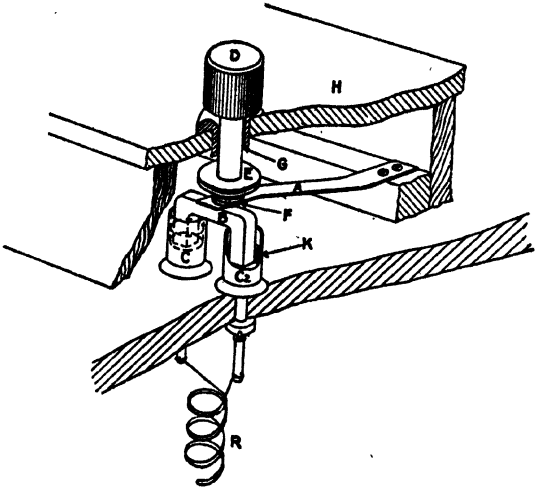


FIG. 21.—Collins' mercury contact.

A, spring; B, ∩-shaped bar (copper link); C and C_2, mercury cups; D, weighted plug; E, spring-plate; F, helical spring; G, opening; H, bridge top; K, mercury; R, coil.

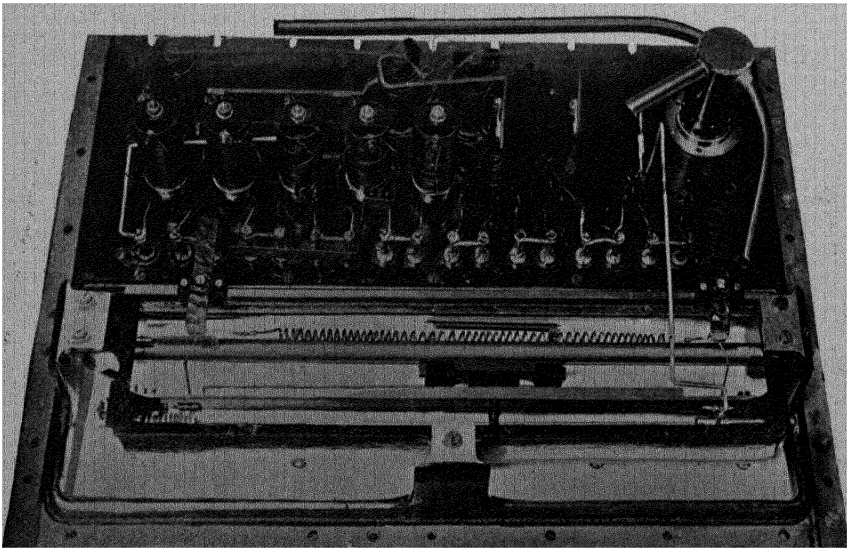


FIG. 21A.—View of underside of resistance thermometer bridge (oil-immersed type), showing construction of the coils and oil circulator.

Fig. 21A shows the form of coil construction employed in a modern resistance bridge.

The coils are of manganin and immersed in well-stirred oil—a good grade of paraffin oil is quite satisfactory for this purpose.

Manganin has an extremely small temperature coefficient of resistance, and also a very small thermal E.M.F. against copper, in this respect affording a marked contrast to constantan or eureka, which has an E.M.F. of about 40 microvolts per degree against copper.

Manganin is, however, subject to gradual changes of resistance and consequently the coils require calibration from time to time.

Recent experiments by Rosa and by Smith have shown that the shellac varnish coating of resistance coils absorbs moisture and in the accompanying change of volume strains are set up in the wire. To eliminate this effect

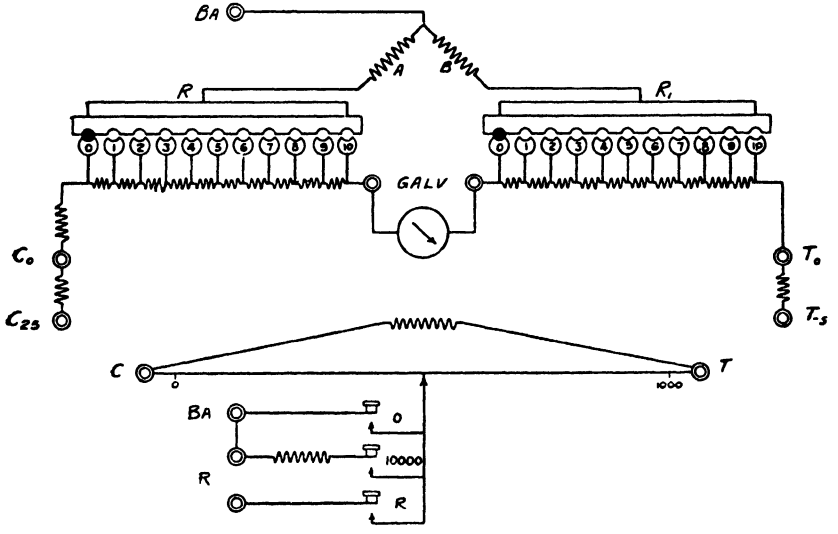


FIG. 22.—Calorimetric resistance bridge.

A and B ratio arms, ...	200 ohms each.
R ten coils, ...	1 ohm each.
R_1 „	0·1 „

of humidity, present-day standard coils are hermetically sealed, using moisture-free paraffin. This mode of construction might well be applied to the coils of reistance bridges.

The bridge wire is of manganin, and both it and the contact maker are immersed in the oil.

Calorimetric Bridge.—Messrs. Dickinson and Mueller have arranged the equal arm bridge * in a convenient form for calorimetric work. The wiring

* Manufactured by the Northrup Company.

diagram is shown in Fig. 22; it will be observed that, while the balance of such a bridge is adjustable at three points, the contact resistance at these three points are so placed as to have a minimum effect upon the accuracy of the bridge.

The slide wire contact is in series with the battery. The contacts of the rheostats R and R_1 are each in series with a ratio coil of 200 ohms or over, where, even though considerable contact resistance were present, the percentage effect would be small. This arrangement of the Wheatstone Bridge also has the advantage of maintaining an almost constant resistance at the terminals of the galvanometer for all bridge settings, thus maintaining both constant damping conditions and deflections proportional to the want of balance for all bridge settings.

The rheostat R provides for the adjustment of the bridge by coarse steps, and the rheostat R_1 by fine steps, while the total continuous slide wire is properly proportioned to be equivalent in its total to one step on R_1 with suitable overlap. The slide wire consists of eleven turns of manganin wire, wound spirally on a marble cylinder, providing in effect a continuous scale 240 inches long. Ten turns of the slide wire are equivalent to one step of the rheostat R_1. One-half of the additional turn is located at the high end and the other at the low end of the scale, thus providing the overlap for steps on R_1. One turn of the slide wire is equivalent to ·01 ohm or approximately ·1° C. in a thermometer whose R_0 is approximately 25·3 ohms. As there are 200 divisions in each turn, $\frac{1}{5}$ of one division (equal to a distance of $\frac{1}{50}$ inch) is approximately equivalent to ·0001° C. The rheostat R_1 is composed of ten ·1-ohm coils, and hence covers a range of approximately 10° C. by steps of 1° C. The rheostat R is composed of ten 1-ohm coils, thus covering a range of 100° C. An additional ·5 ohm resistance, whose principal function is described below, extends the range an additional 5° C., thus making the over-all range 115° C. The coils of the rheostat R_1 must be adjusted to an accuracy of ·00001 ohm, this being equivalent to ·0001° C. in the resistance thermometer, hence the plug of this decade may be shifted during a test. On the other hand, the coils of the rheostat R are each 1 ohm. To adjust these to an accuracy of ·00001 ohm would be useless, since the manganin will not remain constant to $\frac{1}{1000}$ per cent., which would be the accuracy of such an adjustment. Hence, the plug of the rheostat R should not be disturbed during any one test. To guard against the necessity of disturbing R, a ·5 ohm resistance, which may be included in the circuit at will, is connected in series with the rheostat R_1, between the posts T_0 and T_5. If the initial temperature of a test requires a setting in the upper half of the rheostat R_1 with the thermometer lead connected, a rise of temperature during the test might readily require the plug R to be moved in order to maintain balance. To avoid this, the thermometer lead may be connected at T_5 ohm at the beginning of the test, so that the balance point will be in the lower half of the rheostat R_1, and a subsequent rise of 5° C. may be measured without touching R.

(*c*) **Potentiometer Method of Measuring Resistance.**—The well-known

potentiometer method of determining resistances, by comparison with a standard, has been applied to resistance thermometry.

The thermometer coil has four leads: two current and two potential; the current from a steady battery is passed through a standard oil immersed resistance coil and the thermometer coil in series. By measuring the fall of potential across the two coils separately, the resistances may be calculated in the usual manner.

(*d*) **Smith's Difference Bridge.**—In this form of bridge the connections are so arranged that, by two observations and a reversal of connections, the resistance of the leads is eliminated without requiring absolute equality of lead resistance.

Fig. 23 shows the disposition of the bridge connections for the first balance position. P is the thermometer coil with current leads L_1 and L_4 and potential leads L_2 and L_3.

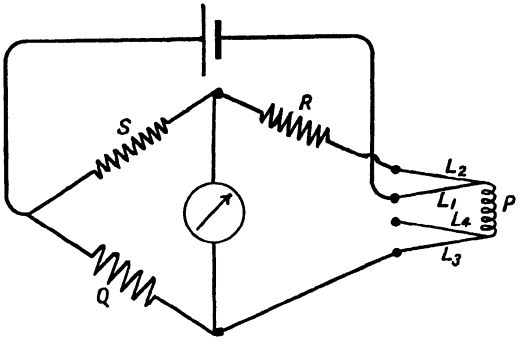


FIG. 23.—Smith's difference bridge.

P, thermometer coil; L_1, current lead; L_2, potential lead; L_3, potential lead; L_4, current lead; R, adjustable arm of bridge; S and Q, equal ratio arms; ●, mercury cup contacts.

Q and S are equal or nearly equal ratio arms, and R is the adjustable arm of the bridge.

When balance is obtained, then

$$P + L_3 = \frac{Q}{S}(R + L_2).$$

The connections are then transposed by a mercury switch, so that the potential lead L_2 is disconnected from R and joined to S; L_3 to R; the battery lead from L_1 to L_4; and P and R are interchanged.*

Fig. 24 now represents the connections.

On rebalancing

$$P + L_2 = \frac{S}{Q}(R' + L_3).$$

* The object of interchanging P and R is to avoid the product of the ratio of R to S by the sum of the two values of R entering into the final equation for P.

Now Q has been adjusted during the construction of the bridge to be very nearly equal to S, so that we can put

$$\frac{Q}{S} = (1 + a)$$

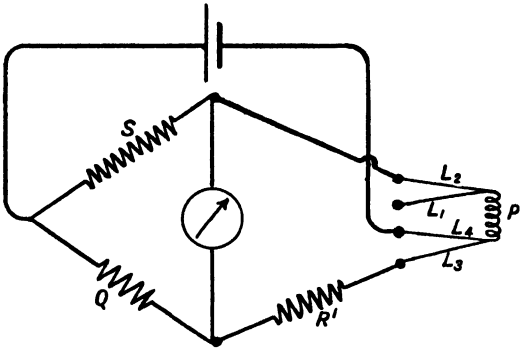


FIG. 24.

where a is a small quantity. Then

$$P = \frac{R + R'}{2} - \frac{a}{2}\{a(R + L_2) + (L_2 - L_3).$$

If Q = S within 2 parts in 10,000, then $a = 0{\cdot}0002$. So that P is equal to $\frac{R + R'}{2}$ within 2 parts in 100 millions, assuming $L_2 = L_3$. If L_2 and L_3 each have a resistance of 0·1 ohm, but differ by 10 per cent., then the error introduced by neglecting a and taking the equation $P = \frac{R + R'}{2}$ as exact is equivalent to about 0·0001° C. on a thermometer with F.I. of 1 ohm.

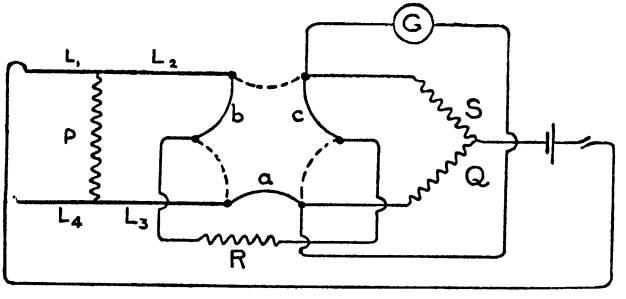


FIG. 25.—Connections to six-pole mercury contact switch.

L_1, L_2, L_3, L_4, leads to the thermometer coil; Q and S, ratio arms; R, variable arm of bridge; P, thermometer coil; a, b, c, heavy copper links dipping into mercury cups.

The reversals which have been indicated above are conveniently made by means of a six-pole mercury contact-switch with connection as shown in Fig. 25. Thick copper links, *a*, *b*, and *c*, are attached to an ebonite disc movable on a vertical axis. The change over is effected by lifting clear of the mercury cups, rotating through 90°, and then lowering. The second position of the links is shown dotted in Fig. 25. It is, of course, easy to arrange for the change in position of the battery lead to be made simultaneously by contacts attached to the same disc.

This bridge method possesses one unique advantage, insomuch that it eliminates lead resistance without assuming absolute equality in their resistance. On the other hand, it suffers under the disadvantage of requiring two settings for each resistance reading, and that six contacts have to be broken and made; the contact resistances being assumed unchanged.

If the leads are made very nearly equal, R and R^1 will only differ by an extremely small amount. This increases both the speed of working and the accuracy, since the above equation assumes reasonable identity in L_2 and L_3.

Hence the bridge is primarily of value when working at steady temperatures.

It will be observed that a bridge wire cannot be employed. Small changes of resistance can, however, be obtained by means of shunted coils. The principle of this method is illustrated by Fig. 26.

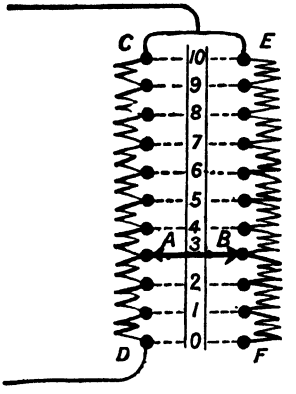


FIG. 26.—Diagram of shunted coils (Smith system).

A B, movable cross-bar; C D, coils of 0·1 ohm each; E F, shunt coils (9·9 ohms each).

The ten coils C D each of 0·1 ohm are in series; any number of the coils E F can be placed as a shunt across the corresponding number of coils in C D by moving the bar A B.

Consider the bar in the position marked 0. We have then ten 0·1 ohm coils shunted by ten coils of 9·9 ohms each. So the effective resistance is

$$\frac{1}{X} = \frac{1}{1} + \frac{1}{99}$$

Hence $X = 0{\cdot}990$

Suppose now the bar A B is moved to position marked 1.

We have now one coil of 0·1 ohm in series with nine coils of 0·1 ohm shunted by nine coils of 9·9 ohms.

Hence, if Y is the effective resistance of the shunted portion,

$$\frac{1}{Y} = \frac{1}{0{\cdot}9} + \frac{1}{89{\cdot}1}$$

$$Y = 0{\cdot}891$$

So that the total resistance is $0{\cdot}1 + 0{\cdot}891 = 0{\cdot}991$. Hence moving the bar one step has increased the resistance by 0·001 ohm.

Similarly it can be shown that each step has a corresponding effect, so that the arrangement is capable of giving a total increase of 0·01 ohm distributed over ten steps.

It is obvious that the studs could be distributed on a circle, so the movement of A B would be one of rotation about its centre.

Fig. 27 illustrates the R arm of a bridge constructed on this principle. Coils of 0·01 ohm and upwards (apart from the dials) have mercury contacts bridged by ∩-shaped pieces of copper (Fig. 28).

The three dials are employed to produce the small changes of resistance.

The contact-brushes enable one or more of the lower resistance coils each to be shunted by the higher resistance ones, the shunting producing a diminution of the total resistance. (As will be explained later, in constant-current bridges the arm R is decreased in resistance with increase in resistance of the platinum thermometer : p. 49.)

This device of shunted coils does not involve any great accuracy in the adjustment of the coil values.

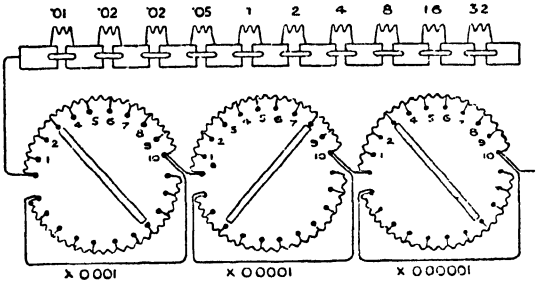


Fig. 27.—Diagram of R arm of bridge.

The resistance coils in the three dials are as follows :—

For the 0·001 dial ten resistances of 0·1 ohm each and ten of 9·9 ohms each.
" 0·0001 " " 0·05 " " 24·95 "
" 0·00001 " " 0·01 " " 9·99 "

For instance, consider the 0·001 ohm dial. Nominally the coils composing this dial are exactly 0·1 ohm and 9·9 ohms. If, however, the coils are badly adjusted so that, instead of a resistance coil being 9·9 ohms, it is 9·95 ohms, the change when this coil is used as a shunt resistance would be 5 millionths of an ohm less than 0·001.

The bridge can be calibrated in the manner described later, so that even if the coils are badly adjusted corrections can be applied to the readings.

(*e*) **Mueller's Bridge.**—A different arrangement of bridge with shunt coils has been described by Mueller. In Fig. 29 the connections of the complete bridge are shown.

The two ratio coils are 250 ohms each, and these are connected by a short slide wire which is used in adjusting them to equality.

The ratio coils terminate in long bars which may be connected, by means of plugs, to the contact blocks of the 1 ohm and 0·1 ohm decades.

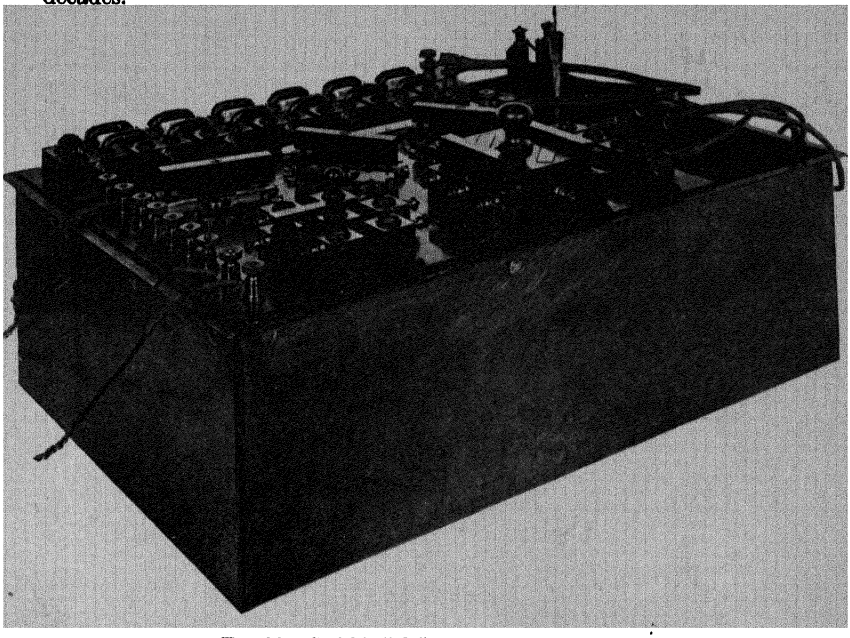


FIG. 28.—Smith's " difference " bridge (oil immersed).

In series with the shunting decades there is a set of ten 10-ohm coils, $C_0 - C_{10}$. These are introduced into the circuit by plugs or mercury contacts.

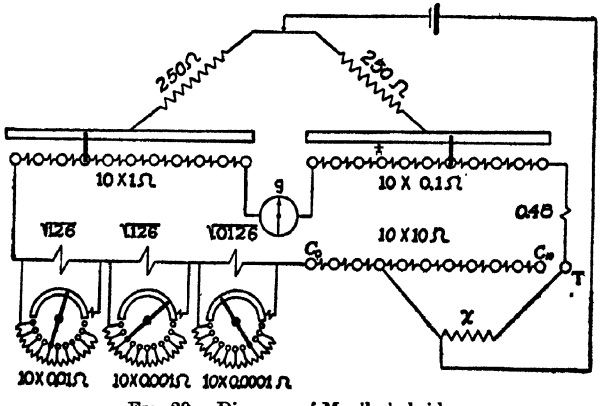


FIG. 29.—Diagram of Mueller's bridge.

Three shunted decades are employed giving 0·01, 0·001, and 0·0001 ohm per step respectively.

In choosing the values for the shunted coils the formula for resistance of coils in parallel was put in the following form : if a resistance r is shunted by a resistance R the effect of the shunt is to reduce r by an amount $\frac{r_2}{R+r}$. In the shunt decades (for example, the 0·01-ohm decade) R is given a series of values such that $\frac{r_2}{R+r}$ successively assumes the values 0·10, 0·09, 0·08 . . . 0·00; that is, successive values of R are defined by the equations $R+r=\frac{r_2}{0\cdot10}$, etc., to $R+\frac{r_2}{0\cdot00}$. Consequently, to secure even-valued coils, a value was sought for r_2 which should contain the factors 7 and 9, and, therefore, be divisible by all numbers below 10. The value $r_2 = 1\cdot26$ was found to lead to suitable values for the coils of the 0·01-ohm decade.

By making r_2 for the 0·001-ohm decade equal to $r/\sqrt{10}$ the successive values of R for this decade are made to differ by a constant amount from the values of R for the 0·01-ohm decade, so that the corresponding coils for the two decades, with two exceptions, will be equal.

The values of the shunted and shunting coils for the three decades are given in Table XI.

TABLE XI.

Position of switch.	0·01 ohm decade. Shunted coil, $\sqrt{1\cdot26}=1\cdot1225$.	0·001 ohm decade. Shunted coil, $\sqrt{0\ 126}=0\ 3550$.	0·0001 ohm decade Shunted coil, $\sqrt{0\cdot0126}=0\cdot1122$.
	Individual coils	Individual coils.	Individual coils.
0	11·478	12·245	12·49
1	1·4	1·4	1·4
2	1·75	1·75	1·75
3	2·25	2·25	2·25
4	3·0	3·0	3·0
5	4·2	4·2	4·2
6	6·3	6·3	6·3
7	10·5	10·5	10·5
8	21·0	21·0	21·0
9	63·0	63·0	63·0
10	∞	∞	∞

A plan of the top of a bridge of this type is shown in Fig. 30. It differs from that shown in Fig. 29 insomuch that switches are employed instead of plugs in the 1-ohm and 0·1-ohm decades. The 10-ohm decade is shown on the right-hand side, and connection to it can be made either by plug or through binding posts. Mercury contacts would be preferable to the plug contacts.

An arrangement is provided for interchanging the ratio coils so that these may be adjusted to equality by means of the slide wire.

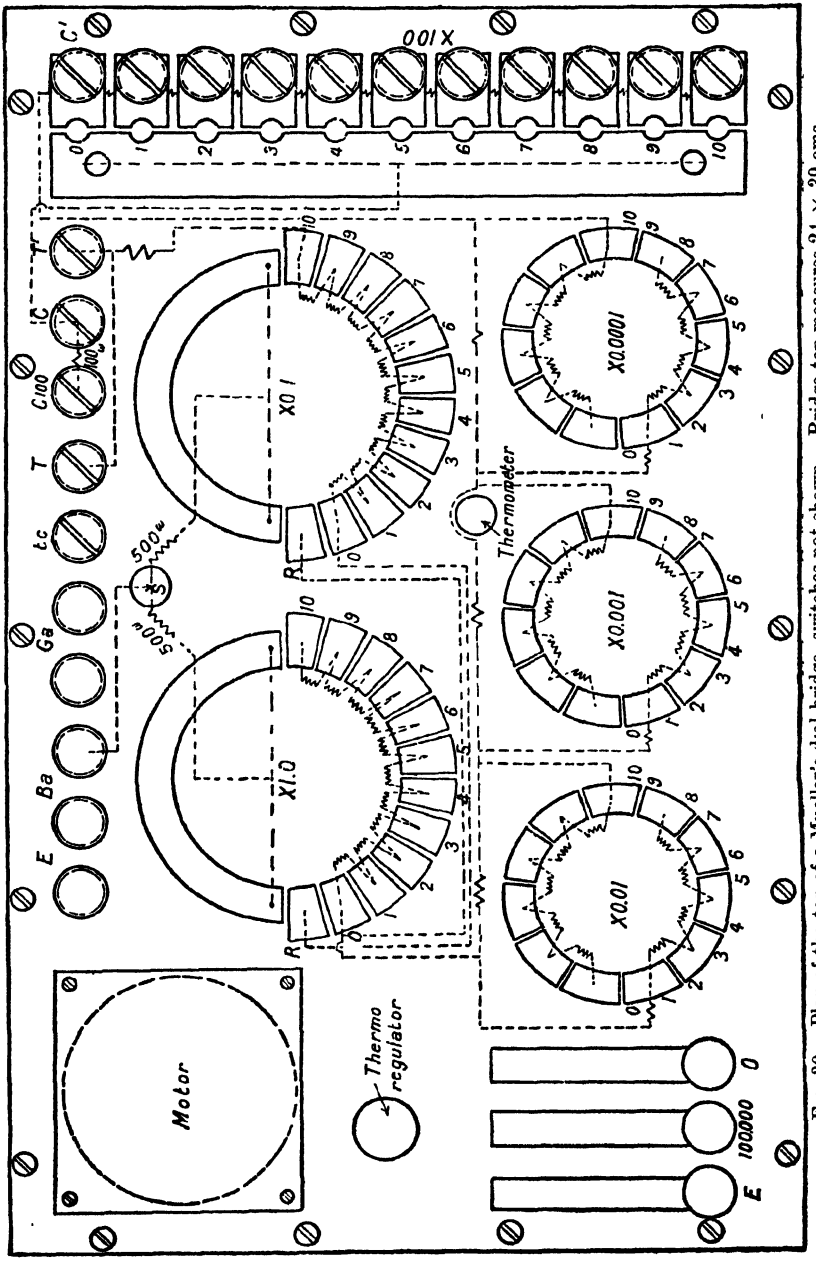


FIG. 30.—Plan of the top of a Mueller's dial bridge, switches not shown. Bridge top measures 24 × 39 cms.

This adjustment may be made as follows :—By connecting the post marked T′ with one of the C′ posts—for example, C′ 40, and connecting *t c* to C′ 20—the first two of the 10-ohm coils may be balanced against the second two.

Then, on shifting the switches of the 1-ohm and 0·1-ohm decades from the zero positions to R, the ratio coils are interchanged and the bridge balance will be disturbed unless the two are equal. If the coils are not equal, adjustment may be made by means of the slide wire until no change in balance is noted on interchanging the ratio coils. A special stop with a release ordinarily prevents moving the switches to the position R.

The three keys are connected in the battery circuit and so arranged that the key E closes the circuit through an external resistance connected between the key posts marked E ; the 100,000 key closes the circuit through 100,000 ohms, and the 0 key through no added resistance.

Temperature Control.—While, in work of the highest precision, it is necessary to control the temperature of the bridge coils within narrow limits, a fair degree of accuracy may be obtained by applying temperature corrections to the coil values. With manganin coils of good quality measurements can be made to about 1 part in 25,000, if the coil temperatures are known within 1° or 2°, and the indications of a mercury thermometer with its bulb near the coils should give the coil temperatures within this limit.

For greater accuracy the bridge must be mounted in an oil bath and thermostatic control employed. In the bridge shown in Fig. 30 the motor for circulating the oil is mounted on the bridge cover with its axis vertical, and drives a screw propeller working in a vertical tube, which also contains a heating coil. The oil is circulated through the tube, along the bottom of the box under a false bottom, thence upward and past the coils, and through the tube again.

A liquid-in-glass thermo-regulator is mounted on the lower side of the false bottom.

A copper coil, similar to the sealed coils used for the 10-ohm and 1-ohm decades, mounted in the bridge and arranged so that its resistance could be measured with the bridge, showed that in such coils the fluctuations in the temperature of the oil, as the regulator operated, were almost completely damped out.

Heating Effect of the Current passing through the Thermometer Coil.—In order that the thermometer bulb may be of small dimensions and the thermometric lag reduced to a minimum, the coil must be made of wire of about 6 mils. in diameter, consequently the heating effect of the measuring current on the value of the resistance is quite appreciable. The bridge coils are sufficiently heavy and well cooled to make the effect on them negligible, hence the limiting value of the current is determined solely by considerations of the thermometer coil.

At any given temperature the increase in resistance is proportional to the square of the current.

The same expenditure of watts at different temperatures does not,

however, produce the same heating effect, since the rate of cooling of a surface by convection and radiation is a function of its absolute temperature.

The precise laws governing the phenomenon have not yet been investigated, and it is only possible to approximate to a constant heating effect for all temperatures by keeping the *current* through the thermometer constant.

Callendar states: "The cooling effect of conduction and convection currents in air in the thermometer tube increases nearly in proportion to the absolute temperature. The effect of radiation also becomes important at high temperatures, and the cooling is then more rapid. If, therefore, the watts are kept constant, the heating effect will diminish as the temperature rises, and a small systematic error will be produced. Assuming that the rate of cooling increases as the absolute temperature θ, and that the watts are kept constant, the heating effect at any temperature θ is $273h/\theta$, where h is the heating effect in degrees of temperature at 0° C."

This train of reasoning led Callendar to conclude that a better rule is to keep the *current* through the thermometer the same at all temperatures, as in that case the heating effect also is nearly constant, if the current flows sufficiently long for the steady state to be attained.

The table below shows the heating effect of the measuring current on two thermometers, using a current of 0·1 amp.—a current ten times larger than that customary in precision work.

TABLE XII.

Temp. °C.	Increment of temperature above surroundings.	
	Diam. wire ·15 mm. (Waidner & Burgess).	Diam. wire ·15 mm. (F. E. Smith)
0	1·65°	1·62°
100	1·69°	1·68°
444·5	1·20°	1·85°

Hence, for the usual value of current ·01 amp. the rise would be ·016°, ·017° at 0° and 100° respectively. The divergence in the values for 444·5° C. has not been explained.

The above values are, of course, only strictly applicable to the particular thermometer investigated.

To eliminate the effect, the following rule has been proposed by Callendar:—"Take away one-third the difference in reading when the battery consists of two secondary cells in series and in parallel from the reading when in parallel."

Modification of a Bridge to obtain Constant Current through the Thermometer.—To satisfy the condition of constant current through the

thermometer at all temperatures it is necessary either to vary the resistance in series with the battery according to a calculated table or arrange the bridge so that the resistance of each arm remains constant.

To effect this it is only necessary to make the value of the arm R a fixed value greater than the maximum ever attained by the thermometer coil, and then insert a variable resistance (plugs and dials) in series with the thermometer to form the other arm of the bridge. Under these conditions an increase in resistance of the thermometer coil is counterbalanced by a decrease in the variable resistance. In such a case the arm R may be composed of simply one coil of the required value. Reference to Fig. 27 will show the dials arranged to work with this system.

Determination of the Bridge Centre.—In thermometers of the compensated lead type it is necessary to determine the bridge centre from time to time, as this is the base point from which the resistance is measured. For this purpose P_1, P_2 and C_1, C_2 ends of the leads should be short-circuited at the thermometer head. Any change with time in the resistance of the flexible leads can thus be detected. It is scarcely necessary to point out that the leads from the bridge to the thermometer should be approximately equal in resistance and the junctions well made. The writer has found flexibles of the material known commercially as Dynamo flexible (5 amps.) to be quite satisfactory. It is composed of about 66 strands of 0·25 mm. diameter copper wire insulated by a double cotton covering, double india-rubber, proof taped and braided.

Elimination of Thermoelectric Effects.—One of the troubles of precision resistance measurements is the thermoelectric effect in the circuits, particularly under conditions where there are big temperature gradients in the thermometer head. The magnitude of the effect is readily seen by closing the galvanometer key with the battery circuit left open. The galvanometer spot under the circumstances will generally take up a new position, and the movement is a measure of the thermoelectric effects in the system.

It is the practice, therefore, to work with the galvanometer circuit always completed and observe the deflection when the battery circuit is made or reversed.

The method of battery reversal is to be preferred, for then the initial drift of the galvanometer spot, due to the heating effect of the current when the battery circuit is first completed, is eliminated.

To eliminate induction effect Dr. E. H. Griffiths devised a thermoelectric key. In this key there is a series of spring tongues so arranged that the galvanometer circuit is always made. When the key is depressed, the galvanometer circuit is broken momentarily, the battery circuit completed, and then the galvanometer circuit remade. By this sequence the galvanometer circuit is open during the period the current is growing in the circuit, and consequently there is no inductive kick of the light spot. It is easy to arrange a battery reversal key on the same principle.

The various junctions and connections in the keys are a frequent source of thermal E.M.F., so it is advisable to box in thoroughly the entire key

including the terminals; some observers have even found it desirable to immerse the key in oil with only the handle projecting.

With the non-inductive windings of the resistance coils now used the induction effect is usually negligibly small, and it is sufficient to have a plain battery reversal key with an " off " position.

Calibration of Box Coils and Bridge Wire.—For platinum thermometry work the relative values only of the coils and bridge wire are of importance. The method of calibration is closely analogous to that employed for the standardisation of a set of weights.

Instead of a thermometer a variable rheostat is connected to the P_1, P_2 terminals of the bridge. This resistance must be capable of fine adjustment; a convenient type which can readily be constructed is shown in Fig. 31. It consists of four dials of 10 coils each, the coil values being 0·1 ohm, 1 ohm, 10 ohms, and 100 ohms respectively. A trough of mercury with a ∩-shaped piece of copper permits of fine adjustments.

The method of construction is readily understood from the diagram. Each coil terminates in mercury cups, so that a movement of the bar cuts out any number. The coils, of course, need not be accurately known.

As an alternative, ordinary P.O. resistance boxes may be used, one box forming a shunt on the other.

This method of successive shunts is, however, rather laborious.

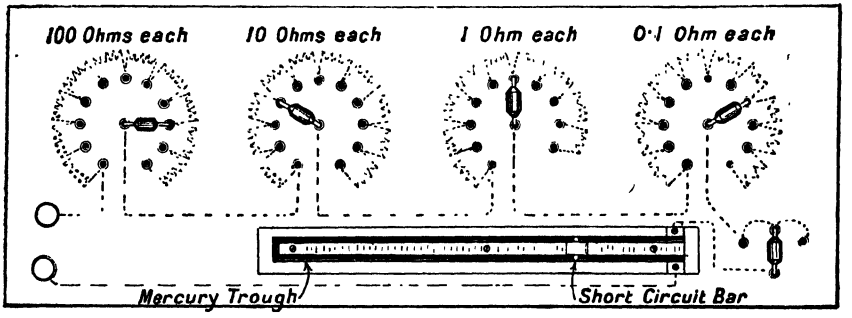


FIG. 31.—Diagram of rheostat employed in calibration of box coils and bridge wire.

(*a*) *Calibration of the Bridge Wire.*—To the terminals C, C of the bridge is connected a short length of resistance wire terminating in two massive pieces of copper, which are drilled to contain mercury cups. Then by the insertion of a ∩-shaped piece of copper the resistance wire can be short-circuited without interfering with its connections to the bridge.

The resistance of the wire should be about 1 unit of the bridge wire.

The variable rheostat is adjusted to bring the contact maker to one end of the bridge wire; to effect this it will generally be necessary to withdraw a plug from the box.

The bridge is balanced in the usual manner. The calibrator coil (connected to C, C) is then short-circuited and balance again obtained at a distance about 1 unit away on the bridge wire. The operation should be repeated a few times.

The rheostat is readjusted so that a new position if taken up on the bridge wire adjacent to the second balancing point and the operation repeated. By a series of such steps the entire length of the bridge wire may be covered.

If we suppose r to be the resistance of the calibrator coil and l_1, l_2 the lengths of wire corresponding to it at various points, then

$$\frac{1}{l_1} \propto r, \text{ etc.}$$

Hence, by plotting graphically the reciprocals of l_1, l_2, etc., as ordinates with the mean bridge wire reading as abscissæ, a curve can be obtained representing the variation in resistance per unit length along the bridge wire.

The values can be converted into those of the "mean box unit" referred to below, by obtaining the resistance of a length of the bridge wire in terms of one of the box coils by the usual substitution method.

(*b*) *Calibration of the Box Coils.*—For convenience it is assumed that the coils are arranged on the binary system, and that the nominal values are 5, 10, 20, 40, 80, etc. . . .

Balance is obtained at any convenient place on the bridge wire by adjustment of the variable rheostat; plug 5 is then withdrawn and the change of bridge wire reading to restore balance observed. The rheostat is readjusted to bring the balance point back to approximately the same position as when plug 5 was in; plug 10 is then withdrawn; plug 5 inserted, and the change in bridge wire reading observed as before.

The same procedure is followed until the difference between the highest coil in the bridge and the sum of the series below is obtained in terms of a length of the bridge wire.

Let the successive differences in bridge wire readings be $x_1, x_2, \ldots x_9$.

Supposing coil 1,280 to be the highest in the set.

Then we obtain the following series of quotations:—

$$\text{Coil } 1{,}280 - (\text{coils } 640 \text{ to } 5) = x_9$$
$$\text{Coil } 640 - (\text{coils } 320 \text{ to } 5) = x_8$$
$$\text{Coil } 320 - (\text{coils } 160 \text{ to } 5) = x_7, \text{ etc.}$$

By subtraction—

$$\text{Coil } 1{,}280 - 2 \times \text{coil } 640 = x_9 - x_8$$
$$\text{Coil } 640 - 2 \times \text{coil } 320 = x_8 - x_7$$
$$\ldots \quad \ldots \quad \ldots \quad \ldots \quad \ldots$$

to $$\text{Coil } 10 - 2 \times \text{coil } 5 = x_2 - x_1.$$

Now, the values of $x_1, x_2, \ldots$ etc., in terms of coil 5 are already known from the previous operations in connection with the bridge wire calibration.

Hence the values of coils 640 to 10 in terms of coil 5 may be found.

Knowing the values of all the coils in terms of coil 5, it is then easy to express them all in terms of the mean coil, and hence in terms of the mean box unit, a corresponding correction being made in the integrations of the bridge wire.

It is preferable, however, to express the coils in terms of the international ohm, and this, of course, can be done by ascertaining the resistance of a standard coil, say 10 ohms, on the bridge.

By expressing the coils in terms of an absolute standard it is possible to keep note of the variations with time in the coils.

The same procedure is followed in the calibration of a bridge fitted with a set of shunted coils instead of a bridge wire. For the shunted coil dials the changes of the shunted coils are of far less importance, and there is little difficulty in adjusting them to the required degree of accuracy.

They possess the advantage of not being subjected to wear, as is the case with a bridge wire.

Standardisation of a Resistance Thermometer.—For temperatures up to 600° a platinum resistance thermometer is generally standardised at the temperature of melting ice (0° C.), of the vapour of water boiling under normal pressure (100° C.), and of the vapour of sulphur boiling under normal pressure (444·5° C.).

For the ice-point the thermometer should be well immersed in finely crushed ice moistened with water; a suitable form of apparatus is shown in Fig. 8, p. 21). Unless the thermometer has been carefully sealed or provided with a drying tube to prevent access of moist air, prolonged exposure to the low temperature will cause electrical leakage owing to the deposition of moisture on the mica.

The steam-point is determined in a standard form of hypsometer such as that shown in Fig. 32. It is advisable to take precautions to prevent

escape of steam rising around the head of the thermometer, as the thermal effects produced are apt to be troublesome.

Alternate readings of the barometer and bridge should be taken and correction made if necessary for the difference in level of the mercury cistern of the barometer and the hypsometer, if the difference in level be considerable.

The sulphur-point can be determined in the standard Meyer tube form of apparatus introduced by Callendar and Griffiths and shown in Fig. 33.

With the Meyer tube apparatus it is necessary to fit the thermometer with an asbestos or aluminium cone as shown in Fig. 33. This cone serves

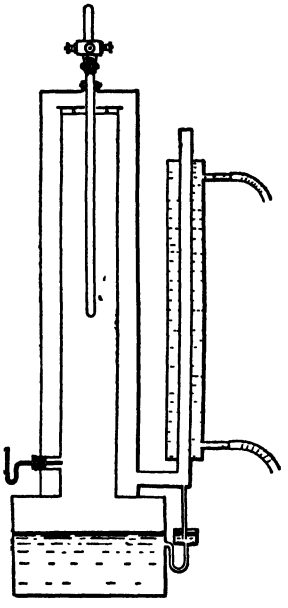


FIG. 32.—Standard hypsometer for determination of steam-point.

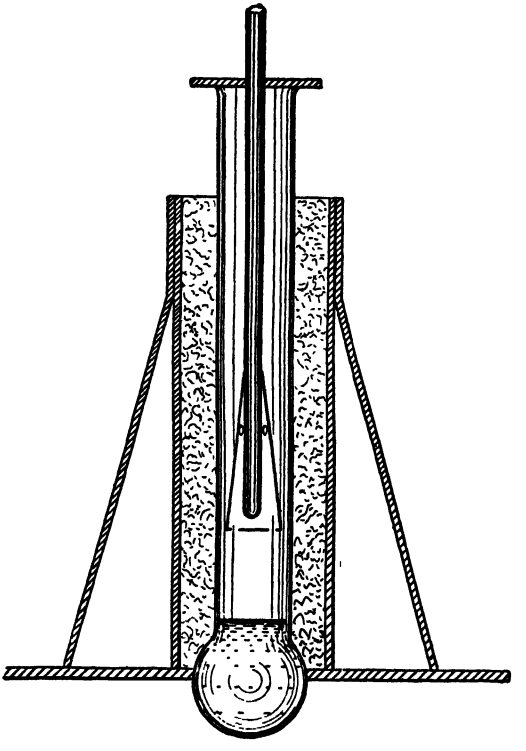


FIG. 33.—Standard Meyer tube apparatus for the determination of the sulphur-point (Callendar and Griffiths).

two purposes: (1) It prevents the condensed sulphur from running down over the bulb and cooling it below the temperature of the surrounding vapour; and (2) it eliminates direct radiation from the bulb to the colder walls of the large tube.

Callendar and Griffiths in 1890 made a careful investigation of these effects; the error due to the first cause was found to be about 0·28°, while

that due to the second cause amounted to 0·49°; consequently an unprotected thermometer would read nearly a degree low in sulphur.

Recently a special study of the type of radiation shield to be employed around the thermometer has been made by Mueller and Burgess.

The various forms of shields investigated are shown in Fig. 35. It was

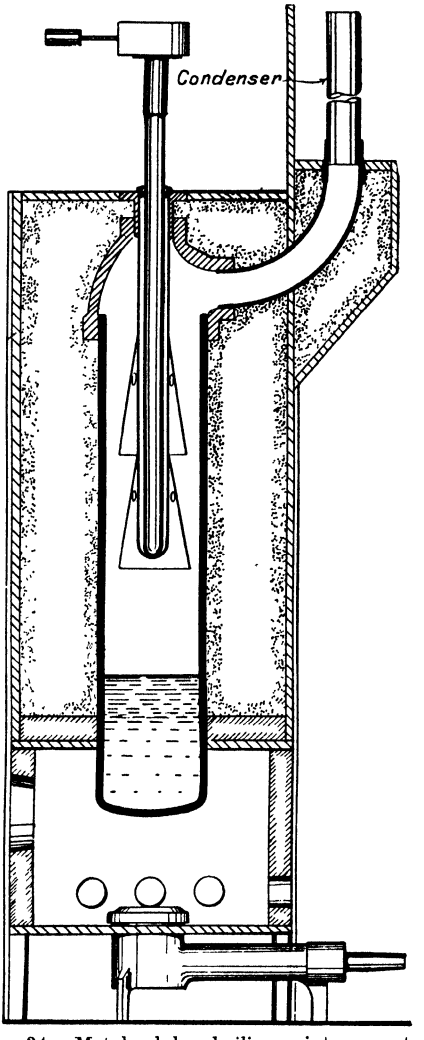


FIG. 34.—Metal sulphur boiling-point apparatus.

noted that the iron shields, either with or without the lower disc, gave practically the same value for the temperature. It was, however, found that when a polished shield of the simple cone type was used the readings were ·2° low with a glass thermometer, and ·02° low with a porcelain enclosed

thermometer. This effect was first observed by Meissner, and shown to be dependent upon the reflecting power of the interior of the shield. When the aluminium cylinder type was employed with the walls sharply corrugated to form a series of wedges, which is, therefore, a good radiator, it was found to be as effective as the other shields. Inadequate shielding is also usually accompanied by considerable variations in temperature, sometimes amounting to 0·1°, when the thermometer is displaced vertically, but the absence of such variation is not necessarily proof of adequate shielding. Nor does it prove that there is no superheating of the vapour, as in one instance constant temperatures were observed with a displacement of 4 cms. where, owing to insufficient depth of liquid sulphur in the tube, the vapour was superheated about 0·5°.

From their investigation Mueller and Burgess came to the conclusion that a simple sheet-iron cylinder from $1\frac{1}{2}$ to $2\frac{1}{2}$ cms. larger in diameter than the thermometer tube and about 4 cms. or more longer than the coil, open

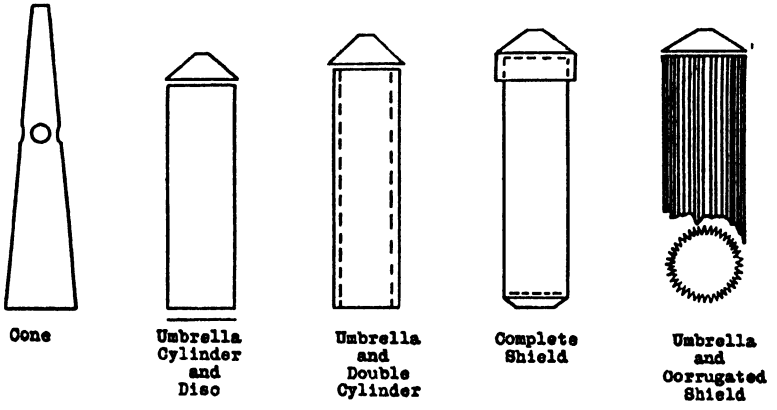


FIG. 35.—Various types of radiation shields.

below and with an umbrella above, was the most satisfactory form of shield, which is practically the same as that originally devised by Callendar and Griffiths. The umbrella should fit the thermometer tube closely and extend beyond the end of the cylinder, leaving a space 5 mms. to 1 cm. high between the umbrella and cylinder for circulation of the vapour.

The sulphur-point is an excellent "fixed point" for calibration purposes*; it is possible to keep the temperature of the vapour steady to within $\frac{1}{100}°$ for hours, account being taken of barometric changes.

When a high order of accuracy is not required in the standardisation of a pyrometer, the form of sulphur boiling-point apparatus illustrated in Fig. 34 will be found useful. It can readily be constructed from a discarded steel cylinder for compressed gas and steam pipe fittings. The condenser is a quartz tube, which is less liable to crack than glass. The cheaper translucent

* Messrs. Mueller and Burgess have drawn up a standard specification for the sulphur boiling-point apparatus. Their proposals are quoted in Appendix I.

variety of quartz is quite satisfactory, since the level of the sulphur vapour may be readily ascertained by lightly touching the tube at various points. The level of the vapour when the apparatus is working normally should be at a height of about 6 inches above the base of the condenser tube.

It will be observed that the cones are permanently fixed in the case of the apparatus shown in Fig. 34.

Purity of the Sulphur.—Ordinary commercial stick-sulphur manufactured by the " Chance process " is satisfactory, since no difference has been observed between its boiling-point and that of highly purified sulphur.

Usually when sulphur is boiled for the first time volatile impurities distil off. A black residue (FeS) is generally found, but in the quantity in which it is usually present this appears to have no influence.

Variation with Pressure of the Boiling-point of Sulphur.—The influence of pressure on the boiling-point of sulphur is quite considerable, in the vicinity of 760 mms. an increase of 1 mm. in the barometric height raises the boiling-point by approximately 0·09°.

The relation between temperature and pressure over the range of importance in practical work has been investigated by Holborn and Henning and by Harker and Sexton (1908), and the results are in close agreement.

Over the range 720-780 mms. the relation between temperature and boiling-point may be represented by the formula—

$$t = t_s + 0{\cdot}0904\,(p - 760) - 0{\cdot}0000519\,(p - 760)^2$$

where t is the boiling-point at pressure p,

t_s ,, ,, ,, 760.

In Table XLVI. the values of t, assuming $t_s = 444{\cdot}53°$ C., have been calculated from the above formula. In addition, the values of the quantity $\left\{\left(\frac{t}{100}\right)^2 - \frac{t}{100}\right\}$ are given for the same values of t; this coefficient is required in calculating the value of δ.

The freezing-point of zinc (419·4° C.) is sometimes recommended as a third fixed point instead of sulphur.

As the sulphur-point is so well established and convenient to use, there do not appear to be very valid reasons for discarding it in favour of a freezing-point determination.

Example of Method of Reduction of Observations taken in the Standardisation of a Platinum Thermometer.—The resistance observations were corrected for the errors of the coil values, the temperature, and the value of the bridge centre deduced.

The resistance at the temperature of melting ice was 257·916 units.

In steam the resistance was 357·953.

The barometric height during the steam-point observations was 766·26, and the temperature of the mercury column and scale 17·55° C.

The barometric height has to be reduced to that corresponding to a column at 0° in latitude 45°.

Tables are available for this reduction in the case of standard types of barometers possessing a brass scale, such as the Fortin type.

The correction for temperature in this case is — 2·19 mms., while the latitude correction is approximately + 0·45 for places on the parallel through London. Hence the corrected value of the pressure is 764·52 at 0° latitude 45°.

The boiling-point of water under a pressure of 764·52 mms. is 100·1654° C. according to Broch's recalculation of Regnault's observations.

Hence increase in resistance for a temperature change from 0° to 100·1654° C. = 100·037 units.

To obtain the value of the F.I. the resistance at 100° C. is required.

$$\delta R \text{ for } 0{\cdot}1654 = \frac{100{\cdot}037}{100{\cdot}1654} \times 0{\cdot}1654 \times 0{\cdot}985 = 0{\cdot}163.$$

[The coefficient 0·985 is the value of $\frac{(\triangle p\, t)}{\nabla\,(t)}$ near 100° C. for a thermometer of $\delta = 1{\cdot}50$. The general formula is

$$\frac{(\triangle p\, t)}{\triangle(t)} = \left(1 - \delta\,\frac{2t - 100}{10{,}000}\right)\Bigg]$$

Hence $$R_{100} = 357{\cdot}790$$

so that $$R_{100} - R_0 \equiv \text{F.I.} = 99{\cdot}874.$$

The resistance in sulphur was 679·165, and the barometric height 766·23 at 17·5°. Correcting for temperature (— 2·19 mms.), and latitude + 0·45 mm. barometric height at 0° and latitude 45° = 764·49 mms. For this pressure the boiling-point of sulphur at this temperature is 444·94° C. (Table XLVI.).

The platinum temperature ($p\, t$) corresponding to the above value of the resistance is

$$\frac{679{\cdot}165 - 257{\cdot}916}{99{\cdot}874} = 421{\cdot}78.$$

So that $t - p\, t = 444{\cdot}94 - 421{\cdot}78 = 23{\cdot}16$.

Now from Table XLVI. $\left[\left(\frac{t}{100}\right)^2 - \frac{t}{100}\right] = 15{\cdot}347$ for $t = 444{\cdot}94$.

Hence $\delta = \frac{23{\cdot}16}{15{\cdot}347} = 1{\cdot}51$.

NOTE.—In reducing platinum thermometer observations to true temperatures Table XLVII. will be found convenient. It has been calculated for $\delta = 1{\cdot}50$; should the thermometer have a different value of δ a small correction can be applied to the readings from Table XLVIII. In fact, these corrections can best be obtained from a small scale curve based on the data given in this table.

Some observers employ a curve connecting $t - p\, t$ with $p\, t$. Unless the curve is drawn on a very large scale it is difficult to obtain sufficient accuracy by this method.

Application of the Resistance Thermometer to High Temperature Work.—Almost the very first scientific use made of the platinum thermometer was for the determination of high temperature freezing-points, as described earlier in this chapter. This application, however, is an operation which

requires considerable care if results of the highest order of accuracy are desired.

The thermometer usually has a bulb of 3 to 4 cms. in length and enclosed in a heavy porcelain sheath. Consequently it is necessary to allow for a depth of immersion of from 6 to 8 cms. in the metal. Further, the rate of cooling should be slow, to diminish possible error due to lag. Heycock and Neville state that the freezing-point of gold could be read to $\frac{1}{100}°$ without difficulty. In a study of the effect of high temperatures on the constants of platinum thermometers they found that the first few heatings to 1,000° C. increased both the R_0 and the F.I. This effect they ascribed to the thickening of the mica plates after exposure to the high temperature and the consequent straining of the fine wire when the coil cools and the wire contracts on to the larger frame.

They concluded that the constants should be determined *before* each temperature measurement of importance, and, provided the leads had been well annealed originally, that these constants should be used in calculating the temperature, regardless of what the values of the constants might be after the experiments. A thermometer should, of course, be thoroughly annealed before standardisation.

Industrial Types of Resistance Thermometers.—For industrial use the sensitive type of resistance thermometer, bridge, and galvanometer are out of the question, and several modifications have been evolved with a view to obtaining robustness combined with ample, if moderate, sensibility.

In the Whipple indicator the resistance box is replaced by a long bridge wire wound spirally on a drum. A sensitive pivoted galvanometer is fixed in the top of the case and balance obtained by rotating the drum. The instrument has a scale graduated directly in ° C., and readings may easily be taken to about $\frac{1}{5}°$ in the range 0° to 1,100° C.

In the Paul Harris indicator the principle of the ohmmeter is applied. The instrument consists of a moving coil indicator having two coils wound on one support and pivoted in a magnetic field. One of the coils is connected across a shunt in the battery circuit, while the other (wound at right angles to it) consists of two windings, one of which is shunted across the platinum thermometer and the other across a standard or comparison resistance. The deflection scale can be arranged to cover a limited temperature range, so that an open scale is possible.

In the Callendar recorder the suspended coil galvanometer carries a boom, which on deflection releases the brake from a clockwork motor. The motor pulls a carriage along a slide wire until balance is obtained. A pen records the position on a rotating drum with paper surface.

In these types of instruments it is advisable to give some attention to the battery. To obtain sensitivity the current through the platinum coil has to be fairly considerable and is attended with the usual rise in temperature of the wire, due to heating effect. Unless the battery current is maintained at about the same value as when the calibration of the instrument was effected small errors in the readings will be produced.

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CHAPTER IV.

THE THERMOCOUPLE.

The Thermocouple.— Pouillet appears to have been the first to realise the value of the thermoelement for the measurement of high temperatures. With an iron-platinum couple and a low resistance tangent galvanometer, he employed the thermoelectric method in a crude way for the measurement of furnace temperatures. Probably the unreliability of the instrument, caused by contamination of the platinum by the reducing atmosphere within the iron gun barrel, discouraged him from pursuing the work. His method of calibration by means of a gas thermometer was very commendable.

Since that time considerable advances have been made in this method of pyrometry, notably in the direction of improving the homogeneity of the thermoelement wires; the development of high resistance moving coil indicators; and of potentiometers adapted for the measurement of the small E.M.F. produced by the thermocouple; until, at the present day, the thermoelectric method of measuring temperature has attained a degree of precision second only to the resistance thermometer, and for temperatures exceeding 1,100° C. it is the only convenient and sensitive electrical method available.

It must be emphasised, however, that the thermoelement is only a subsidiary instrument, whose scale will not stand extrapolation over extended temperature ranges, which practice has led to much confusion in high temperature work in the past.

A thermoelectric pyrometer outfit is made up of the following elements :—

1. The two metals constituting the thermoelement.
2. The electrical insulation of these wires and the protecting tubes.
3. The indicator or potentiometer for measuring the thermal E.M.F.
4. The provision for controlling the cold junction temperature.
5. The wiring system, switches, etc., when the installation consists of more than one pyrometer.

Choice of Metals for use as Thermocouples.—The choice of pure metals and alloys for use in the construction of thermocouples is primarily determined by the temperature which has to be measured.

But for the question of cost, platinum and its alloys would be universally used as their non-oxidisability and high melting-point make them ideally suitable for thermoelectric work.

The necessity of substituting some less expensive material for these rare metals has led to an extended study of other metals and alloys, with the result that it is now possible to measure temperatures up to 1,200° C. with base metal couples with a moderate degree of accuracy, but for scientific work at high temperatures there is no alternative to the rare metal thermo-element.

Base Metal Thermoelements.—For low temperature work up to about 300° C. copper, iron, or silver *versus* constantan are quite satisfactory, possessing a large E.M.F. per degree of the order of 40 to 60 microvolts.

Copper Constantan.—Both copper and constantan are obtainable in any size wires, and the thermocouples maintain their calibration if not overheated. At temperatures above 300° C. rapid deterioration occurs unless the couple is made of heavy section wires, and experience has shown that a precision of only 5° to 10° C. can be expected in measuring temperatures in the neighbourhood of 500° C.

Iron Constantan.—The E.M.F. temperature relationship of iron constantan is a closer approximation to a straight line than is the case with copper constantan. For work at low temperatures the combination has the practical drawback that the iron is liable to rust in a humid atmosphere.

Iron constantan thermocouples are employed in technical work up to 800° C., and are then made of very heavy section wires. After prolonged exposure to high temperatures iron is subject to the development of parasitic currents. These may have their origin in a variety of sources. It is believed that segregation and cavities of occluded gas in the casting can give rise to a want of homogeneity, whilst changes of crystal structure on prolonged heating is also a frequent source of trouble.

Iron Nickel.—This combination of two common metals was once extensively used in industrial work, but has since been largely displaced by alloys more resistant to oxidation and to change at high temperatures.

Nickel undergoes a molecular transformation between 230° and 390° C., which renders the pyrometer unsuitable for use over this range, but it gives fairly satisfactory results between 400° and 800° C.

The E.M.F. temperature relationship of the couple is nearly linear over the working range.

A peculiar fact has been observed about nickel: the pure metal is oxidised and rendered brittle by heating in air, whilst its alloys with chromium and aluminium resist oxidisation fairly well and do not deteriorate rapidly.

Nickel-Chromium, Nickel-Aluminium.—Nickel-chromium: 90 per cent. Ni, 10 per cent. Cr; nickel-aluminium: 98 per cent. nickel, about 2 per cent. Al with Si and Mn.

This combination was introduced by Hoskins, and is sometimes known by the trade name of chromel alumel thermoelement. It originated in a search for a metal to replace the iron element in the iron-nickel thermo-element. The alloy "chromel" proved so successful that a substitute for nickel was found in the "alumel" alloy. The presence of small quantities of silicon and manganese appears essential, for it was found that, although

the pure nickel-aluminium alloy stood up well at high temp. became brittle with use at lower temperatures.

The chromel-alumel couple can be used up to 1,100° C. contin and will stand for short periods a temperature 200° C. higher.

The E.M.F. temperature curve above 100° C. is nearly a straight line.

It should be remembered that the E.M.F. of base-metal couples decrease with prolonged exposure to high temperatures, so frequent recalibration is necessary.

The fact that base-metal thermocouples generate about four times the E.M.F. per degree of platinum, rhodium couple is an advantage from the point of view of the construction of robust pivoted indicators for portable outfits, but since they are less stable than the platinum couples they cannot be employed for work where permanency of calibration is essential.

Platinum Thermoelements.—Platinum : platinum 10 per cent., rhodium. This thermoelement was introduced by Le Chatelier in 1886, and has since remained the most reliable of all combinations tested.

It is generally employed in scientific work at high temperatures and in a great many industrial installations. Such couples will stand 1,500° C., but care must be taken to shield them from reducing gases, silicon, or metallic vapours. Platinum couples must be thoroughly protected from the vapours distilled from graphite or carbon at high temperatures.

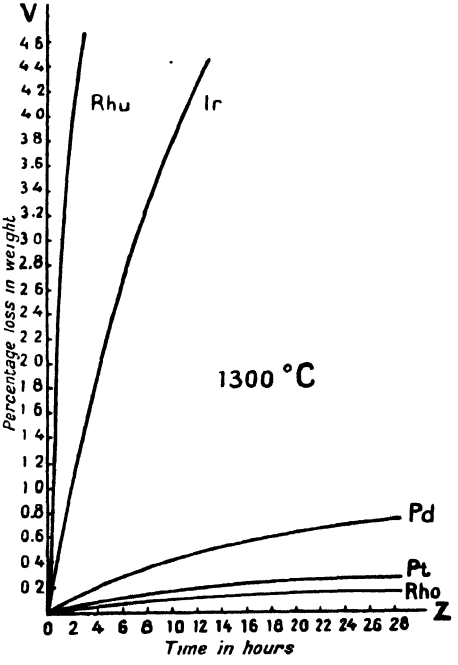


FIG. 36.—Relative volatility of metals of the platinum group at 1,300°.

Z = Time in hours.
V = Loss in weight percentage.

Platinum : Platinum Iridium.—The platinum-iridium alloy, first used by Barus, works satisfactory up to about 1,000° C., but at higher temperatures the iridium volatilises and prolonged exposure causes contamination of the pure platinum limb of the element.

The relative volatility of the rare metals is shown by the curves in Fig. 36, which are based on some experiments made by Sir William Crookes. The metals were kept at a temperature of 1,300° C.

Temperature Indicators of the Millivoltmeter Type.—The majority of the thermocouples used in industrial work are equipped with moving coil

The instruments are identical in construction with millivolt-
ıile the scales are generally graduated to read temperatures directly.
. calibration of such an instrument is correct so long ⱥs the total
ance of the circuit remains unaltered.

When the indicator has a resistance of from 100 to 500 ohms, small variations in the resistance of the leads or of the couple are of no consequence.

An idea of the high sensitivity necessary in the indicator may be formed when a comparison is made with ordinary voltmeters. With a thermocouple outfit it is often desirable to have a full-scale deflection for 10 millivolts, which is only one ten-thousandth of the voltage which the switchboard instrument has to measure on a 100-volt system.

In order to obtain a robust moving-coil system, the indicators fitted to base-metal couples sometimes have a resistance as low as 2 ohms, and if the couples are of heavy section wire, protected from oxidation, the outfits work fairly satisfactorily.

Especial care must be taken with such installations not to cause any alteration of the total resistance of the circuit.

It must be borne in mind that the indications of such an outfit will also be affected by changes of resistance of the leads caused by variations of temperature of the furnace room. It was observed in the case of a 5-ohm resistance indicator that changes of temperature from 0° to 35° C. along 50 feet of wiring from the thermocouple to the instrument caused the indicator to read 10° C. low at 650° C. So, apart from difficulties due to oxidation and varying depths of immersion, high accuracy cannot be obtained with a low resistance millivoltmeter. With platinum thermocouples the cost of the material prohibits the use of thick wire, and it is, therefore, necessary to employ high resistance indicators.

Millivoltmeters are now obtainable of 500-ohm resistance, giving a full-scale deflection for 40 millivolts, and the indications of such an outfit can generally be relied upon within $\pm 5°$ C. When higher accuracy is desired it is necessary to use a potentiometer.

Compensation for Varying Circuit Resistance.—Harrison and Foote have described a scheme of circuits by means of which it is possible to arrange that the total resistance of galvanometer, leads, and thermoelement is periodically adjusted to a fixed value. The principle of the method will be understood from Fig. 37. There is an adjustable resistance r_x in series with the moving coil, and swamping resistance of the millivoltmeter or temperature indicator.

On depressing a key, part r_2, of the swamping resistance is short-circuited, and the remaining part, together with the moving coil r_3, is shunted by the resistance r_4. The instrument is calibrated in terms of the potential drop across its terminals for a maximum value of $r_x = r_1$. In the construction the resistances are proportioned according to the relation $r_2 r_4 = r_1 r_3$. If the resistance r_x is so adjusted that the deflection of the pointer is unchanged by depressing the key K it can readily be proved that the total resistance of the circuit is that for which the instrument is calibrated, the sum of r_x

and all external resistance being thus made equal to r_1. Hence it follows that the instrument measures the true E.M.F. in a simple circuit, or if connected across a resistance or network through which a current flows it indicates the potential drop which would have existed had the instrument not been connected. In this respect it functions as a potentiometer, yet it does not operate on the potentiometric principle, since it does not require a standard cell or an auxiliary battery, the only E.M.F. employed in the adjustment being that of the source measured.

By constructing the apparatus so that the ratio r_3/r_4 is equal to from 5 to 10 it is possible to adjust r_x with 5 to 10 times the precision necessary. Thus, if the galvanometer can be read to $\frac{1}{10}$ of a scale division the line resistance may be adjusted with a precision equivalent to $\frac{1}{100}$ of a scale division, which is at least 10 times the accuracy possible with an indicating instrument. This principle of magnification of errors greatly facilitates the proper adjustment of r_x. By varying the copper to maganin ratio in r_4 it is possible to produce a compensated instrument of zero temperature-coefficient from a millivoltmeter having an excessive copper content.

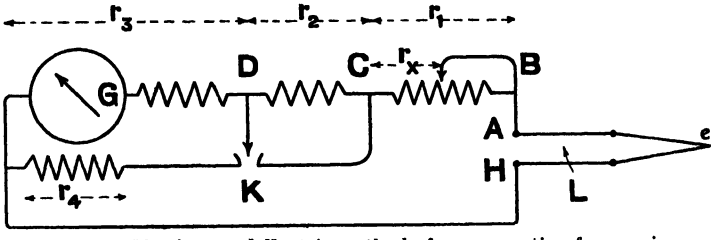


FIG. 37.—Harrison and Foote's method of compensation for varying circuit resistance.

Such an instrument should be serviceable in thermocouple work. The compensated millivoltmeter may also be used in multiple installations of thermocouples having different line resistances, as many resistances r_x being employed as there are couples. These may be inexpensive rheostats, one located in each line between the couple and selective switch, and still the accuracy of adjustment will be high as though precision rheostats were employed.

Potentiometers for the Measurement of Thermal E.M.F.'s.—Since the electromotive forces to be measured are of millivolt order the potentiometer has to be specially designed for the work.

With a low resistance potentiometer and a sensitive moving coil galvanometer, it is possible to measure to 1 microvolt with certainty and with greater precautions measurements to 0·1 microvolt are possible, but rarely necessary.

Essentially, a potentiometer is a row of resistances in series through which a steady current is passed. This current is kept constant by occasionally adjusting it so that the fall of potential through a fixed resistance balances the E.M.F. of a standard (cadmium) cell.

Then, since in a simple circuit the fall of potential is proportional to the resistance, any E.M.F. within the range of the instrument can be measured by balancing it against the drop over the appropriate known resistances.

In Fig. 38 the rheostat R is adjusted until the difference in potential across K is balanced against the E.M.F. of the standard cadmium cell C (1·0185 volts at 15° C.). The E.M.F. of the thermocouple X is balanced on the resistance r, shown here for simplicity as a uniform wire.

The potentiometer can be made direct reading in microvolts, by so constructing it that the fall in potential per ohm resistance is some definite value, for example, 1 volt per 100 ohms. Hence to measure in steps of millivolts requires subdivision of the resistances into 0·1-ohm coils. A bridge wire in series (of the same resistance), having a scale divided into a hundred parts, would enable readings to be taken to 10 microvolts or by estimation to 2. In such a case the point P could move over the studs of the coils, while Q would traverse the bridge wire.

Since potential contacts only are necessary, there is no objection to the use of low resistances in the circuits.

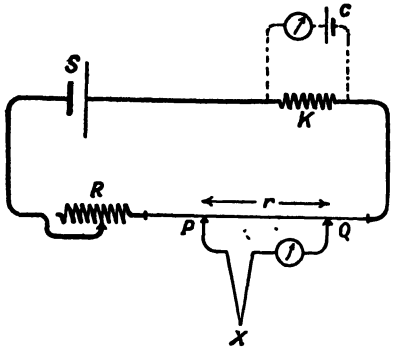


FIG. 38.—Potentiometer for measurement of thermal E.M.F.

R, rheostat (variable); S, storage cell; X, thermocouple; C, standard cell; K, resistance across which standard cell is balanced.

Simple Circuit Potentiometer.—A practical form of the diagram above is shown in Fig. 39.

The current through the potentiometer is adjusted to be 0·01 amp. by balancing the cadmium cell across 101·85 ohms (circuit shown dotted in diagram).

The working range of the potentiometer consists of 100 equal coils arranged in four dials of 25 coils each.

The resistance of each coil is 0·01 ohm, hence the total fall of potential across the hundred coils is 10 millivolts, and across each coil 100 microvolts.

The bridge wire in series with the coils is of 0·01 ohm, and the scale is subdivided into 100 parts, consequently the value of 1 division is 1 microvolt.

By inserting a plug which short-circuits half the resistance across which the standard cell is balanced, the range of the instrument is doubled.

An alternate way of obtaining higher ranges is to employ two or three secondary cells in series and balance against 2, 3, or 4 cadmium cells.

Fig. 40 is a view of the top of the potentiometer; the switch contacts are fixed on the under surface of the ebonite top.

Vernier Forms of Potentiometers.—The above-described potentiometer, which is representative of a large class, has the disadvantage of only permitting steps of equal value. The decade principle common in P.O. resistance boxes is not possible with the simple circuit of series coils.

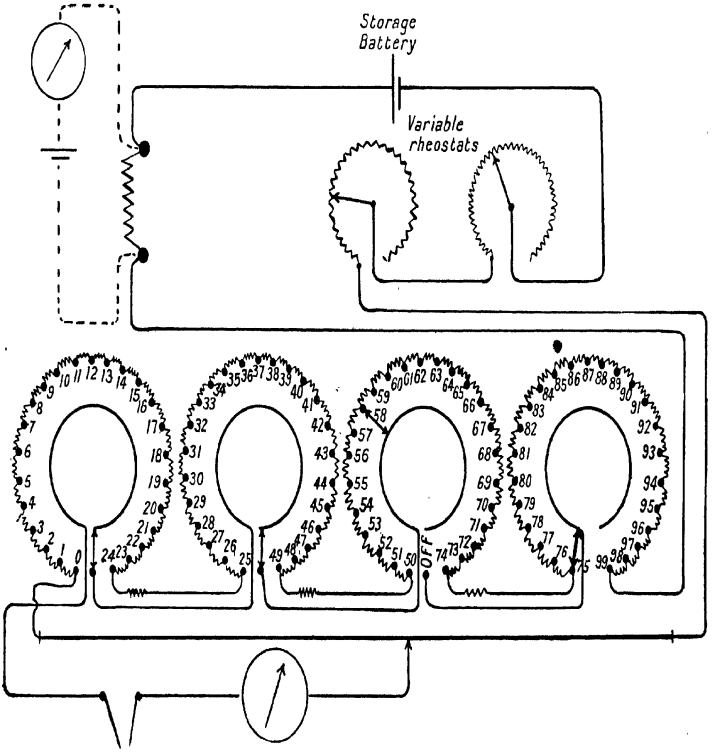


FIG. 39.—Diagram of simple circuit potentiometer.

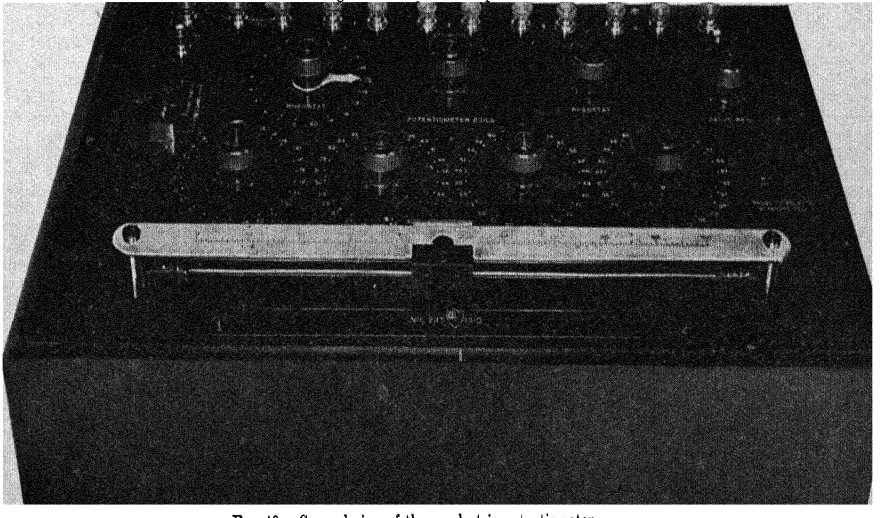


FIG. 40.—General view of thermoelectric potentiometer.

This difficulty was surmounted in a very ingenious manner by Thomson and Varley in their vernier type of potentiometer, which was designed for resistance and cell comparison work.

In this type the bridge wire of the ordinary Clarke potentiometer is replaced by a subdivided resistance coil, which can be placed in parallel with any two coils in series of the main circuit, as shown in Fig. 41.

The storage-battery is connected through a rheostat with a dial consisting of 101 coils of 1,000 ohms each in series. A second dial of 100 coils of 20 ohms each can be placed in parallel with any two adjacent coils of the main dial by a movable contact-maker.

Now, the effect of the second dial as shunt on the two coils of the main dial is to make the effective resistance between the points of contact equal to 1,000 ohms—*i.e.*, that of the individual steps. Hence the fall in potential over the 100 coils in the shunt dial is the same as that over a single coil of the main dial, so that the effect of the shunt dial coils is to give 100 intermediate steps between any two points on the main dial.

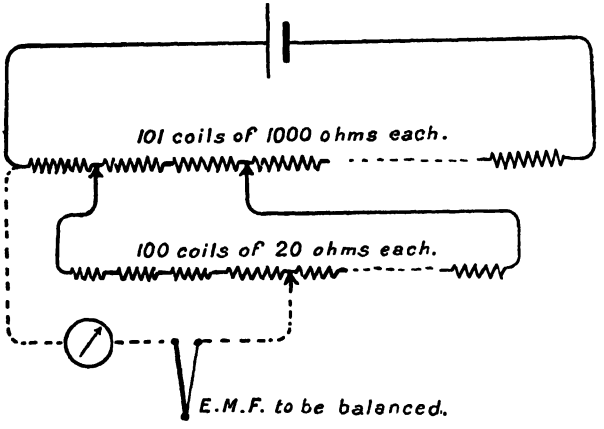


FIG. 41.—Diagram of Thomson and Varley's type of potentiometer.

It will be observed that the contact resistances at the points where the shunt dial is connected to the main dial are assumed to be negligible.

The drawback to the application of the vernier principle to thermo-electric potentiometers is that the coils of the latter have to be of low resistance in order to obtain sensitivity. Hence contact resistances require careful elimination when the principle is applied to low-resistance potentiometers.

Harker (1903) described a simple form of vernier potentiometer in which the second dial above referred to was replaced by a plain bridge wire.

The connections are shown in Fig. 42.

The standard cell is balanced across 101·85 ohms, hence the current is 0·01 amp.

The 20 coils A B each have a resistance of 0·1 ohm, so that the potential

drop per coil is 1 millivolt or 1,000 microvolts. Each of the 11 coils in the row C D has a resistance of 0·01 ohm, consequently the potential difference per coil is 100 microvolts. The bridge wire E F can be placed in parallel with any two coils of C D, and is 0·02 ohm in resistance. The scale is subdivided into 100 parts, each of which corresponds to 1 microvolt. All contacts to the coils in A B and C D are made by means of mercury cups. Manganin bars are laid alongside the cups and drilled with a corresponding series of holes, so that connection at any point may be effected by a ∩-shaped copper bar.

Tinsley has devised a form of vernier potentiometer in which the slide wire is replaced by a dial with 100 stud contacts, between each of which there is a resistance of one-thousandth of an ohm. The potentiometer consists essentially of one main dial of 20 coils of 10 ohms each, across which

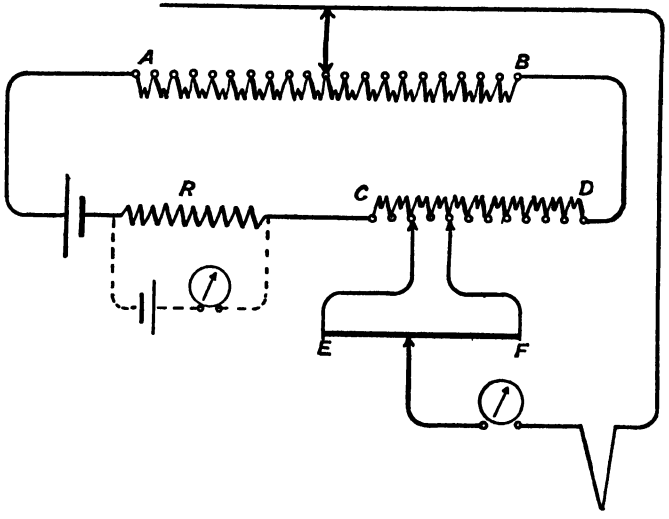


FIG. 42.—Diagram of Harker's modified form of vernier potentiometer.

A to B, 20 coils of 0·1 ohm each; C to D, 11 coils of 0·01 ohm each; E F, bridge wire of 0·02 ohm; R, coil of 101·86 ohms.

is inserted the shunt dial, consisting of 100 coils of 0·2 ohm each (see Fig. 43). This dial is arranged so that it is always shunted across two coils of the main dial in the usual manner. Thus with a current of 1 milliampere through the circuit the main dial reads ·01 volt per stud. The vernier dial reads ·0001 volt per stud, whilst the fine adjustment dial reads ·000001 or 1 microvolt per step. Hence the range of the potentiometer lies between ·1901 volt and 1 microvolt. A range of 10 times this value is obtained by moving the plug from B to A. The current through the potentiometer is set by balancing a cadmium standard cell against 101·85 ohms on the dials and with the plug in position A. When the plug is placed in B the current through

the potentiometer is reduced to one-tenth its original value, whilst the total resistance in the battery circuit remains unaltered.

The design would be improved if the standard cadmium cell was balanced against a separate resistance, as then the adjustments of the dials would not have to be altered when it was desired to check the current in the circuit.

Mr. R. Paul has designed a vernier potentiometer with two ranges; on the lower range E.M.F.'s from 1 microvolt to 17 millivolts can be measured, while the second range is ten times that of the lower.

Fig. 44 shows the connections diagrammatically: in the actual instrument the coils are carried on a series of drums set alongside each other. The standard cell is balanced by varying X* with the plug inserted in A,

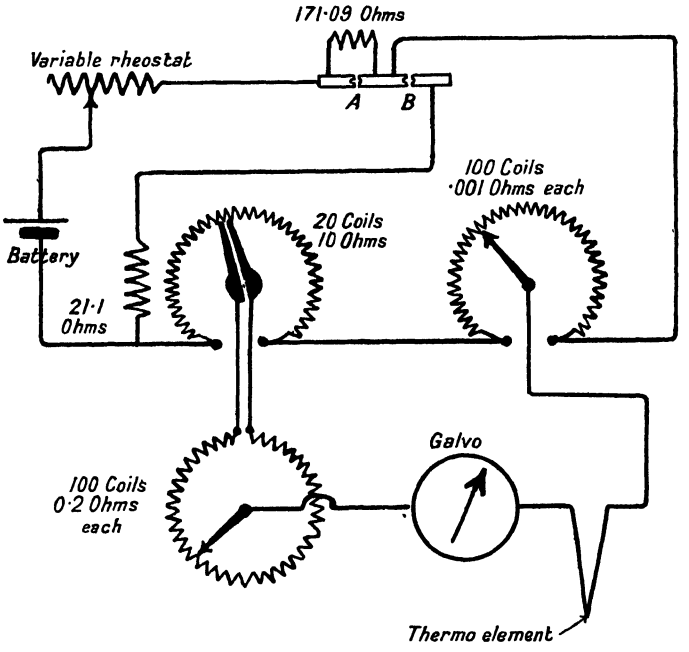


FIG. 43.—Tinsley's vernier potentiometer.

the position corresponding to the higher range. It will be seen that the values of the various resistances are so adjusted that the effect of transferring the plug from A to B is to reduce the E.M.F. on the working portion of the potentiometer to one-tenth the original value, while leaving the resistance of the complete circuit in series with the storage cell unchanged. The plug in the position B gives the lower range.

The current through the potentiometer coils is 0·001 amp. for the higher range, and 0·0001 amp. for the lower range.

* The adjustable resistance X brings the potentiometer resistance up to 1,850 ohms when the E.M.F. of the storage cell is 1·85 volts.

The high resistance of this potentiometer necessitates the use of a galvanometer of high resistance (of the order of 1,000 ohms) and high sensitivity. In fact, for working on the lower range the best class of moving coil galvanometer is required.

Deflection Potentiometers.—A type of instrument, which occupies a position intermediate between the nul potentiometer on the one hand and the moving coil deflection instrument on the other hand, is the portable deflection potentiometer.

In one of this class of instruments the thermal E.M.F. is balanced to the nearest 2 millivolts and the deflection of the pointer observed. The

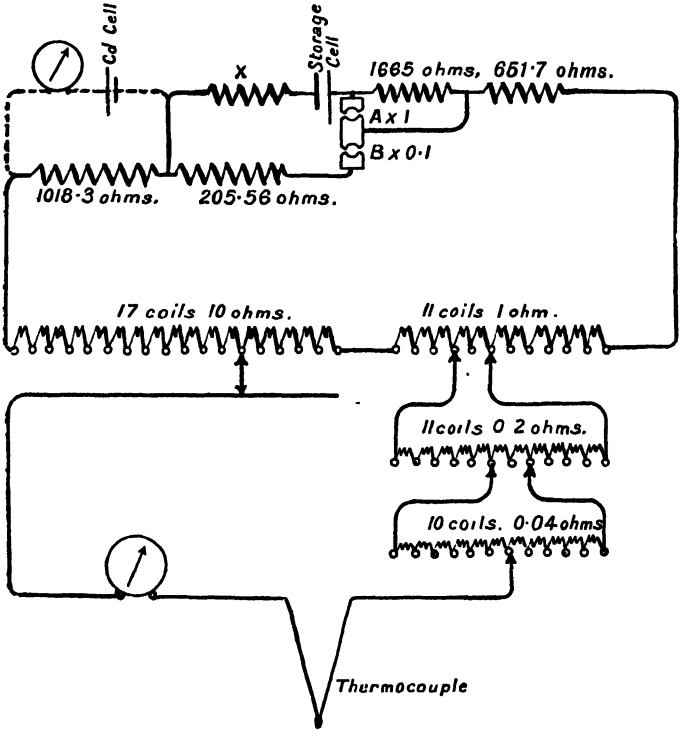


FIG. 44.—Diagram of Paul's modification of a vernier potentiometer. Plug in position B gives the lower range (each division on lowest dial equal to 1 microvolt).

galvanometer has a central zero, and 10 scale divisions correspond to 1 millivolt.

In Fig. 45 are shown the connections of an instrument designed on this basis.

To maintain a constant sensitivity of the indicator for all potentiometer readings it is necessary to keep the total resistance in the galvanometer circuit to a constant value. This is effected by arranging that the

switch on the millivolt studs also cuts out from the galvanometer circuit a resistance equivalent to that added in the potentiometer circuit.

Referring back to Fig. 38, p. 66, let—

G be the resistance of the galvanometer and that of a series resistance;

T be the resistance of the thermoelement;

r the resistance in the potentiometer circuit, across which the thermal E.M.F. is balanced.

$Z + r$ is the total resistance of the main circuit of the potentiometer.

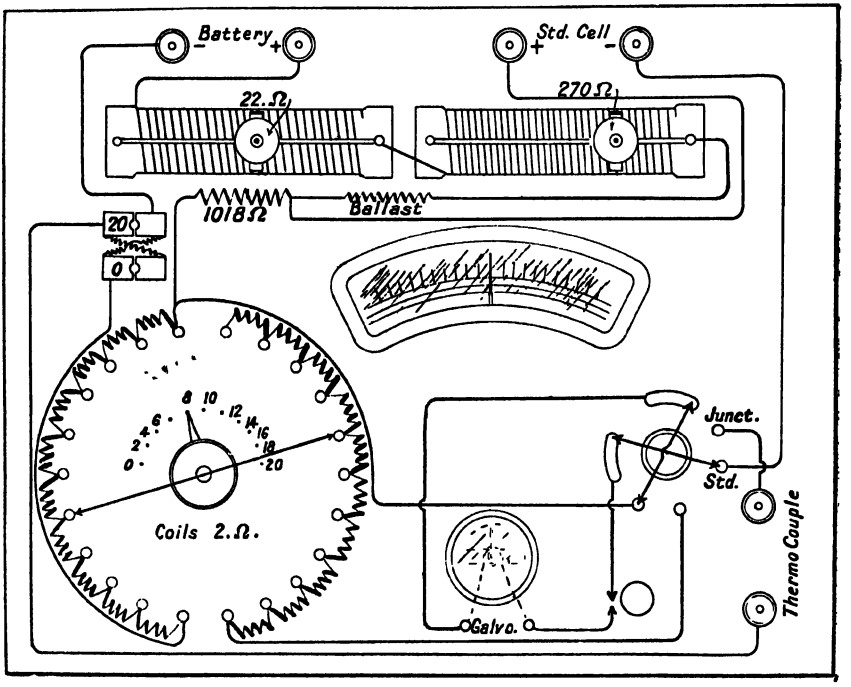


FIG. 45.—Diagram of deflection potentiometer.

(Resistance in the galvanometer circuit kept to a constant value.)

Let $\triangle e$ be the residual unbalanced E.M.F. of the thermoelement which produces the galvanometer deflection. Now the deflection of the galvanometer is proportional to the current through it, and to obtain the magnitude of this current we require the total resistance in the circuit P to Q.

The resistance between the points P and Q is that of the resistance r shunted by the main circuit of the potentiometer outside these points—viz., Z.

Hence the effective resistance is $\frac{r\,Z}{r+Z}$; so the deflection of the galvanometer is proportional to $\frac{\triangle e}{\frac{r\,Z}{r+Z}+T+G}$.

For the small E.M.F. generated by the couple r is small compared with Z. Hence r in the denominator of $\frac{r\,Z}{r+Z}$ may be neglected. So the deflection is proportional to $\frac{\triangle e}{r+T+G}$. From this it follows that to obtain deflections proportional to $\triangle e$ and independent of r, it is necessary to diminish the resistance in series with the galvanometer by an amount r, and this can be automatically effected by the brush arrangement shown in Fig. 45.

Cold Junction Correction.—For accurate work the cold junction should be maintained at 0° C. by inserting the junctions with the copper leads into two tubes standing in ice.

The recent development of the "all steel" Dewar vacuum vessel is likely to remove many of the troubles encountered with varying cold junction temperatures.

When these vacuum vessels are employed the platinum-rhodium thermo-element is made with leads sufficiently long to reach from the couple down into the steel bottle and connections made from this point by means of copper leads. In the vicinity of a hot furnace the bottles will preserve crushed ice for periods up to twenty-four hours, but it is advisable to use tubes of low thermal conductivity for protecting the junctions in the ice, otherwise the heat conduction along the tube melts the ice rapidly.

If it is not feasible to have the cold junction at 0° C. a correction must be applied. This cold junction correction in general is not equal to the temperature of the cold junction, but depends on the temperature of both hot and cold junctions.

(*a*) If the temperature of the cold junction is determined by the aid of a mercury thermometer, then the E.M.F. corresponding to this temperature is to be added directly to the observed E.M.F. of the hot junction.

(*b*) With a pyrometer provided with a direct reading instrument this correction may be accomplished mechanically by changing the zero of the instrument so that when short-circuited it indicates the temperature of the cold junction. An alternate plan, which is convenient when it is desirable not to alter the zero of the indicator, is to correct the observed reading, as follows :—

When the cold junction is at a temperature (t_0) the true temperature may be obtained by adding to the observed temperature (t_2) the quantity obtained by multiplying the value of the temperature of the cold junction (t_0) by a factor which is the ratio of the slopes of the calibration curve (E.M.F.

against the temperature) at the origin and at the temperature (t_1); or putting it into symbols :—

$$\text{Correction} = \frac{\left(\frac{de}{dt}\right)_{0°-30°}}{\left(\frac{de}{dt}\right)_{t_1}} \times t_0.$$

(*c*) The third method of fixing the cold junction correction is a graphical one. By means of a series of curves, such as those shown in Fig. 46, the correction may be determined by inspection. In this diagram the number of degrees to be added to the hot junction temperature are plotted as ordinates and the cold junction temperature as abscissæ. In the diagram curves are drawn for several temperatures (uncorrected) of the hot junction between 400° and 1,700° C.

In industrial installations it is inconvenient to have to apply cold junction

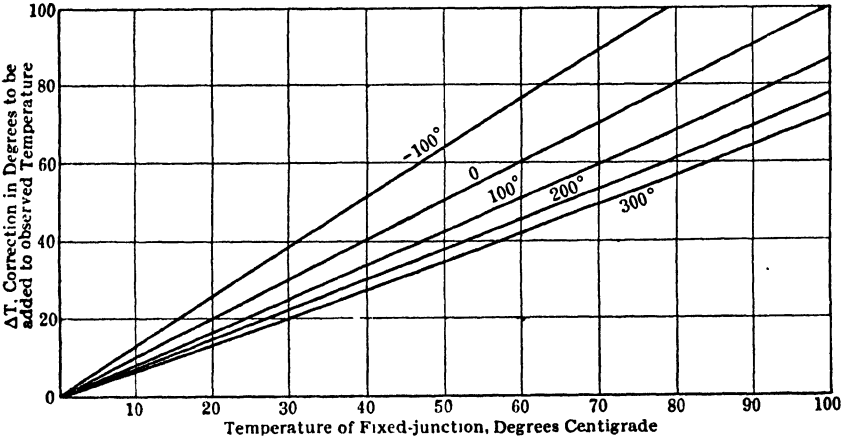


FIG. 46.—Graphical method of correcting for cold junction temperature (L. H. Adams). (Typical set of curves for a Pt-PtRh batch of thermocouples).

corrections or to adjust the zero of the indicator, and a variety of devices have been evolved to minimise the trouble to variations of cold junction temperature.

It is now customary to remove the cold junction from the head of the pyrometer, which may vary a hundred degrees or so if near the furnace wall, to a distant point by means of compensating leads.

Compensating Leads.—For base-metal couples these lead wires are of the same material as those employed in the couple, small stranded wires being used for flexibility. Thus the cold junction is transferred to a point where the temperature is reasonably constant, and from this point copper wires lead to the indicator. The compensating wires may terminate in a cold junction box fitted with a thermostat, or may be buried underground. At a depth of 10 feet beneath the floor of a large building the temperature

remains constant to within 2° C. throughout the year; usually this mean temperature is about 12° C. for temperate climates, but may differ somewhat in the immediate vicinity of a large furnace. To apply this method of control, an iron pipe of the proper length, closed at the bottom, is driven into the ground, and the two cold junctions, well soldered and carefully insulated, are threaded to the bottom of the pipe in such manner as to be conveniently removable when necessary. The top of the pipe may be plugged with asbestos or waste, and covered with pitch to keep water away from the insulation. The scale of the indicator is set to read the mean temperature of the bottom of the tube. It is convenient to have an extra pair of compensating leads or an extra thermocouple with its junction at the bottom of the pipe, to measure this temperature occasionally. A disadvantage of the buried pipe is that the moisture or water may accumulate in the pipe. When this occurs it generally gives rise to galvanic effects, which result in greater error than those caused by changes of cold junction temperature. So that thermostat box arrangement is preferable when possible.

Usually the compensating leads of a base-metal couple are marked, or are equipped with one-way terminals, so that they are easily connected properly to the head of the couple. If reversed at the couple, the leads will cause an error double the amount of the compensation. When compensating leads of a base-metal couple are properly connected to the couple no deflection of the indicator is registered by heating the head of the couple.

The high cost of platinum prevents the use of compensating leads of that metal, but inexpensive wires of copper and nickel-copper alloy are now available for use with platinum and platinum-rhodium couples. These lead wires do not compensate individually, but taken together they compensate to within 5° C. for a variation of 200° C. at the junction of the couple and lead wires. Both terminals on the head of the couple should be kept as nearly as possible at the same temperature. The copper compensating lead is connected to the platinum-rhodium wire of the couple, and the copper-nickel wire is connected to the platinum wire of the couple—*i.e.*, alloy to pure metal in each case. The cold junction is then located at the indicator end of the compensating leads; the temperature at this end may be controlled by one of the methods described; copper wires run from this point to the indicator or potentiometer.

In the majority of cases the compensating leads terminate in the indicator box, and then it is merely necessary to correct for the changes of temperature at the indicator, which is usually favourably situated as regards uniformity of temperature.

Automatic Compensation for Cold Junction Temperatures of Thermocouples.—One simple method of automatically correcting for cold junction temperature is that devised by Darling, in which the control spring of the moving coil is coupled to a compound strip which coils or uncoils when cooled or heated, thereby moving the pointer over the scale.

The length of the spiral is such that an alteration of the given number of degrees in its temperature moves the pointer the same number of degrees

on the scale, or, in other words, the temperature scale of the pyrometer is identical with that of the spiral.

Numerous other methods for automatically compensating for cold junction temperature changes of thermocouples have been proposed and used in connection with millivoltmeters. One of the earliest was a bare resistance wire immersed in a column of mercury located near the cold junction of the thermocouple. An increase in temperature near the cold junction resulted in a rise of mercury column, which short-circuited more of the resistance wire, causing an increase in the potential difference across the millivoltmeter, and this compensated for the decreased electro-motive force of the thermocouple.

The method is open to the objection that the compensation is accurate at only one temperature of the hot junction, for the voltage change across the compensating resistance is a function, not only of the compensating resistance, but of also the current passing through it. As the current changes with the hot junction temperature, it is obvious that accurate compensation for cold junction temperature can be obtained only for one temperature of the hot junction.

Another device operating on the same principle consists of thin carbon

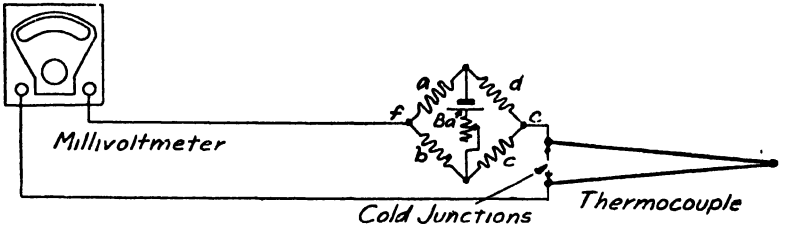


FIG. 47.—Wheatstone bridge arrangement for automatic compensation of cold junction temperature.

discs tightly packed in a porcelain cylinder which has a small coefficient of expansion. These are pressed together by a metal rod (zinc) possessing a large coefficient of expansion. As the temperature rises the rod expands and increases the pressure between the carbon discs, thus decreasing the resistance. The device is connected in series with the thermocouple and indicator. This method of compensation suffers from the same effect as the previous one in giving the desired compensation at only one hot junction temperature.

Fig. 47 shows another scheme of automatic cold junction compensation. The resistors *a*, *b*, *c*, and *d* are connected in the form of a Wheatstone bridge, as shown, and placed near the cold junction of the thermocouple. Three arms of this bridge are made of resistances having a zero temperature coefficient, such as manganin. The fourth arm is made of a metal having a high temperature coefficient, such as nickel. The resistances are adjusted so that they have equal resistances at some reference temperature, such as 0° C. The bridge consequently is balanced at this temperature, and no

difference of potential due to the battery B*a* appears at the terminals *e* and *f*. If the temperature of the cold junction changes and throws the bridge out of balance, this changes the E.M.F. across the terminals *e* and *f*, and if the coils are properly adjusted will exactly neutralise the change in E.M.F. at the cold junction of the thermocouple. The nickel resistance is made low in comparison to the total resistance in the millivolt circuit, so that resistance changes of the nickel coil do not materially change the total resistance in the millivoltmeter circuit. Consequently the compensation is

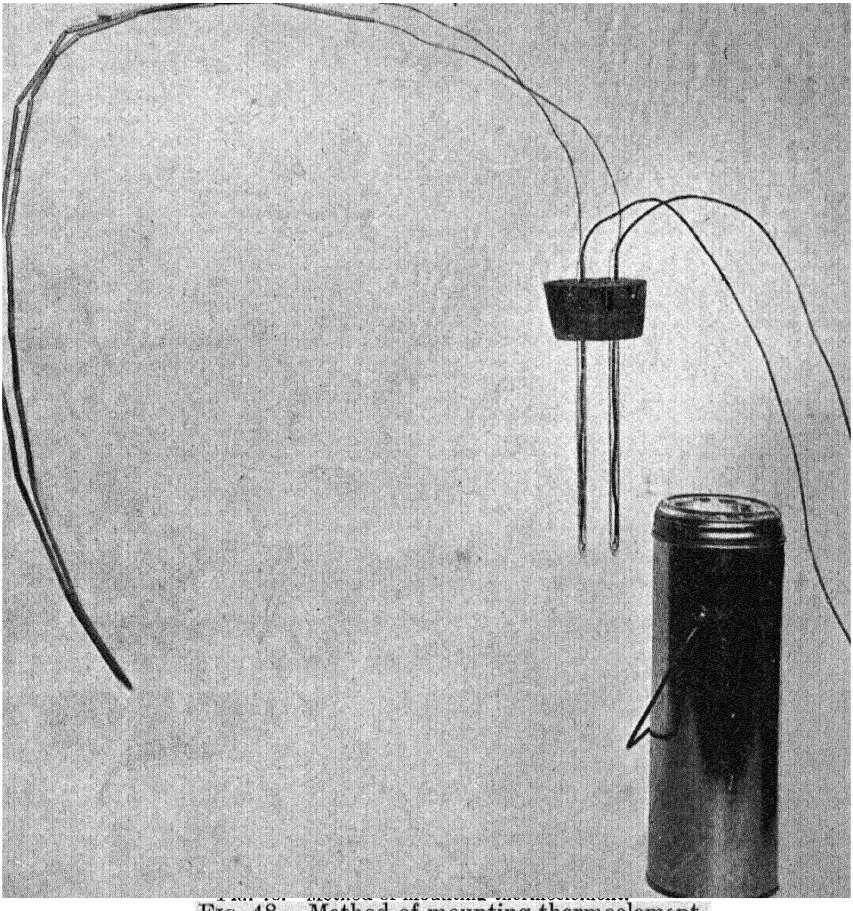


FIG. 48.—Method of mounting thermoelement.

practically correct for all temperatures of the hot junction, provided the voltage at the terminals of the bridge is kept constant. Changes in the voltage battery can be corrected for by means of a rheostat in the battery circuit.

The value of the resistance is so chosen that the scale starts at 0°, or at any other desired temperature.

(*a*) **Methods of Mounting Thermocouples for Laboratory Purposes.**—The choice of protecting sheath for a thermoelement is determined primarily by the conditions by which the pyrometer is to be used. For experimental work where there is no danger of contamination it is possible to use a thermoelement without a protecting tube, and thus diminish "lag" enormously. A convenient method of mounting a thermoelement is illustrated in Fig. 48.

The parts to be inserted in the hot region are insulated with capillaries of fireclay, while the junctions with the copper leads are inserted in glass tubes which are maintained at 0° C. by immersion in powdered ice.

The wide-necked form of commercial vacuum flask is a useful receptacle for the ice.

The two leads on the right of Fig. 48 are of thin guttapercha-covered copper, and are connected to the potentiometer or indicator.

Where there is risk of contamination of the element it is advisable to protect it by enclosing in a glazed porcelain tube.

For temperatures up to 500° C. hard glass capillaries and sheaths can be employed. Similarly, fused silica is available for temperatures up to 1,000° C. for prolonged periods.

A compact type of covering is shown in Fig. 49. Two silica capillaries are fused into a sheath terminating in a bulb at the bottc , a section of the tubing is shown by A.

The wires are threaded through from the end B, which is then sealed up with the junction enclosed in the bulb, as shown. Since the outside diameter is only about 5 millimetres, the couple can be inserted into a small space.

When necessary the tube can be bent with the wire *in situ* by means of the oxy-coal gas blowpipe.*

For work at comparatively low temperatures cotton or silk insulation is quite satisfactory, provided it is paraffined or shellac varnished.

Twin wire of iron-eureka is obtainable with the two wires separately insulated and enclosed in a double covering of cotton or silk. In this form the wires can be laid in grooves a few millimetres deep.

(*b*) **Methods of Mounting employed in Industrial Work.**—For industrial use it is generally necessary to enclose the thermocouple in a tube of glazed porcelain hemispherically closed at one end. The best grades of refractory porcelain have a melting-point above that of platinum, but since the material is porous to gases it cannot be used without a coating of glaze. The tubes are then serviceable to about 1,400° C. only.

The term porcelain comprises a variety of materials from vitrified porcelains to highly refractory porcelains. Vitrified porcelain will not stand rapid changes of temperature, but can be used continuously up to 1,200° C. Such tubes are usually gas-tight without being glazed, but are frequently glazed as an added precaution. Refractory porcelain tubes will stand up

* The thermoelement illustrated was designed for some experiments in which the distribution of temperature in a shallow bath of molten metal was required.

to 1,400° C., but prolonged exposure causes absorption of the softened glaze into the body of the tube.

Fused Silica Tubes.—Fused silica tubes can be used up to 1,000° C. in an oxidising atmosphere free from alkalis.

Prolonged exposure to temperatures above 1,000° C. causes devitrification: the material becomes crystallised, loses its mechanical strength, and is then permeable to gases. It appears that silica is slightly permeable

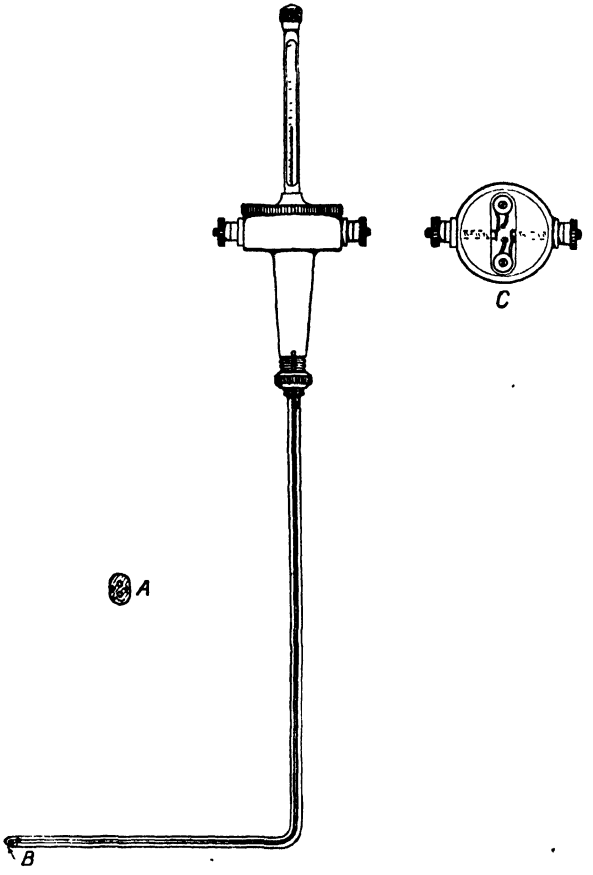


FIG. 49.—Diagram of mounting of a thermocouple for laboratory purposes.
A, section of tubing (sheath); B, junction enclosed in quartz bulb; C, section of head.

to hydrogen at high temperatures, which is a serious drawback, since the presence of hydrogen within the protecting tube of a platinum thermoelement results in the reduction of silica to silicon, which attacks the platinum.

The principal advantage of quartz as a thermoelement protection lies in its extremely low coefficient of thermal expansion which enables it to withstand violent temperature changes without fracture.

Alundum.—This is the trade name for a tubing composed of fused alumina (Al_2O_5) with fireclay as binder. The alumina is shrunk into a dense mass in an electric furnace and then ground and made into tubes by the addition of a little clay.

The unglazed tubing will stand 1,550° C., but is porous, consequently the tubes are frequently given a glaze coating, and this again covered with a layer of alumina.

This method permits the tubes to be used to temperatures exceeding the softening point of the glaze. The limiting temperature of the glazed tubes appears to be about the same as that of porcelain tubes.

Outer Protecting Tubes.—In industrial installations further mechanical protection is required by the porcelain or quartz sheath, and for this purpose carborundum, graphite, and a variety of metallic tubes are employed.

Carborundum.—Carborundum is an electric furnace product primarily composed of carbon and silicon. It is highly refractory and possesses many of the physical properties desirable in a protecting tube for the porcelain sheath.

When heated in an oxidising atmosphere the oxidisation of the silicon to silica begins at 1,200° C. At 1,500° C. the silica formed on the surface of the tube fuses and protects the tube from further oxidation. Very finely crystalline carborundum made into tubing known as "silfrax" is extensively used for furnace work. Carborundum tubes are permeable to gases, and are readily attacked by basic slag. Since carborundum reacts at high temperatures with practically all metals it is essential to employ an inner protecting tube around the thermocouple.

Graphite.—In a reducing atmosphere graphite tubes form an excellent protection to porcelain and quartz sheaths. They are particularly useful in the case of molten aluminium, which readily attacks porcelain.

Plumbago tubes, which are made of graphite and fireclay, will withstand much higher temperatures than fireclay alone, and are frequently used in permanent installations.

Iron and Steel.—The use of wrought iron or steel tubing as mechanical protection is very common in the industries. They are satisfactory up to about 900° C., and the cost of replacement is not a serious item.

Calorising the surface, which consists in impregnating the surface with aluminium, increases the resistance to oxidation, and so prolongs the life of the tube two- or three-fold.

Nichrome.—As a substitute for iron and steel tubes cast nichrome tubes are used to some extent. These tubes withstand oxidation remarkably well, so that their greater cost is more than balanced by their longer life. Up to the present it has not been found possible to draw nichrome into tubes, so castings have to be employed, and with these extreme care has to be exercised to avoid pinholes.

Molybdenum.—This element has a melting-point of about 2,500° C. Experiments have proved that it can be dipped into molten brass, copper,

etc., without being attacked, hence there are possibilities for this material when it becomes available on a commercial basis.

Zirconia.—Fused zirconia is an excellent refractory, and will probably be extensively used when the difficulties of manufacture have been overcome.

Electrical Insulation of the Wires.—The electrical insulation of the wires constituting a thermoelement can be effected by the use of porcelain or fireclay capillary tubing in the case of platinum thermocouples.

Base-metal couples of heavy wire are sometimes insulated with fireclay tubing. A slight fluxing of the oxides with the fireclay is noticeable on the constantan wire when heated to 1,000° C., but the nickel-chromium alloys seem to be free from this trouble.

The alternative method of insulating base-metal thermocouples is to employ asbestos string or tubing painted with a solution of carborundum, firesand, and sodium silicate mixed to a thick paste. When heated above 600° C. this insulation rapidly disintegrates. If the iron element of a thermocouple is protected this way and heated for some time to about 1,000° C.,

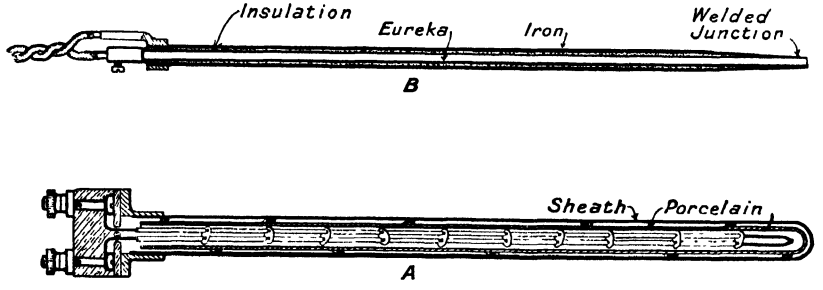


FIG. 50.—Diagram of standard methods of mounting thermocouples.

it will be found that the wire grows to nearly twice its original diameter, and can be easily broken by the fingers. In fact, the iron, asbestos, and carborundum will combine chemically, and no free iron will be left. Carborundum, of course, attacks metals vigorously at high temperatures.

Welding the Wires to form the Hot Junction End of a Thermoelement.—The practice of forming the hot junction by simply twisting the wires together is not to be recommended, particularly with oxidisable metals. The only satisfactory method is autogeneous welding.

Couples composed of platinum and its alloys should be jointed by simply butt welding in an oxy-coal gas blowpipe until a molten bead forms.

For base metal alloys such as nickel-chromium *v.* nickel-copper the following method has been found satisfactory :—

A rod of carbon or graphite, about 6 inches long by 1 inch square section, is heated to incandescence by the passage of a current of a few hundred amperes. In the centre of the carbon a hole is scooped and filled with anhydrous borax. The twisted end of the couple is immersed in the pool

of borax until a bead of molten metal forms around it. The current is then switched off the carbon and the couple withdrawn when cold.

A second method, which is rather more difficult to carry out than the first, is to employ a low voltage arc (about 30 volts); the couple wires form one pole and a stick of carbon the other.

A flux of borax or barium chloride should be used to prevent oxidation.

Notes on the Use of Differential Couples.—When small differences of temperature have to be measured a battery of thermoelements may be employed and connected together in series.

When the battery is composed of a large number of elements it may conveniently be divided into two equal groups of couples. Then, by connecting the two groups in opposition and inserting one end of each in ice, while the other is at room temperature, the E.M.F. should be zero, provided the two groups are exactly symmetrical and there are no internal short-circuits or leaks.

Generally in differential work the battery of thermoelements has to be made as compactly as possible and with the minimum of insulation consistent with safety. The copper wire, owing to its greater specific conductivity, may be of less diameter than the eureka wire without loss of sensitivity; a combination of 0·15 mm. diameter copper wire with 0·25 mm. diameter eureka being quite satisfactory. The junctions should be soldered with silver solder, using a little anhydrous borax as flux. This operation is facilitated by using a minute gas-jet rather than an ordinary blowpipe. Insulation of the bared parts is effected by repeatedly dipping into a solution of celluloid in acetone (freed from water); this coating is suitable for work at room or low temperatures.

The following method of insulating by means of hard rubber has been recommended by Adams:—Enough precipitated sulphur, or, still better, insoluble sulphur, is stirred with rather thick rubber cement (pure gum rubber dissolved in benzene or CS_2) to equal 20-25 per cent. of the solid rubber. The junctions are dipped in the mixture, and after drying in air are maintained at a temperature of 140° C. for 15 hours.

Standardisation of Thermocouples.—For low temperature work, up to about 450° C., the following fixed points are available for standardisation purposes:—

TABLE XIII.

Substance.	Boiling-point of the organic compound or freezing-point of the metal, °C.
Steam,	100°
Naphthalene,	$217{\cdot}9_6 + 0{\cdot}058\,(p. - 760)$
Tin,	231·9
Benzophenone,	$305{\cdot}9 + 0{\cdot}063\,(p. - 760)$
Aniline,	$184{\cdot}1 + 0{\cdot}05\,(p. - 760)$
Cadmium,	320·9
Zinc,	419·4
Sulphur,	$444{\cdot}5 + 0{\cdot}09\,(p. - 760)$

When great accuracy is not desired, the boiling-point of diphenylamine (302° C.) may replace that of benzophenone, being a less costly substance.

For temperatures above 450° C., the reference temperatures are freezing-points of metals or melting-points of salts.

Most of the commoner metals can be melted in small gas-fired crucible furnaces, the material of the crucible depending on the particular metal which is to be melted.

The value obtained for the melting-point should be in agreement with the freezing-point, and both should be independent of the rate of heating and the depth of immersion (within limits) of the thermoelement.

As a general rule, the end of the sheath protecting the thermoelement should be immersed to within about $\frac{1}{4}$ inch of the bottom of the crucible.

The chemical action of the surrounding atmosphere on the heated metal is an important factor, since the solution of the oxide or a gas in the molten metal lowers its freezing-point quite considerably.

For example, the solution of cuprous oxide to form the eutectic (3·5 per cent. of Cu_2O) in copper lowers the freezing-point by 20°, while the absorption of oxygen by silver has a similar influence on its freezing-point.

Metals which require a Reducing Atmosphere.—Antimony, silver, and copper must be melted in a reducing atmosphere. This can be readily effected by covering the metal with a layer of powdered graphite, and employing a graphite or salamander crucible. Another method of preventing oxidation is to pass a stream of coal gas over the surface.

The thermocouple should be carefully protected by means of a glazed porcelain tube. In the case of antimony, Day and Sosman recommend the addition of a thin sheath of graphite over the porcelain.

When an electric furnace is employed for heating, it is possible to maintain an atmosphere of carbon monoxide inside as a reducing agent.

The eutectics of

Aluminium copper, ...	542°
Aluminium iron, ...	649°
Nickel carbon, ...	1,330°

are sometimes used for standardising purposes. These should be melted in a reducing atmosphere. It is as well not to attempt to make up the alloy of eutectic composition, as, just failing to do this, the liquidus would not be distinguishable from the eutectic. By making the alloy so as to contain a few per cent. more of one of the metals than the eutectic alloy, the liquidus is easily distinguishable from the lower point, which is the one required.

Metals which require a Neutral Atmosphere.—The metals nickel and cobalt require a neutral or reducing atmosphere free from carbon compounds.

For nickel freezing-point determinations, the writer has found a refractory clay crucible quite satisfactory with fused borax as flux to prevent oxidation. The thermoelement should be protected by an unglazed fireclay or hard porcelain sheath.

A large-sized crucible of metal is desirable, and to diminish the rate

of fall of temperature the blowpipe should not be turned completely off when the cooling curve is taken.

Covering the exterior surface of the crucible with a layer of carborundum powder, admixed with a small percentage of fireclay, greatly increases its resistance to the cutting action of the blast flame.

Nickel melted under graphite in a salamander crucible was found to give an apparent freezing-point, which was very sharply defined at a temperature about 122° C. lower than the freezing-point of the pure metal. It is a well-known fact that molten nickel absorbs carbon and deposits some of it as graphite on cooling. Presumably this transition point is the freezing-point of the nickel-carbon eutectic.

Day and Sosman, in their melting-point determinations, employed an electric furnace with an atmosphere of hydrogen which was replaced by nitrogen previous to inserting the thermoelement, since the hydrogen would be occluded by the platinum at high temperatures. The nickel was contained in an unglazed porcelain crucible lined with 90 per cent. Al_2O_3 and 10 per cent. MgO.

They found that, in taking the freezing-point of nickel with oxide present, a fairly sharp halt was obtained 10° below the freezing-point, which may represent the eutectic of nickel and nickel oxide. The break disappeared when the nitrogen was replaced by hydrogen for a few minutes.

For cobalt "pure magnesia" crucibles had to be employed, otherwise the metal would penetrate through the lining and attack the porcelain beneath.

Glazed marquardt or pure magnesia tubes were used to protect the thermoelement, but they found it practically impossible to prevent some contamination of the thermocouple.

The difficulties in the determination of the freezing-points of nickel and cobalt are very considerable, owing to the high temperature required.

Metals which can be Melted in Air.—Zinc and gold require no special atmosphere; graphite crucibles should be used and the couple protected by a hard paste porcelain tube glazed.

But for its cost, gold would be an excellent fixed point to employ for standardising purposes, on account of its non-oxidisable nature and purity. It has, however, a tendency to volatilise.

If moderate accuracy is sufficient, the wire method may be used. In this method the junction between the couple wires is effected by a short length of gold wire, and the E.M.F. observed as the furnace rises slowly in temperature. The break in the circuit corresponds to the melting-point of the bridging metal.

Palladium.—The melting-point of this metal (1,553° C.) represents the upper limit of the gas thermometer at the present time. Owing to the cost of the metal the melting-point is generally obtained by the wire method as above described. The double-wound furnace shown in Fig. 76, p. 137, has been found to be very convenient for the calibration of thermocouples at the melting point of palladium.

Day and Sosman employed a charge of 120 to 200 grammes of the metal contained in a crucible of pure shrunk magnesia bound with magnesium chloride. The thermocouple was protected by a pure magnesia tube. The heating was effected in the internally wound furnace described in Chap. I.

The extreme temperature involved imposed a severe strain on platinum-wound furnaces. They found that the danger of contamination by the vapour of the palladium in such work was very considerable.

Melting- and Freezing-points of Salts.—The melting- and freezing-points of salts present greater practical difficulties to accurate determination than those of the metals at medium temperatures.

The latent heat of fusion of most salts is small and, as the solid salt is deposited on the pyrometer tube, it forms a poorly conducting layer, which renders the freezing-point less well defined than is the case with metals.

It is advisable to work with large quantities of material.

For the standardisation of base metal couples in the vicinity of 800° C., the freezing-point of common salt is very convenient.

The salt is contained in a large steel pot (lower end of a discarded gas cylinder), which is heated in a gas furnace.

The freezing-point of pure NaCl * is 801° C., while the ordinary domestic material has a freezing-point from 1° to 3° lower. The salt is very volatile at these temperatures.

It is, of course, necessary to use the couple directly immersed, without any sheath.

The sulphates and carbonates of sodium and potassium are not entirely satisfactory as fixed points. They are rapidly acted on by the water vapour and reducing gases of the furnace. Fused sulphates are slightly reduced to sulphides, and carbonates to hydrates, the magnitude of the change being dependent on the duration of the heating.

Heycock and Neville found that the freezing-point of sodium carbonate became lower the longer it was heated. The deterioration of the salt could be watched by looking into the crucible; the first two or three times the salt was fused it remained quite transparent, but afterwards it became opaque, in consequence of some chemical change.

They found that the sulphates were more stable, and no progressive change could be observed in the freezing-points.

For high-temperature salt-points platinum crucibles must be employed, with the thermocouple directly immersed in the salt, or if sheathed with glazed porcelain, this should be protected with a thin-walled platinum tube fitting it closely. This procedure was employed by them in their resistance thermometer work.

Since there is no metal freezing-point available in the region between copper (1,083° C.) and nickel (1,452° C.), attention has been directed towards the silicates to find some with melting-points in this gap. Jaeger has

* Pure salt guaranteed to be 99·98 per cent. purity is manufactured on a large scale for dairy purposes by C. Moore & Co., Lymm, near Warrington, Cheshire.

suggested the melting-point of lithium silicate (1,201° C.) as a transition-point for calibration purposes. The other two silicates, diopside (1,391° C.) and anorthite (1,549·5° C.), have already been referred to.

The following method was employed by White in the determination of the melting-points of silicates :—

About 3 grams of the salt was contained in a platinum crucible 10 mms. diameter and 18 mms. deep, which was suspended by a platinum sleeve from the open end of a porcelain tube (unglazed).

The supporting tube was surrounded with pure platinum foil to prevent contamination of the thermoelement by iridium vapour volatilised from the heating coil * of the furnace. The thermocouple dipped directly into the molten silicate.

It was found that the values of the melting-point were reproducible to about 1°. Freezing-points could not be determined, since the fused silicates undercooled considerably, sometimes to a glass, in which case, of course, no melting-point would be observed on reheating.

Formulæ for the Representation of the Temperature—E.M.F. Relationship.—When a large number of temperature observations have to be taken by means of a thermoelement, it is advisable to draw up a table on some such scheme as that shown below, by means of which the observed E.M.F. may be readily converted to temperatures.

The first step towards the construction of a table is to interpolate between the fixed points by means of an empirical equation.

Experience has shown that certain classes of curves represent closely the actual form of curve characteristic of the thermoelement.

For example, Adams found that the relationship—

$$E = 74{\cdot}672t - 13{,}892\,(1 - e^{-0{\cdot}00261t}),$$

where E is the E.M.F. in microvolts,

t ,, temp. ° C.,

e ,, base of the natural logarithms,

represented the temperature E.M.F. curve of a batch of copper-constantan correctly to a fraction of a microvolt over the range 0° to 350° C.

By a slight variation in the numerical coefficients the same equation could be employed for any other copper-constantan thermoelement.

In the case of Pt-PtRh couples no single equation, with a reasonable number of constants, has been found which will represent the curve over the whole range from 0° to 1,750° C.

Hence recourse has to be made to three equations covering overlapping sections.

1st, 0° to 400° C.

$$E = At + B(1 - e^{Ct})$$

2nd, 300° to 1,200° C.

$$E = -A' + B't + C't^2$$

3rd, 1,100° to 1,750° C.

$$E = -A'' + B''t + C''t^2$$

* Commercial platinum.

It should be ascertained, in a particular case, that there are no discontinuities in the slope of the curve at the points of transition from one section to another and any slight inequalities should be evened out by adjustment of the successive differences.

The formula proposed by Holman—

$$\log_{10} E = A \log_{10} t + B$$

where e = E.M.F. in microvolts,

t = temp. ° C.,

A and B constants,

is occasionally used, but does not represent the curve as accurately as the above.

From such equations a table can be calculated giving the temperature corresponding to every 100 microvolts or the E.M.F. corresponding to every 10°.

Typical specimens of such tables are shown below.

TABLE XIV.

Copper-constantan. Even hundreds of E system.

E (microvolts)	t °C.	1st diff
0	0	
100	2·60	2·60
200	5·17	2·57
300	7·73	2·56
400	10·28	2·55
500	12·81	2·53
600	15·33	2·52
etc.		

Pt-PtRh. Even tens of t system.

t.	E.	1st diff
0	0	
10	55	55
20	112	57
30	172	60
40	234	62
50	297	63
60	362	65
etc.		

In connection with the difference column, it is of interest to study the curves given by Adams and reproduced in Fig. 51 for the sensitivity of three kinds of couples at various temperatures.

The line for the Hoskins' alloys is broken in the region where the couple is not particularly suitable for temperature measurements.

Once a table has been calculated out it can serve as a basis of other tables for thermoelements of the same group by the aid of a " difference curve." It will be found that but little labour is involved in the construction of a second table, taking the first as basis and amending it in accordance with the requirements shown by the " difference curve."

Typical tables for platinum, rhodium, copper-constantan, and Hoskins' alloys have been published by Adams in " Tables and Curves for Use in Measuring Temperatures with Thermocouples " (Symposium on Pyrometry, American Instit. of Mining and Metall. Engineers), Sept. 1919, p. 165.

Calibration by Comparison with a Standard Thermoelement.—The method of standardising by freezing-point determinations above referred to should only be resorted to in the case of primary standards or as check points in case of doubt. The calibration of one couple by direct comparison with another is both simple and expeditious.

In the case of platinum alloy couples the usual procedure is as follows :—

The heavy porcelain sheath is removed and the wires insulated by capillary fireclay tubing or quartz (see Fig. 48). The junctions of the two couples are tied together by a piece of pure platinum wire and inserted at the mid-point of an electric furnace.

The couples are carried in a liner-tube supported from the cold ends of the furnace to avoid leakage from the heating circuit into that of the potentiometer, since at temperatures exceeding 1,000° C. the electric restivity of porcelain, quartz, etc., falls off rapidly with temperature, and quite minute electric leakages are noticeable when the apparatus is designed to measure E.M.F.'s of the order of one hundred-millionth that of the heating circuit (*i.e.*, 100 volts to 1 microvolt).

The Installation of a Potentiometer Outfit.—In the installation of a potentiometer for thermoelectric work two points require attention—

(1) The elimination of parasitic E.M.F.'s.

(2) The prevention of leakage into the potentiometer circuit from neighbouring lighting or furnace circuits.

Parasitic E.M.F.'s can be largely eliminated by a suitable choice of metals for the resistance-coils, binding-screws, and leads.

Manganin has a comparatively small thermal E.M.F. against copper, and copper terminals are now obtainable. All keys should be protected from temperature fluctuations.

It is obvious that a leakage current must enter the circuit at one point and leave at another, after passing through the galvanometer, if it is to produce errors in the observations.

Leakage into the potentiometer circuit can be detected by observing the deflection when the thermoelement is short-circuited.

When a thermocouple is used in connection with an electric furnace, the heating circuit should be provided with a reversal switch, and the deflection of the galvanometer spot on quickly changing over noted from time to time.

It is a difficult matter to provide an effective insulation of the thermo-

couple from the high voltage heating circuit of a furnace at temperatures exceeding 1,400° C., since the ionised atmosphere conducts slightly.

White recommends a system of shielding, by which a good conductor is interposed at all points between the potentiometer system and the source from which leakage occurs.

For details of the method of application of the equipotential shields, reference should be made to the original papers, a list of which is given at the end of the chapter.

Good electrical insulations of the apparatus should be the first consideration when leakage troubles occur.*

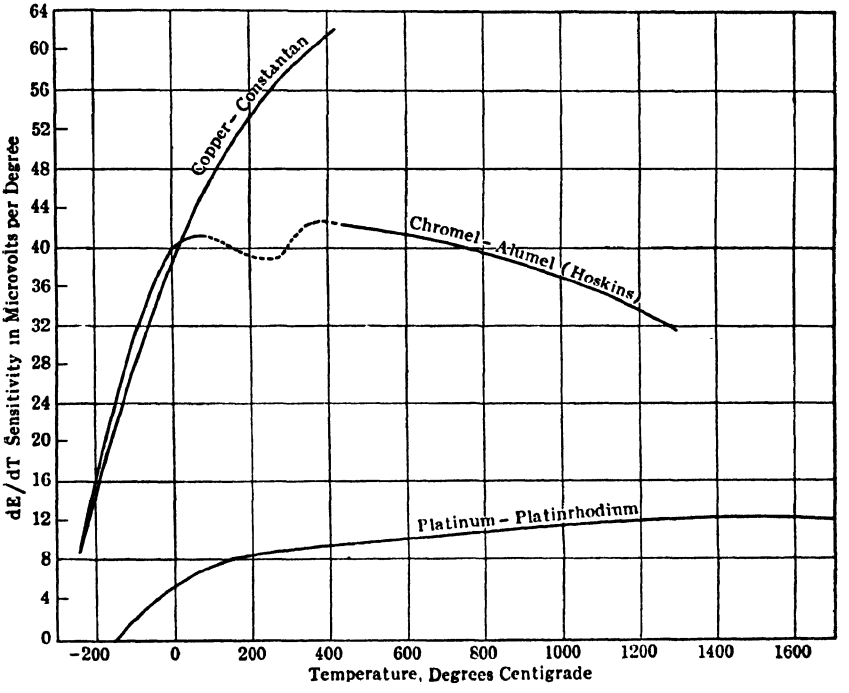


FIG. 51.—Sensitivity of three kinds of couples at various temperatures; $d\,E/d\,T$ in microvolts per degree, is plotted as a function of temperature (*Adams*).

Application of Thermoelements to the Measurement of Extremely Low Temperatures.—The use of thermoelements in practical work at low temperatures has been studied by Onnes and Dewar. Onnes favours constantan *v.* steel on account of the large E.M.F. developed. Dewar found cupro-nickel *v.* gold to be satisfactory down to liquid hydrogen temperatures.

During the course of his work Dewar observed some curious changes after exposure of the couples to low temperature.

If the junction had been soft-soldered the E.M.F. would not be reproducible after exposure to liquid hydrogen temperatures. Hard-soldering

* Alternating instead of continuous current is also advantageous for heating.

was found to be quite satisfactory. He found it advisable to cool the couple repeatedly to the lowest temperature before calibration in order to ensure that it had settled to an equilibrium state.

For low temperature work the couples are generally calibrated by a direct comparison with a hydrogen or helium gas thermometer.

A study of the curves in Fig. 51 shows that the thermoelectric method lacks sensitivity at low temperatures, and for any work requiring accurate measurements of temperature the resistance method should be employed.

Contamination Tests on Thermocouples.—Despite all the care taken in the use of platinum thermoelements at high temperatures, contamination troubles arise in the course of time. Even if the couple is carefully protected from external influences by sheathing in glazed tubing it is impossible to eliminate completely an internal source of trouble—namely, the volatilisation of rhodium or iridium from the alloy limb on to pure platinum limb.

It must be remembered that recalibration of a suspected thermocouple will not show whether the portion inserted in the furnace is contaminated or not. Should the affected length be within the uniformly heated region, it is immaterial what the composition of the wire may be.

A variety of methods have been devised for detecting the contaminated region of a thermoelement. The simplest is to stretch the wire between supports, connect the ends to a galvanometer, and run a small Bunsen flame along beneath. In the contaminated region the galvanometer will show marked deflection from the normal position. Each limb of thermoelement should be tested separately.

There is no known method of restoring a contaminated couple to its original state, but an improvement can sometimes be effected by prolonged heating and fluxing the surface with borax. The only safe policy is to cut off the contaminated portions.

Base-metal thermocouples are particularly liable to develop heterogeneity after prolonged exposure to high temperatures, this being usually due to structural changes in the alloy. When this occurs the readings obtained will depend upon the depth of immersion if the affected part happens to be in a region where there are temperature gradients. Hence it is advisable to keep a check on a pyrometer permanently installed by inserting a standard couple into the furnace alongside it with the hot junctions in close proximity. Observations should be taken at a series of temperatures. If the conditions prevailing in the furnace are fairly definite and the heterogeneity effect small, consistent values should be obtained for the difference between the two couples. If, however, the differences are of variable magnitude and not reproducible it would be advisable to discard the suspected couple.

It is, of course, useless to expect the same accuracy in a test of this character as would be obtained under laboratory conditions. But the data should prove the accuracy of the temperature observations. It is advisable to use as check couple one of small cross-section and protected by a thin tube. It would then serve to show whether the depth of immersion of the

working couple is sufficient. When heavy iron protecting tubes are employed it may happen that the conduction along the tube is so considerable as to keep the temperature of the hot junction below that of the region in which it is placed.

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CHAPTER V.

THE "FOURTH-POWER" LAW OF RADIATION AND TOTAL RADIATION PYROMETERS.

At temperatures exceeding 1,300° C. the practical difficulties encountered in the use of thermoelements, resistance thermometers and gas thermometers are very considerable, even under the favourable conditions prevailing in the laboratory. For industrial work the difficulties are vastly greater and other methods have to be resorted to, such as those based on the laws of radiation. With pyrometers of the radiation type it is not necessary to subject any portion of the instrument to the temperature of the furnace, and there is no upper limit to the temperature which can be measured.

The present chapter will be devoted to the consideration of the fundamental law of radiation—that connecting the total radiation and temperature—and to pyrometers based on this law.

The Stefan-Boltzmann Law.—The earliest suggestion of a simple relation connecting the radiation of a surface and its temperature was that of Stefan in 1879. He observed that the experimental results of Tyndall on the heat loss from a platinum wire at 1,200° C. and at 525° C. were in the ratio of 11·7 to 1, while the ratio of the fourth powers of these two temperatures (in absolute measure) was 11·6 to 1.

From this he concluded that the total radiation is proportional to the fourth power of the absolute temperature.

Subsequent investigations, however, showed that this generalisation was too wide, the law being valid for "full radiators," and that metallic surfaces of high reflecting power obeyed a different law. Platinum, for example, radiates at a rate more nearly proportional to the fifth power of the absolute temperature. Tyndall's temperature scale was probably incorrect, and the loss by convection was not separated from the radiation loss.

In 1884 Boltzmann gave a theoretical proof of the fourth-power law based on thermodynamic principles and Maxwell's electromagnetic theory of light. He pointed out that the law was only valid for an "ideal black body." Kirchoff defines a "black body" as one which has the property of allowing all incident rays to enter without surface reflection and not allowing them to leave again.*

The radiation emitted by such a body would possess a character independent of the properties of any particular substance and would be identical

* See "Theory of Heat Radiation," *Planck Trans.* by Masius.

with the radiation within a uniformly heated enclosure. This conception of a perfect black surface and its practical realisation, by means of an enclosure at a uniform temperature, is due to Kirchhoff.

He demonstrated conclusively that the radiation issuing from a small hole in a uniformly heated enclosure would be "full radiation" for that temperature, such as would be emitted by an ideal black body.

The simplicity of the law and the fact that most industrial furnaces, etc., are fair approximations to uniform temperature enclosures have been factors of immense service in the development of high-temperature pyrometry.

The formal statement of the Stefan-Boltzmann law is

$$S = \sigma (\theta^4 - \theta_0^4)$$

where S is the energy per sq. cm. per sec.;

σ a numerical constant the experimental value of which is $1{\cdot}279 \times 10^{-12}$ gm. cals. per sec. per cm.^{2};

θ the absolute temperature of the surface;

θ_0 „ „ „ surroundings receiving the radiation.

It will be observed that as a method of defining absolute temperature the law is independent of the specific properties of any particular substance; the ideal black body in this respect playing the same *rôle* as that of a perfect gas in the definition of the gas scale.

A comparison at one temperature above zero with the gas scale would suffice to determine σ and hence connect the two scales.

Since, however, Boltzmann's demonstration involves an imaginary thermodynamic cycle with radiation as working fluid, it is necessary to confirm the theoretical deduction by experimental observations over an extended temperature range. Shortly after its formulation the law was submitted to test by various investigators; the most comprehensive series of experiments were carried out by Lummer and Pringsheim, who investigated the radiation from a "black body" enclosure over the temperature range 100° to 1,300° C.

Lummer and Pringsheim's Experiments.—For the measurement of the radiation the authors employed a modified form of Langley bolometer—an instrument depending on the change of electrical resistance of platinum with temperature. Details of the instrument are given later.

The general disposition of the apparatus is shown in Fig. 52.

A was a hollow vessel containing boiling water. This source of radiation was used as a standard of reference for calibrating the bolometer from time to time, since only by this means could the variations produced by changes in the battery current and galvanometer sensitivity be eliminated.

The radiation could be cut off from the bolometer by means of a water-cooled shutter.

The "black body" C was employed for the range of temperature from 200° to 600° C. It consisted of a hollow sphere of copper blackened inside

with platinum black and contained in a bath of well-stirred molten salt. This salt bath could be maintained at any desired temperature by regulating the flame. The temperature was measured by means of a high-range mercury thermometer and a thermoelement.

The procedure in carrying out the observations was as follows :—

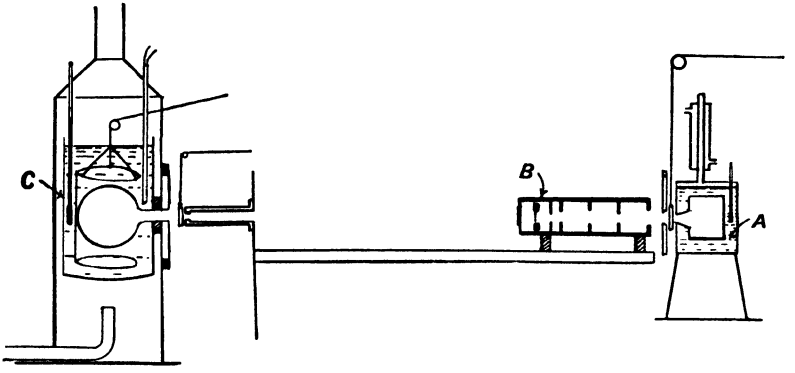


FIG. 52.—Diagram of apparatus for the range 200° to 600° C.

A, vessel with boiling water; B, bolometer; C, molten salt bath around the hollow sphere (black body enclosure).

The bath was heated up to the desired temperature and maintained steady; then the water-cooled shutter was raised to allow radiation to fall on the receiving face of the bolometer. When the galvanometer deflection had attained its maximum value the shutter was lowered and galvanometer zero redetermined; if it differed slightly from the previous value the mean was taken.

For higher temperatures, from 600° to 1,300° C., the construction of the "black body" is shown in Fig. 53. D was an iron cylinder (coated inside with platinum black) enclosed in a double-walled gas muffle. The

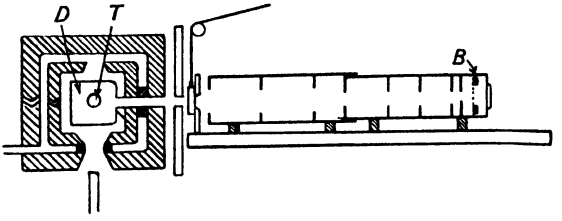


FIG. 53.—Diagram showing construction of "black body," for the range 600° to 1,300° C.

D, iron cylinder, "black body" enclosure; T, porcelain tube carrying thermoelement; B, bolometer.

temperature of the interior of the iron cylinder was obtained by a thermoelement enclosed in a porcelain tube T passing through the furnace.

The Bolometer.—Essentially this is a Wheatstone's bridge, the four arms of which consist of grids of thin platinum foil similar in all respects. The method of connecting up the grids is shown in Fig. 54. Grids 1 and 3 are in the opposite arms of the bridge, and the strips of 3 are set to receive the radiation passing through the gaps of 1. The other two grids, 2 and 4, are similarly disposed, but shielded from radiation by a box.

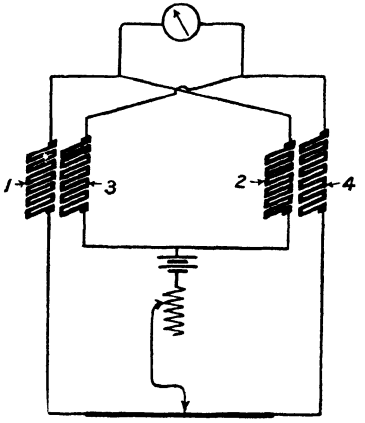


FIG. 54.—Diagram of the connection of the resistance grids in a bolometer.

To prevent wandering of the galvanometer zero, the disposition must be as symmetrical as possible and the whole instrument enclosed in a well-lagged box provided with diaphragms to cut down the radiation, falling on the absorbing surface, to a parallel beam of about 16 mms. in diameter.

The grids are of foil from one to two thousandths of a millimetre thick and with a resistance of about 60 ohms each.

The method of constructing such exceedingly thin conductors is worthy of notice. A sheet of platinum is welded to a thick sheet of silver and both are rolled down. The grid is then punched out and attached to a hollow slate frame. When thus supported the silver is dissolved by nitric acid from the straight limbs, the elbows on the slate being protected by varnish.

The appearance of the face of one of the grids after coating with platinum black is shown in Fig. 55, while Fig. 56 is a view of the back surface.

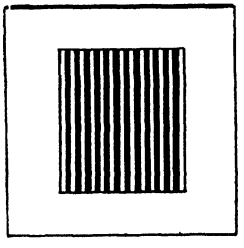


FIG. 55.—Front view of a grid, after being coated with platinum black.

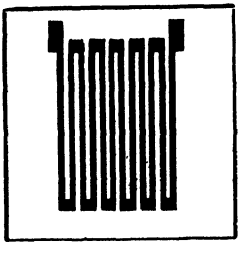


FIG. 56.—View of the back surface of grid, after coating with platinum black.

Since the quantity of radiation received varied as the difference of the fourth powers of the absolute temperatures of the radiator and receiver, it was necessary to vary the sensitivity of the bolometer in order to keep the galvanometer deflections within measurable limits. Two means of effecting this were employed: (1) variation of the sensitivity of the Wheat-

stone bridge by changing the battery current; (2) alteration of the distance between the "black body" and the bolometer. Theoretically the quantity of radiation received per unit time, by unit area, at a distance r from a point source, varies inversely as r^2. Lummer and Pringsheim ascertained that their experimental arrangements complied with this theoretical condition, by taking observations at varying distances between the "black body" and bolometer. It was found that the galvanometer deflections varied inversely as the square of the distance.

The observations were all reduced to a common unit (arbitrary), based on the radiation from the "black body" at 100° C. at a standard distance of 633 mms.

If d is the deviation of the needle for "black body" at absolute temperature θ, and k a constant, the mean value of which for their instrument is 123·8.

$$\text{Then } d = k\,(\theta^4 - 290^4)$$

where 290° is the absolute temperature of the water-cooled shutter (*i.e.*, 17° C.).

In Table XV. the experimental observations are compared with values calculated from the fourth-power law. The calculated temperatures are obtained by taking the mean value of k.

TABLE XV.

Temp (° abs C.) of black body.	Deflection (reduced).	K × 10^{10}.	$\theta_{calc.}$	$\theta_{obs.} - \theta_{calc.}$
373·1	153	127	374·6	− 1·5
492·5	638	124	492·0	+ 0·5
723	3,320	124·8	724·3	− 1·3
745	3,810	126·6	749·1	− 4·1
*789	4,440	(116·7)	778·0	+11·0
810	5,150	121·6	806·5	+ 3·5
868	6,910	123·3	867·1	+ 0·9
*1,092	16,400	(115·9)	1,074	+18
*1,112	17,700	(116·3)	1,095	+17
1,378	44,700	124·2	1,379	− 1
1,470	57,400	123·1	1,468	+ 2
1,497	60,600	120·9	1,488	+ 9
1,535	67,800	122·3	1,531	+ 4

Between 100° C. and 1,000° C. the deviation of the calculated from the observed temperatures are small, of the order of 3°, and exhibit no systematic variation. Between 1,000° C. and 1,360° C. the discrepancies are greater, and the observed values are systematically larger than the calculated. It should be remembered, however, that their temperature scale is based on

* These experiments were carried out with the gas furnace at temperatures overlapping those obtained with the salt bath. The large discrepancies are due to lack of uniformity of temperatures with a small flame. It will be seen that the observation at 789° C. is eliminated by observations 4, 6, and 7 with the nitrate bath.

the gas thermometer work of Holborn and Day, and this extended to 1,150° C. only. Beyond this point the values are based on extrapolation of the E.M.F.-temperature curves of thermocouples, a procedure which has since been shown to lead to erroneous results. Up to 1,100° C. it is probable that the temperature scale of Day and Holborn is reliable to about 3°. Consequently Lummer and Pringsheim's experiments establish the validity of the fourth-power law to 1,150° C. to the same order of accuracy as the gas scale was known at that time.

Fourth-Power Law between 1,063° C. and 1,549° C.—In an investigation, whose primary object was the comparison of the "optical scale," based on Wien's distribution law, and the "total radiation" scale, based on the fourth-power law, Mendenhall and Forsythe checked the Stefan-Boltzmann law at the two temperatures 1,063° C. and 1,549° C. These temperatures are the melting-points of gold and palladium* respectively as determined by Day and Sosman.

The comparison was effected in an indirect method. The melting-points of gold and palladium were observed in terms of the scale of a certain optical pyrometer under "black body" conditions. The temperature of a carbon tube furnace could then be maintained at these two temperatures by observations with the optical pyrometer, which merely served as a transfer instrument The apparatus for verifying the fourth-power law is shown in Fig. 57.

The "black body" is the graphite tube T, 30 cms. long, 14 mms. inside diameter, and 3 mms. wall thickness. A graphite diaphragm G is placed 1 cm. out of centre, the left-hand segment being used as "black body." The coaxial tubes H and K are merely to reduce the heat loss by radiation, etc.

The apparatus was water-cooled as shown; the total radiation thermopile P being protected from stray radiation by water-cooled diaphragms, while a movable water-cooled shutter Q contained the limiting aperture. The geometry of the apparatus was so arranged that radiation from the graphite diaphragm G alone entered the thermopile. A motor M, movable by means of a rod V, carried a sector S of definite aperture on its shaft. By a movement of the rod the motor could be swung up and the rotating sector placed in front of the thermopile so that the radiation from the furnace was reduced in a known ratio, depending on the clear aperture of the sector.

The thermopile consisted of a single Bi-Sb and Sb-Cd alloys couple, the "hot" junction being soldered to a very light receiving disc of silver foil 3 mms. in diameter, a similar disc being attached to each cold junction, where the alloys joined copper leads. The silver disc "hot" junction was blackened with acetylene smoke and mounted at the centre of a hemispherical concave mirror, so as to make the absorption as perfect as possible. The thermocouple was directly connected with a low-resistance galvanometer, a resistance box being connected in series to control the sensibility.

Special attention was given to the elimination of any possible error

*At the present time higher values are ascribed to the above fixed points.

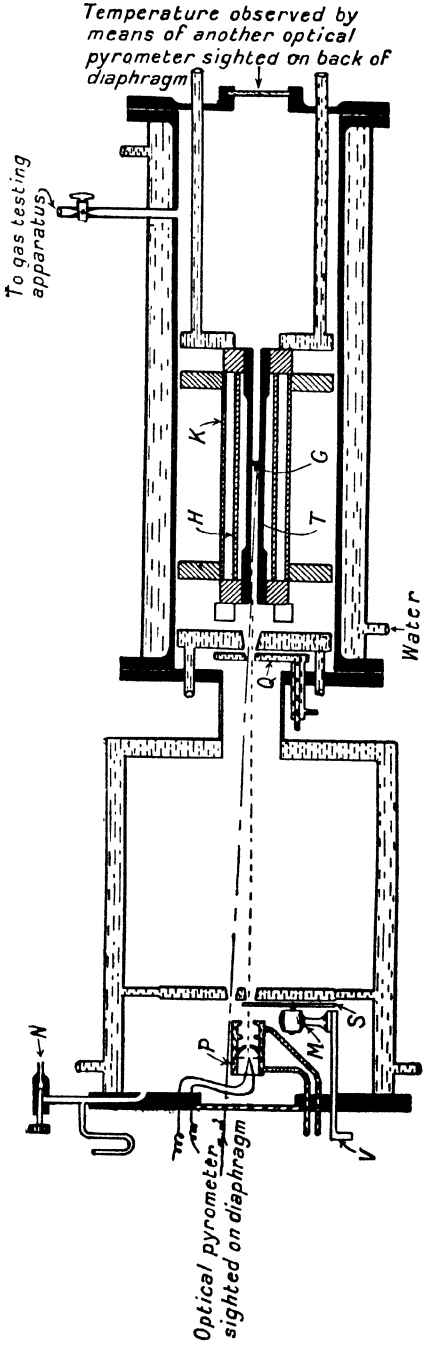


FIG. 57.—Diagram of apparatus employed for the verification of the fourth-power law.

T, graphite tube; K and H, co-axial tubes to reduce heat loss; G, graphite diaphragm; P, water-cooled radiation thermopile; Q, movable water-cooled shutter; M, motor carrying rotating sector; S, disc with sector opening; V, rod to swing motor and discs out of line of sight; N, pin valve to control ingress of nitrogen to obtain steady pressure.

due to absorption of radiation by the gases inside the furnace. With a hot object, such as graphite, it is impossible to obtain a perfect vacuum, and fluctuations of pressure would have had a serious influence on the sensibility of the thermopile.

During the observations a steady pressure (from 5 to 15 mms. of mercury) was maintained in the apparatus by controlling a valve governing the nitrogen supply; the pressure could be maintained constant within 0·2 mm. by careful regulation; a Fluess and Gaede pump steadily exhausting at the other end.

To ascertain whether the residual gas exerted appreciable absorption on the radiation, samples were drawn off from time to time to a side tube and the deflections of an auxiliary thermopile read with and without the gas, employing a Nernst filament as radiator; the authors claim that they could detect such effect if it amounted to $\frac{1}{10}$ per cent.

Theory of the Sectored Disc.—The object of a sectored disc is to cut down the radiation by a definite fraction so that the same galvanometer deflection is obtained for two different temperatures of the radiator or "black body."

Suppose the deflection x is obtained when radiation from an object at absolute temperature T_1 is received through a clear aperture sector, and the same deflection obtained for temperature T_2 with a rotating sector having transmission ratio S (where $S < 1$).

$$\text{Then } x = K A T_1^4 \text{ for the first condition}$$
$$\text{and } x = K S A T_2^4 \quad ,, \quad \text{second} \quad ,,$$
$$\text{Hence } T_1^4 = S T_2^4 \text{ or } T_2 = \frac{T_1}{\sqrt[4]{S}}.$$

In practice it was found impossible to bring the two deflections to absolutely the same value, consequently it was assumed that the deflections were proportional to the total energy in the two cases.

The aperture in the sector was cut in the ratio $(1336/1822)^4$, where 1,336 is the melting-point of gold and 1822 the melting-point of palladium, in absolute temperatures.

Consequently, the ratio of the galvanometer deflections at these two temperatures, if the fourth-power law was obeyed, should be unity.

From twelve comparisons the observed mean value was 1·001. The maximum value of the ratio found was 1·007 and the minimum 0·998. A few typical observations are shown in Table XVI.

This indicates an agreement well within the possible limits of experimental error of $\pm$ 0·5 per cent. at each of the two temperatures.

All the experimental evidence available supports the conclusion that the Stefan-Boltzmann law is valid over the entire temperature range covered by the gas thermometer. It may, therefore, be employed with confidence, in view of its plausible theoretical foundation, as the basis of methods for the evaluation of high temperatures.

TABLE XVI.

Deflection at 1063° C.	Deflection at 1549° C., with sectored Aperture.	Ratio column 2 to column 1.
29·28	29·33	1·002
29·08	29 17	1·003
29·33	29·33	1·000
28·29	28·27	0·999
28·27	28·25	0·999
		Mean 1·001

Total Radiation Pyrometers.—Pyrometers based on the fourth-power law for the measurement of high temperatures are merely thermopiles so arranged that the instruments are (1) direct reading, (2) robust, (3) quick in action, (4) and have arrangements to render the readings independent of the distance between pyrometer and hot body, within certain limits.

Féry's Telescope Pyrometer.—Féry appears to have been the first to evolve a practical form of pyrometer based on the Stefan-Boltzmann law, and capable of measuring temperatures between 500° C. and 1,500° C.

In the early types the instrument consisted of a telescope having a minute thermocouple connected to a sensitive portable galvanometer. The hot junction and the source of radiation were brought to the conjugate foci of the lens by focussing in the usual manner.

The difficulty with this type was the lens, which had to be transparent for both the visible and infra-red radiation.

Fluorite was found satisfactory for temperatures above 900° C., since it possesses a nearly constant coefficient of absorption throughout the spectrum. The indications of the instrument, however, did not follow the fourth-power law owing to the fact that fluorite has an absorption in the infra red at about 6 μ, and is not transparent for wave lengths greater than 10 μ.

For industrial work fluorite was too costly, so glass was employed and the instrument calibrated empirically over the working range.

The ordinary varieties of glass are opaque for wave lengths greater than 3 μ.

Féry's Mirror Pyrometer.—These difficulties were avoided by the use of a concave mirror to collect the radiation.

Fig. 58 represents a modern type of instrument. The mirror M is capable of being racked backwards and forwards to focus the radiation on the thermo-couple receiver at S. The cold junctions of the couple are shielded from radiation by the tongue T and a box surrounding both the couple and the inclined mirrors X.

To enable the observer to focus accurately the radiation on to the hot junction, in the same plane as this, two small semi-circular mirrors, inclined

to one another at an angle of 5° to 10°, are mounted in the thermocouple box, an opening of about 1·5 mm. at the centre of the mirrors forming the limiting diaphragm immediately in front of the couple. Then, unless the image of a straight line viewed through E is exactly in the same plane as the two inclined mirrors, it will appear broken at the plane of intersection

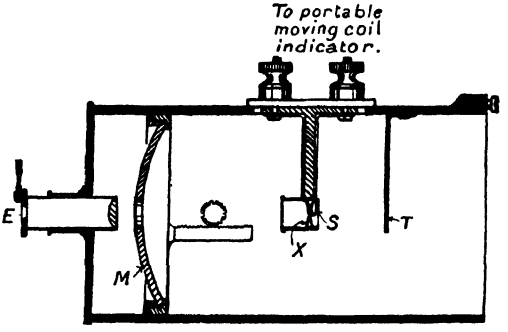


FIG. 58.—Diagram of Féry's mirror pyrometer.

M, mirror (nickel-plated); S, hot junction of thermocouple; T, projecting metal tongue to shield thermocouple from direct radiation; X, inclined mirrors.

of these mirrors. Fig. 59 illustrates the paths of the rays producing the distorted images. The observer moves the concave mirror until the relative displacement of the two halves of the image disappears.

In the earlier forms of this instrument the mirror was of glass silvered

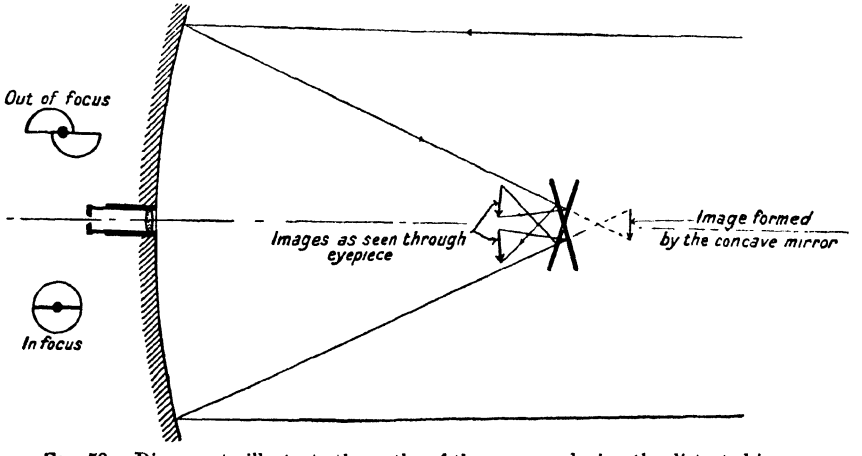


FIG. 59.—Diagram to illustrate the paths of the rays producing the distorted image.

on the back. Since glass is a very good reflector of the infra-red, the heat rays were reflected in part from the front air-glass surface and in part from the back glass-silver surface. The two groups of rays were brought to the same focal point by making the radii of curvature of the two surfaces slightly

different. If, however, the thickness of the glass is small, 1 to 2 mms., the same radius of curvature can be used for the two surfaces without appreciable error.

Later instruments have a glass mirror with a gold deposit on the front surface, others gold or nickel on copper.

Independence of Distance.—So long as the image of the hot object formed by the concave mirror is sufficiently large to overlap the sensitive thermo-element, then it is the intensity of the heat image and not the total heat reflected that is measured by the instrument. Now, it can be easily shown that this intensity is independent of the distance from the hot object. If, for example, the distance between the instrument and the hot object is doubled, then the total amount of heat received by the concave mirror is reduced to one-fourth, but the area which the image covers is simultaneously reduced to one-fourth, so that the actual heat intensity of the image remains constant.

To limit the cone of radiation falling on the disc attached to the hot junction, a small diaphragm is fixed on the front of the box containing the couple and mirrors. In other forms the box is dispensed with and the inclined mirrors used as diaphragm, the disc being placed a millimetre or so below the plane of the mirrors, which in all types are cut away opposite the disc.

Relation between Size of Object and the Distance for the Féry Type of Pyrometer.—It is a simple matter to calculate the minimum size of object required by the geometry of the Féry optical system.

The relation between the sizes of the object and image formed by a concave mirror is $O = I\left(\frac{u}{f} - 1\right)$, where O is the diameter of the object, I that of the image, u the distance from the object to the mirror, f the focal length.

For the ordinary types of Féry's the aperture in the diaphragm in front of the receiving disc is about 1·5 mms. diameter, f the focal length about 7·6 cms.

The table below, due to Burgess and Foote, gives the size of source for various distances assuming the above data.

TABLE XVII.

u (cms.).	Diameter source (cms.)
70	1·2
80	1·4
100	1·8
150	3·1
200	4·2
300	6·3
500	10·7

Extension of the Temperature Range by the Use of Diaphragms.—Instruments are often provided with a second scale extending over a higher range of temperature. This is effected by the addition of a diaphragm over the front of a pyrometer, which cuts down the radiation by a definite fraction. While theoretically the "law" * of the instrument should be unaffected by the addition of the diaphragm, it is generally found that the index is not exactly the same with and without the diaphragm. The change is probably due to secondary radiation from the diaphragm, which necessarily becomes heated by exposure to direct radiation from the hot object, and also to the change in the distribution of the air currents within the case, caused by the presence of the diaphragm.

The extrapolation of the scale of temperature is effected by assuming the validity of the "law" of the instrument as determined by experiments over the range of temperature measurable with thermoelements.

Féry "Spiral" Pyrometer.—The construction of this instrument resembles

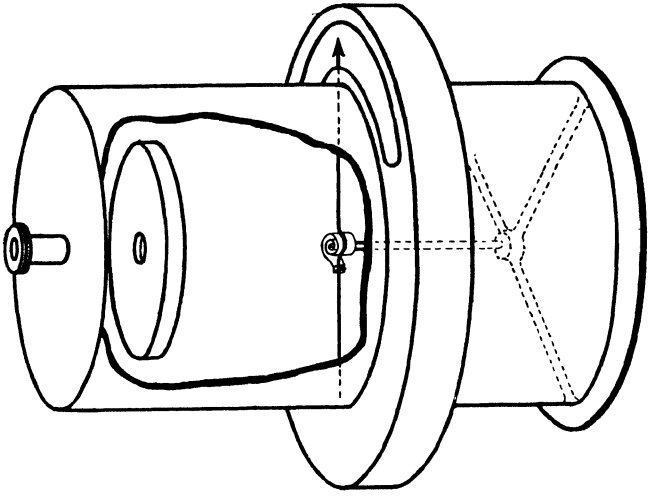


FIG. 60.—Féry spiral pyrometer.

that of the thermoelectric type, except that the couple is replaced by a bimetallic spring spiral (Fig. 60) carrying an aluminium pointer, which is moved over a dial, graduated in degrees Centigrade, under the influence of the differential expansion and uncoiling of the spring when radiation is concentrated upon it. In some of the instruments the spring is trimetallic, the thermal expansion coefficient of the intermediate metal being itself intermediate to that of the two outer metals. Thus, gold, platinum, and invar have been employed. The spiral is similar to that used in the thermometer of Breguet. A strip 0·02 mm. thick and 2 mms. wide is coiled into a spiral 2 mms. in diameter. The centre of the spiral is connected by a shank to a small disc, and on this disc is usually mounted the pointer.

* Value of the index in $E = a T^b$.

(In Fig. 60 a slightly different mounting is shown. The shank is fixed and the pointer is mounted at the other end of the spiral.) Usually a mirror is placed behind the spiral, so that the radiation which passes through and between the turns of the spiral is reflected back upon it.

It is of interest to consider the method of spacing of the temperature scale engraved on the instrument. Suppose that the scale is first placed linearly or in terms of angular deflection of the pointer :—

Let d = angular deflection,
T_0 = absolute temperature of spiral,
T = absolute temperature of furnace,
E = energy falling upon spiral.

The angular deflection of the pointer is approximately proportional to the temperature of the spiral ; the temperature of the spiral is approximately proportional to the energy absorbed by it ; this energy is approximately proportional to the fourth power of the absolute temperature of the furnace ; or

$$d \propto T_0 \propto E \propto T^4.$$

Hence,
$$d = \text{const. } T^4.$$

Hence, determining the deflection corresponding to any one furnace temperature fixes the constant in the above relation and permits the computation to all other deflections. Actually, the pyrometer does not exactly follow the fourth-power law, but rather the relation

$$d = c\,T^b,$$

where b is an empirical constant slightly different from 4.

If a calibration is made at a number of different temperatures the exponent b may be determined from the slope of the best straight line drawn through the observations, plotting log d against log T. The spiral pyrometer has an especial advantage in being self-contained, requiring no accessories such as lead wires, galvanometer, etc., but its accuracy is not equal to that of the thermoelectric instruments. The readings depend somewhat upon the position in which the pyrometer is held and upon the previous condition of the instrument. For example, tilting the case to the right or left alters the reading, and slightly different readings may be expected when (1) the pyrometer has been sighted upon a source at a higher temperature immediately before taking a certain reading, and (2) when the initial source sighted upon was at a lower temperature.

The Foster Fixed-focus Pyrometer.—The construction of this pyrometer will be understood from Fig. 61.

The receiving disc on the couple and the front diaphragm D of the pyrometer are located at the conjugate foci of the mirror M. Then so long as the cone A O B is filled by the radiation from the hot object the readings are independent of the distance.

The position of the point O is marked by the wing nut on the telescope

tube. The angle is made such that the diameter of the source sighted upon must be at least one-tenth (or in some instruments one-eighth) the distance from the source to the wing nut.

The rather large area required to sight upon is occasionally a disadvantage.

Various precautions are taken to prevent secondary effects, such as stray radiation from the sides of the tube, etc., from influencing the readings.

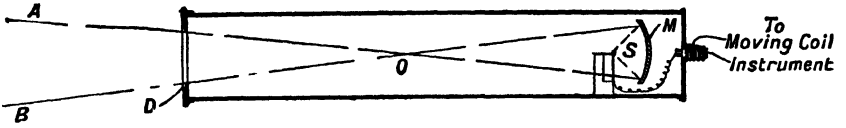


FIG. 61.—Diagram illustrating construction of the Foster fixed-focus pyrometer.
A and B, limiting value of cone of radiation; D, front diaphragm; M, concave mirror; S, receiving disc on end of thermocouple.

This is generally effected by additional diaphragms in the tube, and also by cutting a coarse screw-thread on the internal surface.

The Thwing Pyrometer is somewhat similar to the Foster, but has a cone instead of a concave mirror. The receiving disc of the couple is situated at the apex.

Radiation from the furnace enters the diaphragm and falls upon the hollow conical mirror. The hot junction of a minute thermocouple is located at the apex of the cone, and the cold junctions are outside. By multiple reflection along the sides of the conical mirror the radiation is finally concentrated upon the hot junction of the couple.

For permanent installations, the tube is ventilated and has several extra

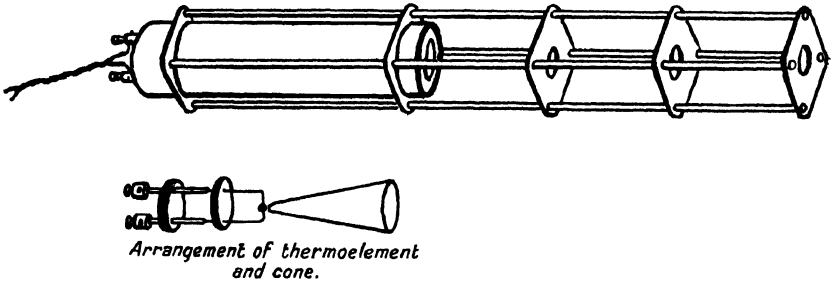


FIG. 62.—Thwing total radiation pyrometer.

diaphragms to prevent the local heating of the instrument and stray radiation reaching the couple.

Portable Total Radiation Pyrometer.—A form of total radiation pyrometer has recently been developed in which the moving coil indicator is an integral part of the telescope.

The radiation from the hot object is concentrated on to a minute thermo-junction contained in an evacuated glass bulb.

The instrument is of the fixed-focus type, and all that the observer has to do is to sight the telescope on to the furnace and ensure that the image completely covers the disc of the receiving thermojunction, which occupies the centre of the field.

Normally the moving coil system of the indicator is clamped, and can be released by depressing a button.

When the observer is sighting on the hot object the button is pressed and the moving coil allowed to swing to its equilibrium position under the influence of the electromotive force generated at the thermojunction.

On releasing the press button the coil is clamped in this position, and thus the observer can read the position of the pointer on the scale at leisure.

Whipple has introduced a modification of the Féry pyrometer. In this type a closed tube of salamander or fireclay is inserted into the furnace or molten metal, and the radiation from the hot end focussed on a minute thermocouple ; the instrument being of the fixed focus type.

For taking temperatures of molten metals, the radiation from which departs considerably from full radiation, and for furnaces with a smoky atmosphere, this form of pyrometer has proved to be of considerable service. The drawback of this type for very high temperature work is the impossibility of obtaining an impermeable tube, and should oil vapour or fumes pass into the interior it would seriously vitiate the results.

Use of a Radiation Pyrometer with a Source of Insufficient Size.—It is sometimes necessary to use a radiation pyrometer at such a distance from a small source that the aperture of the instrument is not completely filled.

Thus with the Féry pyrometer, the image of the source formed at the receiver may be smaller than the limiting diaphragm immediately before the couple. The most satisfactory method of using the radiation pyrometer under such conditions is to construct a new limiting diaphragm of the proper size and recalibrate the pyrometer, sighting upon a black body. Another method which may be employed with small sources is to compute the actual size of the image found at the receiver and correct the observed deflection, making use of the assumption that the galvanometer deflection is proportional to the area of the image as long as the image is smaller than the limiting diaphragm. Thus, if the area of the opening to the receiver of the Féry pyrometer were 1 mm., and the area of the image of the source formed by the gold mirror were 0·5 mm.^{2}, the correct temperature would be given by the value corresponding to a deflection twice that of the actually observed deflection. Errors due to aberrations of the gold mirror will affect the measurements to some extent.

By the formula $$\frac{O}{I} = \left(\frac{u}{f} - 1\right),$$

where O is the diameter of the source,
I is the diameter of the image,
f is the focal length of the concave mirror,
u is the distance from source to mirror.

As a rough check upon this method of using a Féry pyrometer Burgess and Foote made the following measurements :—The area of image required by the pyrometer was 1·77 mms. The source remained at approximately a constant temperature 1,260° C., and its size was altered by means of a water-cooled diaphragm.

Area of Image.	Observed E.M.F.	Area of Receiver / Area of Image	Observed E.M.F. / Ratio of Areas	Temperature Computed.
Mm.	Millivolts.			C.
0·302	1·04	5·86	6·09	1,290
0·695	2·33	2·55	5·94	1,280
0·807	2·78	2·19	6·09	1,290
1·564	4·32	1·13	4·88	1,200
1·77	5·64	1·00	5·64	1,260
				Mean 1,265

The above-computed temperatures have a wide range, but without doubt, if especial care were taken, the accuracy could be increased, possibly to $\pm$ 20° C. This method will not give as satisfactory results as may be obtained by replacing the limiting diaphragm with one of smaller opening and then recalibrating the instrument by sighting upon a black body.

Sources of Error in Practical Forms of Radiation Pyrometers.—Since the ideal radiation pyrometer would give galvanometer deflections proportional to the intensity of the radiation emitted by the hot object, and hence to the difference in the fourth powers of the absolute temperatures, a calibration at one temperature would be sufficient to supply all the data necessary for the computation of the temperature scale. When T is large compared with T_0, the deflections should be proportional to T^4 (T_0^4 being negligible in comparison with T^4).

It is generally found, however, that the index is not 4, but varies between the limits 3·8 to 4·2 for various instruments.

In any particular case the value of the index may be obtained by plotting the logarithms of the deflections and temperatures. The experimental points will in general be found to lie on a straight line.

Many factors contribute to produce variations in the value of the index from 4.

1. The electromotive force generated by the thermocouple is not strictly proportional to the temperature difference between the hot and cold junctions. When the rise in temperature of the receiving disc above the surroundings is of the order of 80° this factor has an appreciable influence.

2. The thermocouple and inclined mirrors are enclosed in a small cell. Stray reflections from the walls falling on the receiving disc produce disturbances.

3. The rate of heat loss from the junction is not strictly proportional to its temperature excess.

4. Conduction of heat along the couple wires produces a slight temperature rise in the cold junction.

5. In addition there are the various errors to which the millivoltmeter readings are liable.

Occasionally one finds that an instrument will follow the fourth-power law with considerable exactitude. This is to be ascribed to the fact that the small residual effects accidentally neutralise each other's influence, rather than to theoretical perfection of design.

The other characteristics of practical types of radiation pyrometers which require study in the case of each individual instrument are—

1. That its indications are independent of the distance from source to pyrometer and independent of the size of the source when this is above the minimum size required by the geometry of the instrument.

2. That the final reading is quickly attained. While theoretically an infinite time is required to reach the equilibrium state (*i.e.*, when the receiving disc emits as much heat as it receives), most practical types reach the steady state in a minute or so. The time interval required depends, of course, on the individual pyrometer.

Occasionally a maximum reading will be quickly reached and then it begins to decrease, the final value only being reached after 15 to 20 minutes. This anomalous behaviour is generally due to conduction along the wires of the couple and to secondary radiation from the sides of the cell and the diaphragms.

Such an instrument must be calibrated under the same conditions as those under which it will be used in practice.

CALIBRATION OF RADIATION PYROMETERS.

Instruments are generally calibrated by comparison with a standard instrument over the range 500° to 1,400° C. A uniformly heated muffle forms a convenient source of radiation closely approximating to a "black body" radiator.

The standard instrument requires more elaborate study. For this purpose a large platinum foil wound electric furnace is convenient; this should be provided with suitably disposed diaphragms, and the pyrometer focussed on a plug of refractory material fixed in the centre of the furnace. Across the face of this plug one or more platinum-platinum-rhodium couples should be stretched, so that the mean temperature of the surface is obtained with accuracy.

To obtain a cone of radiation of sufficient size to fill the field of the pyrometer it is necessary to employ a furnace with an aperture of two or three inches in diameter.

At high temperatures a considerable amount of cooling takes place by convection from the open mouth of a horizontal furnace.

Some improvement is effected by inclining the mouth downwards at

an angle of 20° to 30°. With the furnace maintained at a steady temperature a series of points on the calibration curves of the pyrometers may be obtained by employing rotating sectors to cut down the radiation.

It must be remembered that the use of sectors for cutting down the radiation to give lower "apparent" temperatures is only legitimate if the receiving disc of the pyrometer has a constant coefficient of absorption for all wave lengths, since the form of the spectral energy distribution curve varies with the temperature.

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CHAPTER VI.

TOTAL RADIATION FROM OXIDE AND METALLIC SURFACES.

Total Radiation from Metallic Surfaces.—While muffles, furnaces, and heating chambers generally employed in the industries closely approximate to " full radiators," the surfaces of metallic objects depart considerably from the ideal contemplated by the Stefan-Boltzmann law. Consequently, a radiation pyrometer calibrated on a " full radiator," if employed to take the temperatures of such surfaces, will give readings which are too low.

When the surface is oxidised, the difference between the apparent and real temperature will be a function of the condition of the surface, and it is difficult to apply a correction with any degree of certainty.

The radiation from some of the commoner metals has been investigated with the conclusions summarised below.

Definition of the Emissivity of a Surface.—At the present time the term " emissivity " is used to denote the ratio of the heat emitted by unit area of the surface to that emitted by an equal area of a " full radiator " at the same temperature, and not in the older sense of the term, when it denotes the heat emitted divided by the temperature excess of the surface above the surroundings.

Hence, if W is the total radiation emitted by unit area of the surface at absolute temperature T to surroundings at temperature T_1, and σ is the " black body " constant, then

$$W = E\sigma (T^4 - T_1^4)$$

where E is defined as the emissivity constant for the surface at T.

The Emissivity of Oxidised Metallic Surfaces.—I. Nickel Oxide, NiO.—When nickel is heated to a high temperature in air, there is formed on its surface a tough, smooth layer of NiO.

The emissivity of this oxide surface has been studied over an extended temperature range.

(*a*) Randolph and Overholser investigated the subject up to a temperature of about 500° C. The work of these observers was primarily directed towards the determination of the heat loss from surfaces, and to separate the effects of convection and radiation, the total loss and the radiation loss were independently determined, so that the convection loss could be obtained by difference.

The radiation was measured by a robust absorption pyrometer. The comparison black body was a cast-iron pipe, closed at one end and heated by three independent resistance coils. A number of thermoelements were

distributed to obtain the average temperature, and at 500° C. the variations were of the order of 3° C.

The nickel disc was 19·3 cms. in diameter; it was electrically heated, the temperature being obtained by a thermocouple soldered to the back, allowance being made for the gradient through the disc.

As might be anticipated, the emissivity was dependent on the state of oxidation of the surface, and this again on the time during which it had been maintained at a given temperature. For example, starting with a polished disc maintained steady at 500° C. the emissivity increased rapidly at first, and did not attain a steady stage until about 90 hours had elapsed.

If observations were made at a lower temperature, after the surface had been maintained at a higher temperature for some time, the emissivity constant would depend on the maximum temperature only.

The results obtained for a surface previously heated to a temperature exceeding 600° C. are shown graphically in Fig. 63, in conjunction with those obtained at higher temperatures by Burgess and Foote.

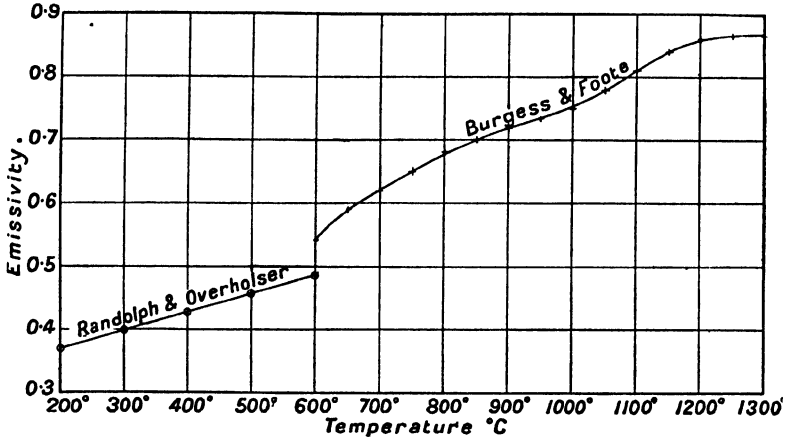


FIG. 63.—Variation with temperature of the emissivity of nickel oxide.

(*b*) Burgess and Foote employed an ordinary Féry radiation pyrometer for the measurement of the radiation, calibrated to give true temperatures under black body conditions.

Observations were made of the apparent temperatures, the corresponding true temperatures being obtained by methods described below.

Theory of the Method.—If E denotes the total emissivity of an approximately non-selective, radiating surface at absolute temperature T_1 and S the apparent temperature observed with the radiation pyrometer, then

$$Q = \sigma (S^4 - T_0^4)$$

$$Q = E \sigma (T_1^4 - T_0^4)$$

Hence $$\sigma (S^4 - T_0^4) = E \sigma (T_1 - T_0^4)$$

so that $$E = \frac{S^4 - T_0^4}{T_1^4 - T_0^4}.$$

Above 600° C. the term T_0^4 may be neglected, as a simple calculation will show :—

If, for example, E is about 0·5, the error in its value by neglecting T_0 would be only 0·007 at 600° C. and 0·0002 at 1,300° C.

Hence the emissivity may be calculated by the simple expression

$$E = \left(\frac{S}{T}\right)^4$$

Since in practical types of radiation pyrometers the index is rarely exactly 4, the above expression requires slight modification in such cases.

Taking the characteristic exponent of the empirical relationship between E.M.F. and temperature as b, so that

$$e = a\,T^b$$

then, if e' is the E.M.F. generated when sighted on a radiating surface of apparent temperature S (absolute) and true temperature T,

$$E = \left(\frac{e'}{e}\right)^{\frac{4}{b}}$$

To obtain the true temperatures corresponding to the apparent temperatures two methods were available which gave results in close accord.

(1) The application of the idea embodied in the Joly meldometer, in which the melting-points of microscopic specimens of various substances were observed, such as NaCl (800° C.) ; Na_2SO_4 (884° C.) ; Au (1,063° C.).

Experiments were made to ascertain that the temperature of the strip did not differ appreciably from that of the specimens.

(2) By the use of an optical pyrometer calibrated to read true temperatures when sighted on such a surface. This pyrometer is based on the principle of matching the intensity of the light from an electric lamp filament with the light from the hot object (see p. 127).

The pyrometer was calibrated initially for a " full radiator " conditions, and then the departure of the nickel oxide surface was obtained by sighting on the surface of a nickel tube, electrically heated, and into a small diaphragmed enclosure in the centre of the tube. By properly locating the diaphragms in the interior of the tube " black body " conditions could be realised quite satisfactorily.

Theoretically the experiments might be simplified by using the total radiation pyrometer directly to sight on the outside of the oxidised tube and on the interior : the first observation giving the apparent temperature while the second would give the true temperature. But, owing to the large aperture that would be necessary in comparison with that required for an optical pyrometer, this method of obtaining the true temperature would present practical difficulties.

It should be remarked, however, that the principle employed (of measuring the radiation by concentrating it on the thermocouple by means of a metallic

mirror) is only valid so long as the coefficient of reflection of the surface does not vary with the wave-length.

This appears to be the case for gold over the spectrum range from 1 to 14 μ.

The variation of emissivity with temperature of NiO is shown graphically in Fig. 63, while the data are given in Table XVIII.

TABLE XVIII.

Temp. ° C., . .	600	650	700	750	800	850	900	950	1,000
Emissivity, . .	0·54	0·59	0·62	0·65	0·68	0·70	0·72	0·73	0·75
Temp. ° C., . .	1,050	1,100	1,150	1,200	1,250	1,300			
Emissivity, . .	0·78	0·81	0·84	0·86	$0{\cdot}86_5$	$0{\cdot}86_7$			

The data for lower temperatures obtained by Randolph and Overholser were—

Temperature, ...	200° C.	400° C.	600° C.
Emissivity, ...	0·37	$0{\cdot}42_5$	$0{\cdot}47_5$

TABLE XIX.—Corrections which must be added to the Apparent Readings of Radiation Pyrometers to give True Temperatures when sighted on an Oxidised Nickel Surface.

Apparent temp. ° C., .	500	600	700	800	900
Correction, . . .	120°	110°	100°	95°	85°
Apparent temp. ° C., .	1,000	1,100	1,200		1,250
Correction, . . .	75°	65°	55°		50°

II. Iron Oxide.—A knowledge of the emissivity of iron oxide is of considerable importance technically, since it enables corrections to be made in the readings of radiation pyrometers when taking the temperatures of billets, rails, etc.

Burgess and Foote made observations on the same lines as those described above in the case of nickel; in this case, however, electrically heated iron tubes of various sizes were employed as radiators.

The results are given in Table XX.

TABLE XX.

True temp. ° C.,	500	600	700	800	900$_1$	1,000$_1$	1,100$_1$	1,200
Emissivity, .	0·85	0·85	0·86	0·87	0·87	0·88	0·88	0·89
Correction to apparent temp.,	30°	30°	35°	35°	40°	40°	45°	

It is possible to calibrate a total radiation pyrometer to give approximately true temperatures when sighted on an oxide surface by inserting a resistance coil in series with the indicator when standardising on the customary "black body" furnace. The value of the resistance can be calculated from the constants of the instrument.

Temperature Gradient through the Oxide Layer.—Iron oxide is a comparatively poor heat conductor, consequently it might be expected that the true surface temperature would be appreciably below that of the body of the metal.

Experiments with a thermocouple inside the tube to give the true temperature showed that the gradient through the oxide was considerable and apparently independent of the size of the tube. It would appear that the thickness of the oxide layer is automatically rendered of the same order of magnitude for different times of heating by the flaking off which occurs.

Data obtained by Burgess and Foote concerning this gradient are in good agreement with those obtained by Burgess, Crowe, Rawdon, and Waltenberg on rail sections, the couple being inserted in a small hole drilled parallel to the length of the rail and as near the oxide as possible.

Temp. inside layer, .	610° C.	715° C.	820° C.	930° C.	1,080° C.
,, outside layer, .	600° C.	700° C.	800° C.	900° C.	1,000° C.

These results show that any method of obtaining the temperature of rails, ingots, etc., by observations of the surface temperature, is liable to serious error unless account is taken of the gradient through the oxide film.

Emissivity of Molten Metals.—The total radiation pyrometer is of very limited use with molten metal surfaces. Such surfaces can never be freed from haze or fog, and the radiation from the walls of the furnace or crucible reflected at the molten surface is apt to produce serious errors.

Burgess has made some observations on the difference between the apparent and real temperatures in the case of metallic copper and cuprous oxide surfaces, using a Féry pyrometer.

The following relationships were found to be approximately true. In these equations t is the true temperature and F the apparent.

Molten copper, clear surface—

$$t = 3{\cdot}55\ F - 1{,}018$$

Surface covered by cuprous oxide—

$$t = 1{\cdot}41\ F - 169$$

The difference between the apparent temperatures—when the pyrometer was first sighted on the clear copper surface and then on the oxide surface, both being at the same temperature—amounted to as much as 300° C.

The apparent freezing-point of copper (clear surface) was found to be 600° C. compared with the true value of 1,083° C.

The emissivities of the two surfaces at various temperatures are given in Table XXI.

TABLE XXI.

Temperature °C.	Emissivity (molten copper).	Temperature °C.	Emissivity (cuprous oxide)
1,075	0·16	800	0·66
1,125	0·15	900	0·60
1,175	0·15	1,000	0·56
1,225	0·14	1,100	0·54
1,275	0·13		

Thwing has made some observations on the emissivities of both molten iron and molten copper relative to that of iron in the solid state (presumably oxidised). No details are given concerning the experiments. He states that molten cast iron at 1,300° C. to 1,400° C. has an emissivity of 0·29 that of the solid metal. Mild steel (molten) at 1,600° C. has a relative coefficient of 0·28, which coefficient appears to hold up to 1,800° C. Molten copper has an emissivity of 0·14 that of solid iron.

Some of the experiments appear to have been made on the streams of molten metals issuing from the furnaces.

Absorption in the Medium through which the Radiation passes.—The radiation has generally to pass through a gaseous medium before reaching the pyrometer. At present the information available concerning the effect of any absorption by the medium on pyrometric observations is very scanty.

The subject is complicated by the fact that most gases and vapours have fairly sharply defined absorption bands, and that the distribution of energy among the wave-lengths of the continuous spectrum emitted by a " black body " varies with the temperature. Should one of the absorption bands coincide with the maximum energy wave-length of the spectrum its influence would be very marked, whereas at another temperature that

particular wave-length might contain but a very small fraction of the total energy in the spectrum, consequently the loss by absorption would be insignificant.

Tyndall, about 1859, made a pioneer investigation of the diathermancy of gases and vapours. The apparatus employed consisted of a brass tube closed at the ends by plates of rock salt. Facing one end of the tube was a source of radiation, such as a cube containing boiling water or a glowing spiral of platinum. At the other end was placed a thermopile. When the interior of the tube was exhausted the deflection of the galvanometer connected with the thermopile was reduced to zero by bringing up a compensating cube to the other face of the thermopile. The gas under test was then introduced into the tube; if it exerted any absorption effect the galvanometer needle would be deflected. The fraction of radiation absorbed could be obtained by observing the full deflection produced when

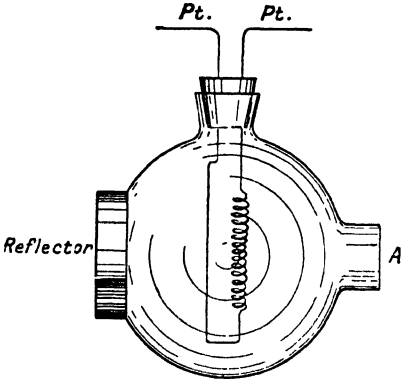


FIG. 64.—Mounting of platinum spiral.

a screen was interposed between the thermopile and the tube. The compensating cube then produced the same effect as the radiation which previously traversed the exhausted tube.

Tyndall found that air, oxygen, hydrogen, and nitrogen, if carefully purified, exerted no sensible absorption, while water vapour and carbon dioxide had a marked absorption. Vapours of organic compounds also had a considerable absorbing effect.

Table XXII. summarises the results obtained for a few of the substances investigated by him. The source of radiation was a platinum spiral enclosed in a glass globe 3 inches in diameter with an opening at A: shown in Fig. 64. The metallic reflector was used to augment the flux of radiation without sensibly altering its quality.

In some lamps the spiral was *in vacuo*, a plate of rock salt being employed for the window.

TABLE XXII.—Percentage Absorption of Various Gases.

Source of radiation : a platinum spiral at various temperatures.

Gas.	Appearance of spiral.			
	Barely visible.	Bright red.	White hot.	Near fusion.
Carbon disulphide,	6·5	4·7	2·9	2·5
Chloroform, . .	9·1	6·3	5·6	3·9
Sulphuric ether, .	43·4	31·4	25·9	23·7
Formic ether, .	45·2	31·9	25·1	21·3

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CHAPTER VII.

THE DISTRIBUTION OF ENERGY IN THE SPECTRUM OF A "FULL RADIATOR" AND THE PRINCIPLES OF OPTICAL PYROMETRY.

The Distribution of Energy in the Spectrum of a "Full Radiator."—The theoretical work of Boltzmann established the fourth-power law of radiation, which received ample experimental verification by Lummer and Pringsheim.

The next advance in the development of the theory was made by Wien in 1896, who deduced a number of relationships between the radiation in the spectrum of a "full radiator" and the temperature.

The first deduction is known as Wien's displacement law :—

$$\lambda_m = b\,T^{-1} \text{ or } E_m = k\,T^5$$

where λ_m is the wave-length of maximum energy and E_m is the maximum energy ordinate.

For the distribution of the energy among the various wave-lengths in the spectrum Wien deduced the expression

$$E_\lambda = c\,\lambda^{-5} f(\lambda\,T)$$

in which $f(\lambda\,T)$ could not be determined by purely thermodynamical reasoning.

By making certain arbitrary assumptions concerning the radiation emitted by vibrating gaseous molecules, he succeeded in resolving the function of $\lambda\,T$, and obtained the relationship

$$E_\lambda = c_1 \lambda^{-5} e^{-\frac{c_2}{\lambda T}}$$

for the distribution of energy among the various wave-lengths in the spectrum.

Experimental work, which will be referred to later, showed that the above expression only represented the facts for a limited range of λ and T. Since that time various attempts, based on plausible assumptions, have been made to discover the correct expression, but without success.

The one formula which does represent the experimental data closely under all conditions is Planck's—

$$E_\lambda = c_1 \lambda^{-5} \frac{1}{e^{\frac{c_2}{\lambda T}} - 1}$$

This expression, however, is based on assumptions which are inconsistent with the fundamental laws of electrodynamics.

The subject has aroused considerable interest during recent years, and reference must be made to the literature of the subject for fuller information.*

It will be observed that for small values of λ and T Planck's equation approximates to that of Wien, and the concordance is sufficiently close for wave-lengths in the visible spectrum to permit of the use of the simple form of Wien's for the range of temperature covered in practical optical pyrometry.

Experimental Study of the Distribution of Energy in the Spectrum of a "Full Radiator" at Various Temperatures.—In 1899 Lummer and Pringsheim published a further contribution to the subject. Their experiments on this occasion were directed to the determination of the distribution of energy in the spectrum of a "full radiator." At first they employed the various types of uniformly heated enclosures which they had constructed for their

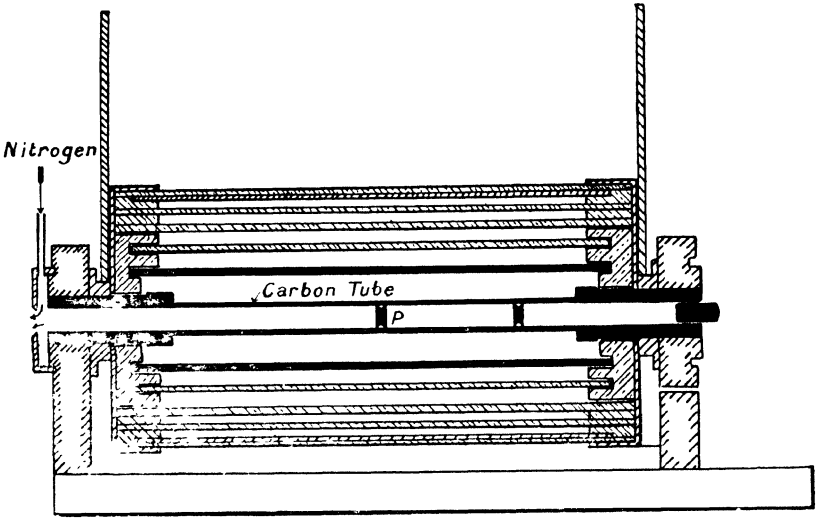


FIG. 65.—Diagram illustrating the construction of the carbon tube furnace.

experiments to test the Stefan-Boltzmann law. Later they introduced many practical improvements in the apparatus, and, by basing their method of measuring temperature on the fourth-power law, they were able to continue their experiments to very high temperatures. This procedure also led to a great simplification in the form of their "full radiator," which could then be reduced to an electrically heated carbon tube.

Description of the Experimental Arrangements.—The carbon tube furnace construction is shown in Fig. 65.

The tube was of uniform wall thickness (1·2 millimetres), 34 cms. long, and 1 cm. internal diameter. The ends were inserted into heavy carbon blocks, copper-plated and fixed into metallic clamps.

* See list at end of chapter.

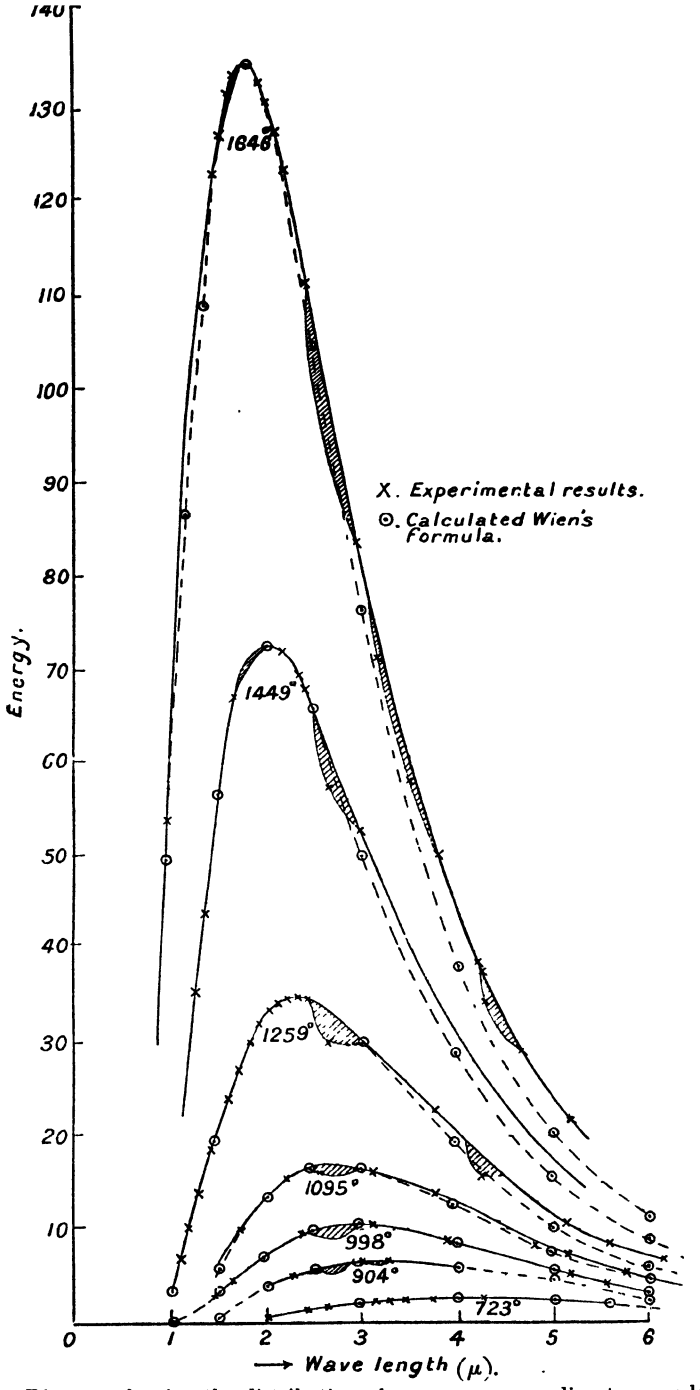


FIG. 66.—Diagram showing the distribution of energy corresponding to wave-length.

A stream of nitrogen was passed into the cap at the mouth of the furnace to diminish oxidation.

The plug P (in the centre of the tube) and the left half of the furnace was equivalent to a " black body " in respect of radiation.

The spectrum was produced by a fluorspar prism, and corrections applied to convert the prismatic to normal energy curves by means of the known dispersion curve of fluorspar.

The distribution of energy was measured by means of a linear bolometer, which was enclosed in an air-tight case to diminish the absorption effects of carbon dioxide and water vapour.

The bolometer consisted of a single strip of platinum foil 0·6 mm. wide.

The distribution of energy corresponding to wave-length is shown graphically in Fig. 66.

The shaded areas on the curves represent the absorption effects of the intervening medium.*

From these curves the value of λ_m and the energy corresponding to E_m could be directly obtained.

The experimental results were in agreement with the two laws—

$$\lambda_m T = \text{constant} = A, \text{ say}$$
$$E_m T^{-5} = \quad " \quad = B$$

The distribution formula—

$$E_\lambda = c_1 \lambda^{-5} e^{-\frac{c_2}{\lambda T}}$$

was found to be only approximately true, as shown graphically by the dotted lines. Table XXIII. summarises the numerical data.

TABLE XXIII.

Temp. abs. °C	λ_m.	E_m.	A From $\lambda_m T = A$.	B From $E_m T^{-5} = B$.	$T = \sqrt[5]{\frac{E_m}{B_{mean}}}$ °C	Diff. $T_{obs.} - T_{calc.}$
621·2	4·53	2·026	2,814	$2{,}190 \times 10^{-7}$	621·3	+0·1
723	4·08	4·28	2,950	2,166	721·5	−1·5
908·5	3·28	13·66	2,980	2,208	910·1	+1·6
998·5	2·96	21·50	2,956	2,166	996·5	−2·0
1,094·5	2·71	34·0	2,966	2,164	1,092·3	−2·2
1,259·0	2·35	68·8	2,959	2,176	1,257·5	−1·5
1,460·4	2·04	145·0	2,979	2,184	1,460·0	−0·4
1,646	1·78	270·6	2,928	2,246	1,653·5	+7·5
		Mean	2,940	$2{,}188 \times 10^{-7}$		

The above data refer to the early series, in which the temperatures

* Water vapour, carbon dioxide, and ozone have absorption bands in the infra-red.

were obtained by means of a thermocouple. Since the couple had been calibrated to 1,000° C. only, temperatures above this point are dependent on extrapolation of the thermoelectric scale. The variations in the values of A are within the limits of error possible in the determination of λ_m, and it will be observed that the values of B depend on the 5th power of the temperature.

The departure from Wien's law is systematic; this can be seen by comparing the various values of the constants c_1 and c_2, corresponding to increasing wave-lengths :—

λ	1·21μ	1·96μ	2·20μ	3·63μ	4·56μ
$c_1 \times 10^{-11}$	1,067	1,219	1,449	1,771	2,261
c_2 (Micron-degrees)	13,510	13,810	14,240	14,800	16,510

In the series at higher temperatures with the carbon tube furnace, it was possible to measure the energy of still greater wave-lengths, and the results show that Wien's law is not applicable to values of λT exceeding 3,000. The departure from the formula is shown by the following values of λ and c_2 :—

λ	8·3μ	12·3μ	17·9μ
c_2	18,500	24,800	31,700

Planck's Formula.—Planck's formula reduces to that of Wien's for small values of λT, consequently experimental proof of the validity of Wien's law is equally applicable to Planck's formula.

It now remains to consider the evidence for Planck's formula when λT is so large that Wien's law is not capable of representing the results.

Rubens and Kurlbaum studied the radiation of wave-length 51·2μ in the " black body " spectrum of a radiator at various temperatures.

This particular wave-length was chosen for practical reasons. If radiation of all wave-lengths is successively reflected from rock-salt surfaces, that corresponding to the wave-length 51·2μ alone receives metallic reflection ; the rest is either absorbed or refracted.

Advantage was taken of this property to isolate monochromatic radiation of long wave-length from the continuous " black body " spectrum.

In Table XXIV. the experimental results are compared with those obtained by calculation from the various formulæ.

It will be observed that Planck's formula represents the experimental results with a fair degree of accuracy, although subsequent investigations have shown that the divergences are greater than the possible error of experiment.

TABLE XXIV.

$\lambda = 51{\cdot}2\mu$.

Temp. abs. °C.	E_λ (observed).	Calc. Wien's.	Calc. Rayleigh's.	Calc. Planck's.
0	—	−121·5	− 20	− 23·8
85	− 20·6*	−107·5	− 19	− 21·9
193	− 11·8	− 48·0	− 11·5	− 12·0
293	0	0	0	0
523	+ 31·0	+ 63·5	+ 28·5	+ 30·4
773	+ 64·5	+ 96	+ 62·5	+ 63·8
1,023	+ 98·1	+118	+ 97	+ 97·2
1,273	+132·0	+132	+132	+132
1,523	+164·5	+141	+167	+166
1,773	+196·8	+147·5	+202	+200
∞		+194	∞	∞

Experiments with the wave-lengths $\lambda = 24{\cdot}0\mu$ and $\lambda = 31{\cdot}6\mu$ were also in accord with Planck's formula.

Rayleigh's formula—

$$E = \frac{c_1}{\lambda^4} \frac{T}{e^{\frac{c_2}{\lambda T}}}$$

is based on plausible assumptions, consistent with the laws of electrodynamics, and fits the experimental results for large values of λT, failing for values of λT less than 3,000.

For large values of λT Planck's formula reduces to that of Rayleigh's.

Variation with Temperature of the "Total Brightness."—To verify the relatoniship

$$E_m = K T^5$$

Lummer and Pringsheim employed a Lummer-Brodhun spectro-photometer, and worked with different parts of the luminous spectrum from red to violet. Owing to the rapid increase in the intensity of the luminous radiation with temperature, it was necessary to employ a number of absorption plates; at the highest temperature the intensity was reduced to $\frac{1}{8000}$ part to bring it within measureable limits.

	°C.	°C.
Temp. by 4th-power law (various distances), . .	2,345	2,348
Temp. by $E_m = K T^5$, ...	2,325	2,327

* The negative values are due to the fact that, when the radiator was below room temperature (20° C.), it received more energy from the thermopile than it emitted.

They were able to obtain an accuracy of about $\pm$ 20° C. with the total radiation pyrometer, and the calculated temperatures were in agreement within these limits of accuracy.

The relationship $\lambda_m T$ = constant was also checked and the value 2,930 obtained for the constant of a "full radiator." When the radiation from polished platinum was studied the constant was found to be 2,620.* Hence it is possible to estimate roughly the temperature of any object whose radiation is intermediate in character between that from a perfectly black body and polished platinum by determining λ_m by means of a bolometer and a dispersion apparatus.

This has been done for a number of radiators by Lummer and Pringsheim. The maximum value of T is obtained from $\frac{2,930}{\lambda_m}$ and the minimum from $\frac{2,620}{\lambda_m}$.

TABLE XXV.

Hot Object.	λ_m	$T_{max.}$ °C.	$T_{min.}$ °C
Arc light, . . .	0·7μ	4,200 abs.	3,750 abs.
Nernst lamp, . .	1·2	2,450	2,200
Welsbach mantle, .	1·2	2,450	2,200
Incandescent lamp, .	1·4	2,100	1,875
Candle, . . .	1·5	1,960	1,750
Argand burner, . .	1·55	1,900	1,700

Comparison of Wien's Law and Stefan-Boltzmann's Law to 2,800° C.—The work of Lummer and Pringsheim and their contemporaries was carried out before the researches of Holborn and Valentiner, of Jacquerod and Perot, and of Day and Sosman, had established the high temperature scale in terms of the gas thermometer, consequently it is difficult to form any precise estimates of the limits of accuracy to which the radiation laws may be regarded as proven at high temperatures. Recently Mendenhall and Forsythe have made a comparison up to 2,800° C. between two pyrometers, one based on "fourth-power" law and the other on Wien's law. The pryometers were calibrated by observations of the melting-points of gold and palladium, the values for which, on the scale of the nitrogen gas thermometer, had been determined by Day and Sosman.

The Optical Pyrometer.—This was of the disappearing filament type described on p. 127. The principle of the instrument is that of a telescope. An image of the hot object is superposed on the filament of a small electric

* There is no theoretical basis for the application of the law to the radiation from platinum, and subsequent investigations have shown that $\lambda_m T$ is not a constant for polished metallic surfaces, but increases with temperature. The constant value obtained by Lummer and Pringsheim is due possibly to the small range of temperature employed, or to lack of polish on the radiating surface.

lamp. Matching is effected by making the apparent brightness of the image identical with that of the filament by varying the current through the latter.

Since Wien's law is applicable to monochromatic radiation and not the entire visible spectrum, it is necessary to isolate as narrow a spectral range as possible. Generally this is effected by the use of a piece of good red glass; in the present case, however, they employed a spectroscopic eyepiece. The latter has the theoretical advantage of giving a narrower band and consequently a nearer approach to the ideal conditions contemplated by Wien's law. The width of the band transmitted was determined and found to be 200 A.U. ($0{\cdot}02\mu$) with a centre at $\lambda = 0{\cdot}658\mu$.

The calibration of the instrument—*i.e.*, the relationship between intensity of radiation and the current necessary to match it—was effected by the use of a system of rotating discs of measured aperture.

This method of reducing the intensity has already been referred to in connection with total radiation pyrometers, and the same principle is involved here.

Taking the logarithmic form of Wien's law,

$$\log E_\lambda = K - \frac{c_2}{\lambda} \cdot \frac{1}{T}$$

If balance was obtained with clear aperture on a "black body" at temperature T_1, and an apparent temperature T_2 was obtained through a sector of transmission ratio K, then

$$\log \frac{1}{K} = \frac{c_2 \log e}{\lambda}\left(\frac{1}{T_1} - \frac{1}{T_2}\right)$$

so that, by a series of observations on a furnace maintained at a constant known temperature, it was possible, by employing a series of discs with various values of K, to calibrate the pyrometer over a range of temperature. The apertures of the discs were measured by means of a dividing engine. Two steady temperatures were used as checks on the calibration.

The minimum aperture employed was about "$\frac{1}{180}$." This proved difficult to make accurately, and on measurement was found to be 2° 1′ 50″ instead of 2°. This error, however, would only produce a divergence of 5° C. in the computed scale if the nominal value of 2° angle had been taken.

The apparatus employed in the intercomparison is shown in Fig. 57 and the results are summarised below :—

TABLE XXVI.

No. of comparisons.	Temp °C.	$T_{optical} - T_{total\ radiation}$.	Range of observations.
9	1,750	Less than $\pm 0{\cdot}5°$	2°
7	2,200	,, $+2°$	4
3	2,500	About $+2°$	4
4	2,800	,, $+4°$	7

The difference is systematic, but not greater than the possible error of experiment. By an alteration in the assumed value of either c_2 or λ the systematic difference could be eliminated. For example, if, instead of $0{\cdot}658\mu$, the value of $0{\cdot}657\mu$ is taken, the differences disappear.

The Total Radiation Pyrometer.—It will be observed from a study of Fig. 57, p. 99, that the "total radiation" pyrometer was enclosed in the evacuated chamber containing the furnace, while the optical pyrometer observations were taken through a glass window. A small correction * was necessary for the absorption of this window in the visible radiation.

OPTICAL PYROMETRY.

While theoretically the "total radiation" type of pyrometer has the advantage of being based on principles whose validity have received ample confirmation, the optical type of pyrometer possesses considerable practical advantages in so much that it does not demand an object of large dimensions to sight upon. Also the influence of imperfect "black body" conditions is not so serious as in the case of the total radiation types.

COMMERCIAL FORMS OF OPTICAL PYROMETERS.—The two common forms of optical pyrometers are the "disappearing filament" type and the "polarising" type.

A. **The Disappearing Filament Type.**—This type of pyrometer was introduced about twenty years ago by Morse in America, but the principle involved—the matching of the brightness of a lamp filament against that of the hot object—was in use as far back as 1888.

In its earliest form the Morse pyrometer consisted of a metal tube about 3 inches in diameter and 8 inches long, open at both ends, and provided on one side with a projection serving as a means for holding an incandescent lamp.

At the centre of the tube was mounted the lamp, which was connected in series with a battery, rheostat, and milliammeter.

The instrument is shown diagrammatically in Fig. 67.

In making a temperature measurement the operator holds the pyrometer in front of his eye and, looking through, observes the lamp filament superposed on the furnace or hot object as background. Owing to the different distances of lamp and furnace from the observer, it is necessary to vary the accommodation of the eye when looking at one object and then at the other.

By adjustment of the rheostat the current in the lamp is varied progressively until the lamp filament and furnace appear equally bright.

When the filament disappears against the furnace as background, the current through the filament is a measure of the temperature.

Holborn and Kurlbaum modified the instrument by adding an objective

* The method of obtaining this correction is described on p. 139.

and eyepiece (see Fig. 68). The objective projects an image of the furnace upon the plane of the lamp filament, and the fatigue of the eye due to constantly varying the accommodation is avoided.

Theoretically, the image of any source as observed through a particular

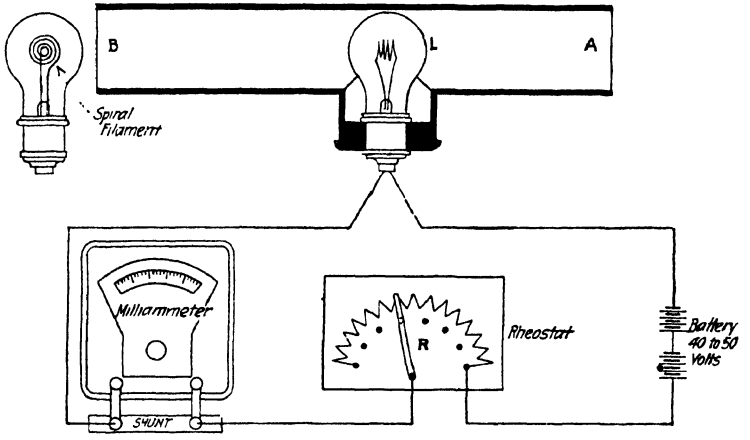


FIG. 67.—Arrangement of original form of Morse pyrometer.

telescope will not vary in brightness with a change in distance from the source (except, of course, differences due to air absorption, etc.), providing a certain solid angle is always filled with radiation from the source and this angle is of such size that the cone if rays entering the eye is constant. This

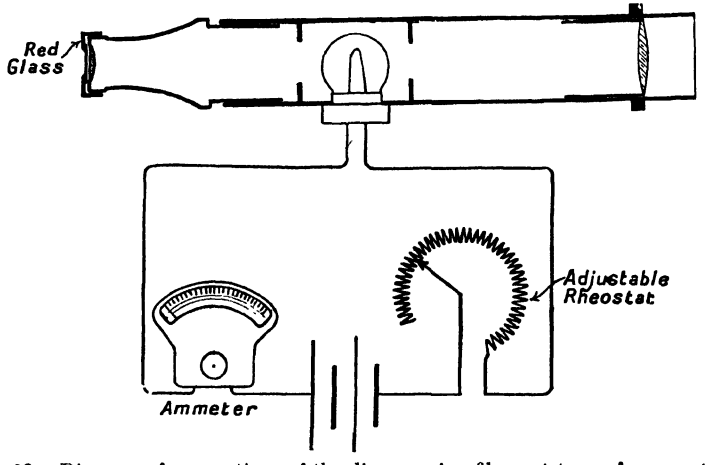


FIG. 68.—Diagram of connections of the disappearing filament type of pyrometer.

angle is generally determined by having the eyepiece at a fixed distance from the pyrometer lamp and having before the eyepiece a limiting diaphragm of such size that it is always filled with light from the objective lens. It is

also necessary to have a fixed diaphragm between the objective lens and the pyrometer lamp (see Fig. 69).

In all modern instruments of this type a red filter glass is fixed in the eyepiece.

This serves two purposes :—

(*a*) The matching of the intensities is facilitated, as practically monochromatic radiation is obtained, so there are no colour differences at high temperatures. This is of particular value in dealing with surfaces which do not radiate light of the same composition as that emitted by black body, since the intensity of radiation of any one colour from such surface increases progressively in a definite manner as the temperature rises.

(*b*) The scale of the instrument can be extrapolated in the basis of Wien's law, employing a rotating sector or absorption glass for cutting down the intensity of the source.

In recent years Forsythe and his collaborators at the Nela Research Laboratory have made a thorough study of this form of pyrometer, and shown how many of the errors in temperature measurements with the instrument may be avoided by attention to the details of this design.

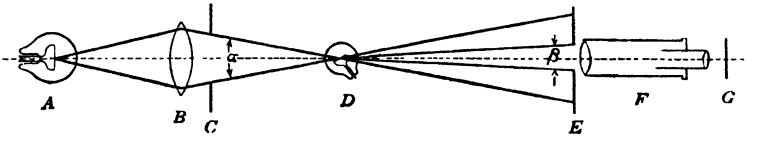


FIG. 69.—Arrangement of optical system of disappearing filament type pyrometer.

A, Lamp filament or hot object, the temperature of which is being determined.
B, Objective lens.
C, Entrance cone diaphragm.
D, Pyrometer filament.
E, Eyepiece diaphragm.
F, Eyepiece.
G, Monochromatic filter glass.

A laboratory form of disappearing filament instrument for precision work is shown in Fig. 70. The design of this instrument is due to Messrs. F. H. Schofield and Edgar A. Griffiths, and is based on the researches of Forsythe and his collaborators. Two lamps are fitted, and they can be readily interchanged so that a check is obtained on the permanency of the calibration. The rotating sector is arranged just in front of the lamps as the experiments of Mendenhall and Forsythe have proved that in this position the definition is practically independent of the position of the opening of the sector relative to the filament when crossing the field. The difficulty only occurs when taking the temperature of small objects such as incandescent lamp filaments.

The Polarising Type of Optical Pyrometer.—König in 1894 described a new type of spectrophotometer. In this instrument the two beams of light were resolved into two spectra and comparison effected between beams of identical colour throughout the spectrum. In 1901 Wanner applied the

essential principles of this instrument to the design of an optical pyrometer. In this case the radiation from the hot object is the one beam while the

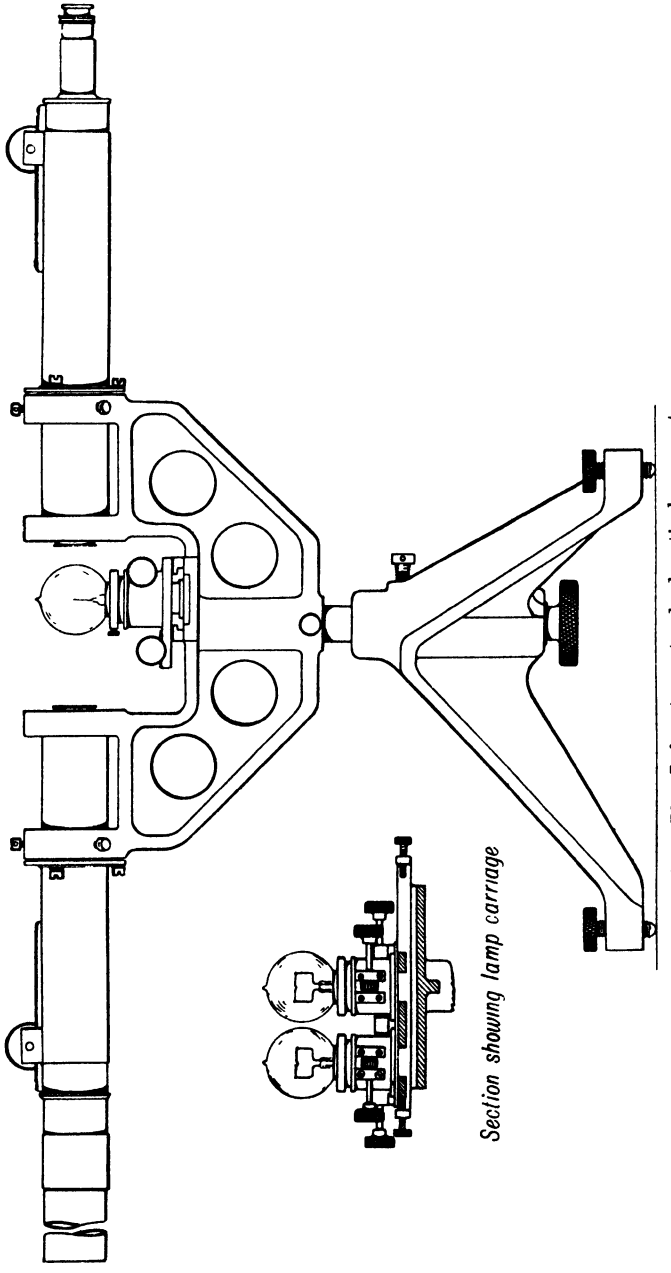


FIG. 70.—Laboratory standard optical pyrometer.
(The lamps are enclosed in a box (not shown) with holes in the line of sight.)

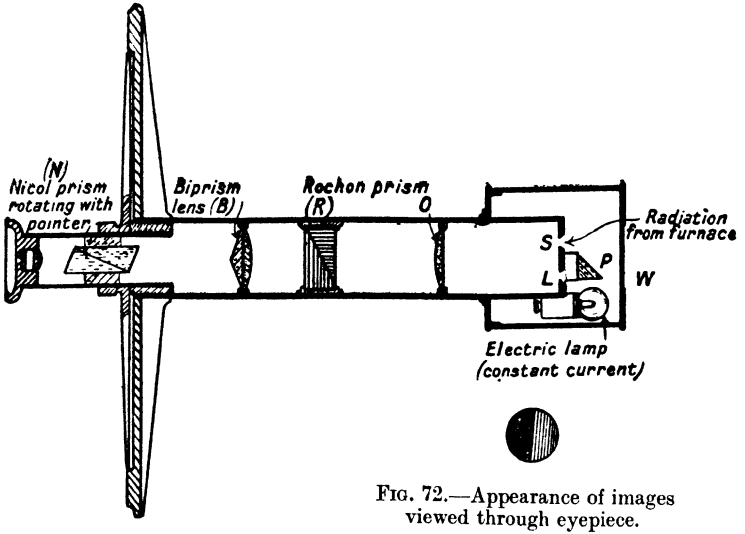


FIG. 71.—Diagram illustrating Wanner's modification of König's spectrophotometer.
S and L, small circular aperature; O, lens; R, Rochon prism; B, biprism lens; N, Nicol prism.

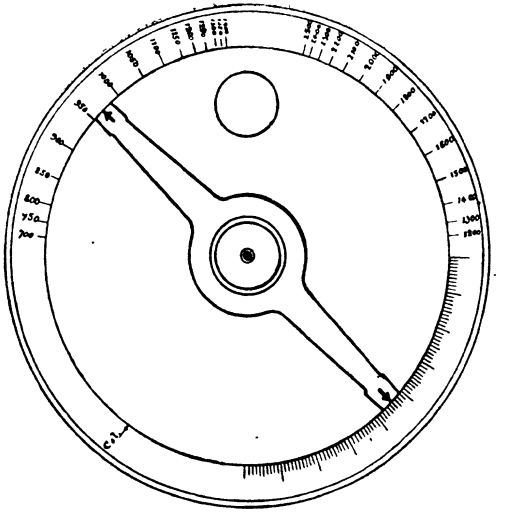


FIG. 72.—Appearance of images viewed through eyepiece.

light of constant intensity from an electric lamp supplies the comparison beam.*

The essential features of the instrument will be understood from Fig. 71.

The radiation from the hot object is received through the circular hole S, while the electric lamp illuminates the matt surface of the right-angled prism P, which in turn directs the light on to the circular hole L symmetrically disposed with S about the optical axis of the system.

The lens O renders the two beams parallel. R is a Rochon prism, which splits each beam up into components polarised at right angles.

The function of the biprism lens B is to produce deviation in the beams of such amount that an image from each of the two sources is brought into juxtaposition. On consideration it will be seen that the biprism splits each image up into two, thus bringing the total up to eight.

These images are semicircular patches uniformly illuminated. The two in juxtaposition are polarised at right angles (Fig. 72) and are viewed through the eyepiece, the other images being screened out.

The Nicol prism N can be rotated around the optical axis, its position being indicated by a pointer attached.

To understand the precise functions of the various optical parts it is advisable to consider the effect of each individually.

In Fig. 73 the contribution of each component is shown. The circular holes S and L are at the focus of O, so the images produced will be uniformly illuminated circular discs—*i.e.*, of the face of the lens—which the biprism splits up into semicircles.

The arrows indicate the plane of polarisation of the light.

A screen is arranged to cut off all the images except the two worked with.

To understand the function of the Nicol prism suppose for the moment that the two beams are of equal intensity, then, with the plane of polarisation of the Nicol prism making an angle of 45° with the direction of polarisation of either beam, a uniformly illuminated circle would be observed having a diametrical line across where the two fields come into contact.

Rotation of the Nicol prism in either direction will cut down the intensity of one of the beams and increase that of the other.

Hence, if the beams are initially of unequal intensity, matching of the intensities, as viewed through the eyepiece, is possible for a certain position of the prism between the extinction positions 0° and 90°.

Theory of the Polarising Type of Pyrometer.—It is proved in text-books of Light, that if I_1 and I_2 are the intensities of two plane polarised beams of radiation matching at angles φ_1 and φ_2, a beam of constant intensity,

* The current through the lamp is maintained at a predetermined value by means of a rheostat and ammeter. From time to time the intensity of the beam given by the electric lamp is matched against that from an amyl acetate lamp by adjustment of the current. This renders the scale of the pyrometer independent of the permanency of the electric lamp.

such as that from an electric lamp, when viewed through a Nicol prism, then :—

$$\frac{I_1}{I_2} = \frac{\tan^2 \varphi_1}{\tan^2 \varphi_2}$$

In optical pyrometry, by the insertion of a direct-vision prism or a piece of suitable red glass in the path of the two beams it is possible to work with narrow spectral bands and consequently apply Wien's law.

According to this law the intensity of light of wave-length λ emitted by a " full radiator " is given by the expression—

$$I = \frac{c_1}{\lambda_5} e^{-\frac{c_2}{\lambda T}}$$

Suppose I_1 is the intensity of wave-length λ at temperature T_1.

I_2 " " " " T_2.

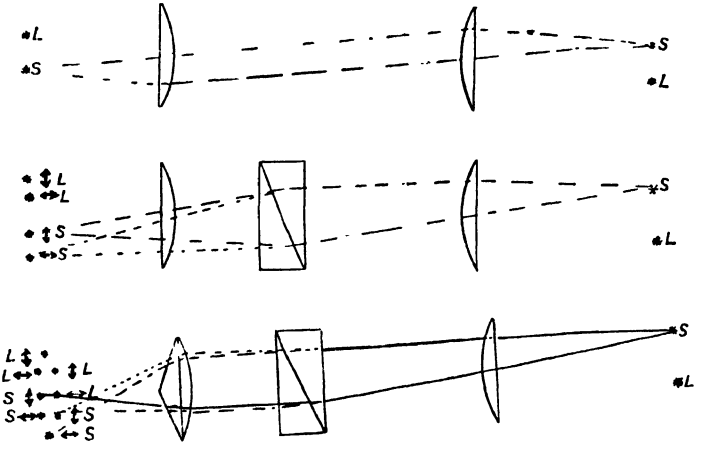


FIG. 73.—Diagram showing functions of various optical parts of the spectrophotometer. The arrows ⟷ and ↕ indicate plane of polarisation. Eight images are formed in all, of which six are stopped out.

By Wien's law

$$\frac{I_1}{I_2} = e^{\frac{c_2}{\lambda}\left(\frac{1}{T_2} - \frac{1}{T_1}\right)}$$

Hence

$$\frac{I_1}{I_2} = \frac{\tan^2 \varphi_1}{\tan^2 \varphi_2} = e^{\frac{c_2}{\lambda}\left(\frac{1}{T_2} - \frac{1}{T_1}\right)}$$

Taking logarithms to the base e,

$$2(\log \tan \varphi_1 - \log \tan \varphi_2) = \frac{c_2}{\lambda}\left(\frac{1}{T_2} - \frac{1}{T_1}\right)$$

so that the relation between φ and T is of the form

$$\log \tan \varphi = a + \frac{b}{T}.$$

Hence, if a series of values of φ and T are obtained, when (log tan φ) is plotted against $\frac{1}{T}$, the points should fall on a straight line.

Theoretically, a single determination of the angle φ corresponding to a known temperature T, together with a knowledge of c_2 and λ should suffice to give a complete calibration of the instrument. In practice, however, it is very difficult to obtain perfection in the optical parts and freedom from strain in the lenses which affects the polarised beam. So it is generally advisable to calibrate the instrument against a "black body" over the entire range.

Experience with commercial forms of the pyrometer indicates that the divergence from the theoretical line is greatest near the extinction positions owing presumably to defects in the Nicol prisms and scattering of light.

Extension of the Scale above 1,400° C.—The range available with this type of pyrometer without an absorption device is from 700° to about 1,400° C. It is possible to go a little below 700° C., but the intensity of the light transmitted is so feeble as to preclude accurate observations below this point. The scale closes in rapidly as angle 90° is approached, consequently 1,400° C. is the general working limit for this range.

By employing absorption glasses of appropriate density it is customary to have a second scale from 900° to 2,000° C.; a third (two absorption glasses) from 1,200° to 2,500° C.; and a fourth (three glasses) from 1,400° to 4,000° C. The last mentioned covers the extreme temperature possible terrestrially—namely, that of the electric arc.

The intensity of the radiation emitted by a hot object increases very rapidly with the temperature; for example, the intensity of red light from a "full radiator" at the temperature of the melting-point of iridium (2,290° C.) is roughly 2,000 times greater than that at the temperature of the melting-point of gold (1,063° C.).

The range of temperature that can be measured in the ordinary way by the disappearing filament type of optical pyrometer without some device for cutting down the intensity of the radiation from the hot object is from 600° to 1,500° C. The comparison lamp cannot be run at much higher temperatures than 1,600° C. without rapid deterioration. The scale is extended by the use of absorption devices or rotating sectors. With the early form of disappearing filament pyrometer, the absorbing device generally used consisted of two black mirrors inclined at an angle of 45°. In this arrangement the beam of light from a hot object is reflected twice at an angle of 45 incidence, and thereby weakened to about $\frac{1}{200}$ of its original intensity.

To extend the scale of the pyrometer up to about 2,700° C., the usual practice at the present day is to insert a piece of neutral-tinted glass in the

path of the beam from the furnace or to employ rotating sectors of definite aperture.

A discussion of the methods of computing the transmission factor is given later.

Relative Merits of the Disappearing Filament and Polarising Types of Optical Pyrometers.—The filament type is essentially a telescope, and consequently it is easy to select out the object whose temperature is desired; the polarising type does not permit of a sharply defined image; in fact, the field should be a uniformly illuminated semicircular patch. A blurred image of the hot object is, however, distinguishable by moving the eye about a little. With the polarising type it is necessary, when taking the temperature of a metallic surface, to sight normally since the light given out at oblique incidence is largely polarised.

The polarising type has three noteworthy features:—

1. Extrapolation of the scale on the basis of Wien's or any other radiation law is readily effected, as the instrument is essentially a photometer.

2. The temperature scale is independent of the permanency of the electric lamp,* which is set from time to time against an amyl acetate lamp.

3. The scale closes in at high temperatures and is reasonably open over the middle portion (800° to 1,200° C.).

The "disappearing filament" type is nowadays employed in work of the highest precision, as its simplicity renders possible a high degree of accuracy in its mechanical construction.

CALIBRATION OF THE INSTRUMENT.—The calibration of optical pyrometers can be readily effected by reference to a standardised thermocouple in an electric furnace arranged to give approximately full radiation by a series of diaphragms suitably disposed.

Fig. 74 shows a furnace arranged for optical pyrometer calibration up to 1,370° C.

The pyrometer is sighted upon the central diaphragm, which has the junction of a thermojunction on its surface to give the temperature of the enclosure.

With the furnace illustrated in Fig. 76 the calibration can be carried to 1,550° C.

The calibration of the disappearing filament type cannot be carried beyond 1,550° C. without the use of an absorbing glass, since the permanency of the resistance of the filament is liable to be affected by running for long periods to the top temperatures.

For representing the relationship between the current and temperature in the case of the disappearing filament type of pyrometer a parabolic formula $i = a + b\,t + c\,t^2$ is applicable, whilst for the polarising type the appropriate formula is $\log \tan \varphi = a + \frac{b}{T}$.

* It may be remarked that a 1 per cent. variation in the current through the lamp produces a 9 per cent. variation in the light emitted, consequently the current requires accurate adjustment.

Standardisation by Observation of Transition Points.—It is possible to calibrate optical pyrometers by direct observations of freezing- or melting-points, without the use of a thermocouple as intermediary.

In the case of materials which require a reducing atmosphere and do not react at high temperatures with graphite, Kanolt employed the following method :—

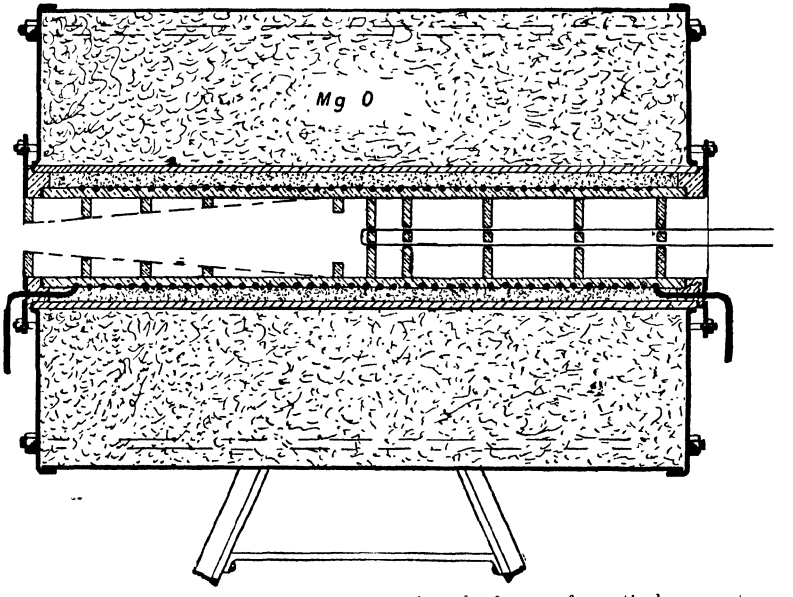


FIG. 74.—Diagram illustrating the construction of a furnace for optical pyrometer calibration.

The substance was contained in a graphite crucible with re-entrant tube carried from the lid, as shown in Fig. 75.

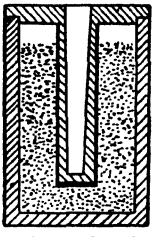


FIG. 75.—Graphite crucible with re-entrant tube supported from the lid.

The crucible was heated in a graphite spiral furnace and the pyrometer sighted on the bottom of the tube; this ensured that approximately black body conditions were obtained.

On plotting the heating or cooling curves a well-defined halt was observed at the transition point.

The following metals and salts were employed :—Antimony, 630° C.; copper-silver eutectic, 779° C.; silver, 962° C.; copper, 1,083° C.; diopside (melting), 1,391° C. Prolonged heating of diopside in contact with graphite had no apparent effect on the value obtained for the melting- point.

Attempts have been made by Hoffmann and Meissner to employ a similar method in the case of the palladium freezing-point.

A hard porcelain crucible and tube were used with an oxidising or neutral

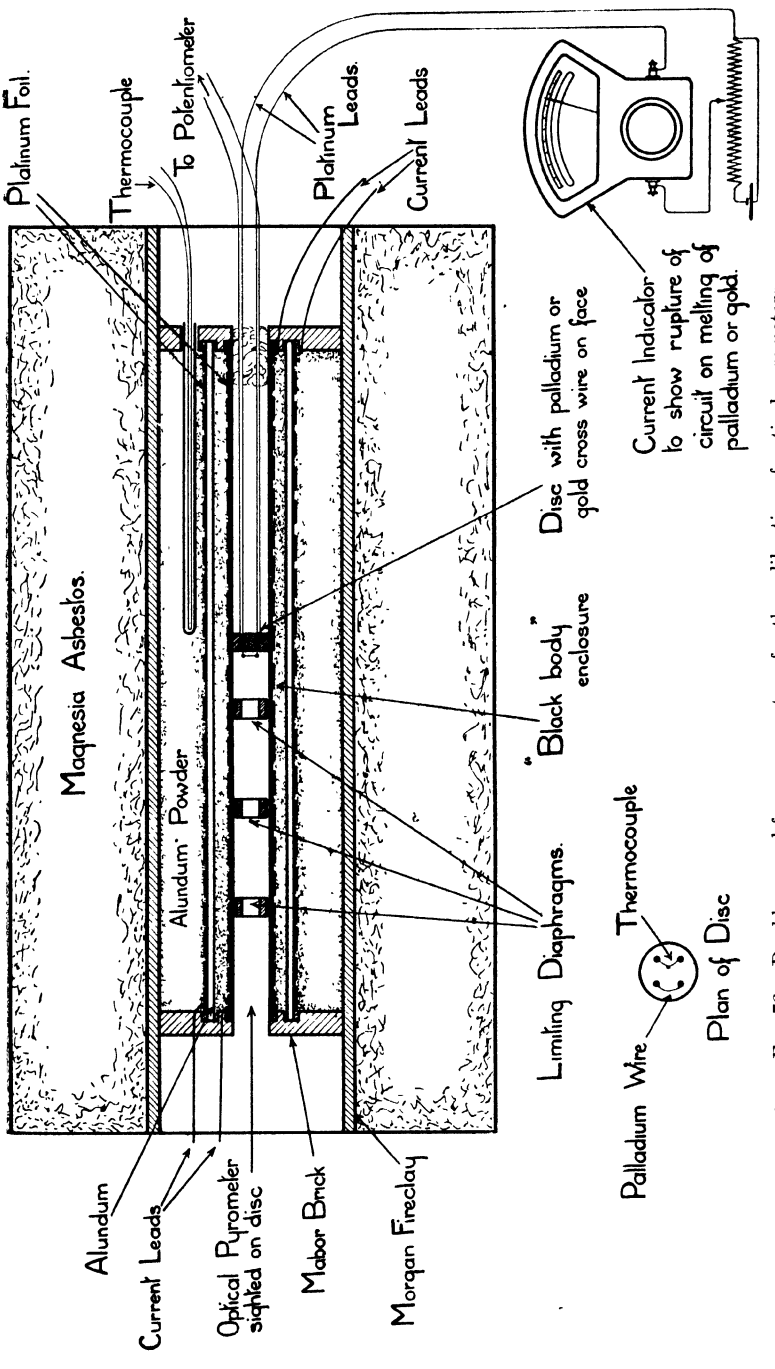


FIG. 76.—Double-wound furnace as set up for the calibration of optical pyrometers under "black body" conditions.

atmosphere around the metal. It was found that the molten palladium attacked the porcelain with the formation of a brownish substance.

An additional difficulty was the "spitting" of the fused metal, accompanied by considerable temperature fluctuations; this could not be prevented even by the passage of a stream of pure nitrogen into the metal.

For the direct calibration of a pyrometer in terms of the melting-point of palladium the simplest procedure is to make the palladium wire a part of a circuit and heat it up in a furnace under "black body" conditions.

A double wound furnace is necessary for this (see Fig. 76).

The two windings are arranged on the cascade principle: the outer

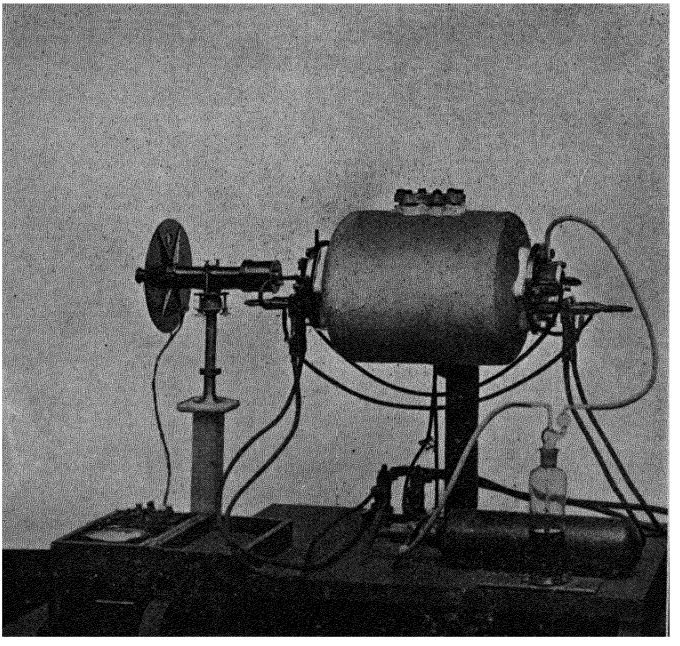


FIG. 77.—General view of Eden's carbon tube furnace for the comparison of optical pyrometers.

The pyrometer is sighted on a disc of carbon in the middle of the furnace.

coil brings the temperature of the furnace up to about 1,000° C., while the inner one raises the temperature of the centre up to 1,550° C.

The pyrometer is sighted on the fireclay disc, across the face of which is placed a thermocouple and a short length of palladium wire connected to platinum leads.*

* A second thermocouple may be used instead of the platinum leads with the palladium wire forming a bridge between the two arms. The two couples will heat up at the same rate until the melting-point is reached when the second will show a well defined halt.

The melting-point can be detected by the break of the circuit, and the temperature at this instant should be noted.

The melting-point of platinum can also be employed as a fixed point in the same way.

Calibration of Optical Pyrometers by Comparison with a Standard Instrument.—When an optical pyrometer has been standardised by reference to high temperature melting-points and its scale calculated, it is a simple matter to calibrate other instruments by comparison.

A carbon tube furnace suitable for temperatures up to about 2,500° C. is illustrated in Fig. 77, while Fig. 78 shows, on a large scale, the carbon tube complete with its water-cooled electrodes.

The body of the furnace is of cast aluminium with water-cooled covers.

The carbon tube is protected from oxidation by filling the shell with finely divided lamp-black.

The ends are closed by thin glass windows and a stream of nitrogen is passed through the tube to clear away any smoke produced.

A loosely fitting plug of carbon is fixed about midway in the tube, and the pyrometers sighted upon it in turn when the furnace is at a steady temperature.

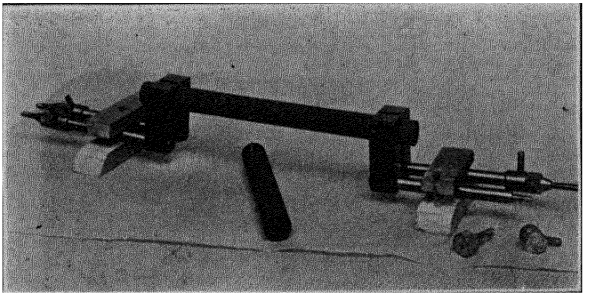


FIG. 78.—Carbon tube and water-cooled electrodes of furnace shown in Fig. 77. The leads carrying the current to the furnace are clamped to the brass tubes.

Alternating current of the order of 100 amps., from a low-tension transformer, is required to operate the furnace.

Extrapolation of the Scale of an Optical Pyrometer.—Over the range 700° to 1,500° C., through which it is possible to calibrate an optical pyrometer against a thermo-element under "black-body" conditions, it is immaterial what the wave-length transmitted by the filter glass may be. But when it becomes necessary to extend the scale to high temperatures, the use of a rotating sector or an absorption glass is necessary to cut down the intensity. The higher range is calculated on the basis of Wien's law, as follows :—

Calculation of the Constant of an Absorption Glass or Rotating Sector.—It is assumed that the absorption glass or sector cuts down the intensity of light in the radiation from the hot object in the ratio of S to 1. If T_1 is the observed temperature without absorption glass, and T_2 the apparent

temperature of the same object with absorption glass, then by Wien's law

$$E = c_1 \lambda^{-5} e^{-\frac{c_2}{\lambda T_2}}$$

$$S E = c_1 \lambda^{-5} e^{-\frac{c_2}{\lambda T_2}}$$

$$\log_e S = \frac{c_2}{\lambda}\left(\frac{1}{T_1} - \frac{1}{T_2}\right)$$

where c_2 is a numerical constant whose value is 14,350 micron degrees, and λ is the wave-length. So that T_1 can be calculated from the observed T_2 if S and λ are known from independent measurements.

If the red filter glass was strictly monochromatic, the wave-length transmitted, λ, would be a constant. Thus it would be the same for any energy distribution and temperature of source.

As it is impossible in practice to obtain absolutely monochromatic filter glass, the question arises which particular wave-length in the spectral band transmitted by the glass to be employed in the calculations?

In order to decide upon the appropriate wave-length it is necessary to consider the function of the filter glass.

Now the quantities actually compared in pyrometry are the integral luminosities as observed through the filter glass, so it is obvious that the wave-length to be employed in calculation (or the "effective" wave-length as it is termed) must be such that for any definite temperature interval the ratio of the radiation intensities for this wave-length according to Wien's law shall equal the ratio of the integral luminosities as observed through the glass.

Determination of the "Effective" Wave-Length for Various Temperature Ranges.—The following method for the determination of the "effective" wave-length for the interval between two definite temperatures of a full radiator has been described by Hyde, Cady, and Forsythe. Other methods, depending on a knowledge of the sensibility curve of the eye, have been described by the same authors, by Pirani, and by Foote, who gives a mathematical treatment of the question.

(1) *Direct Determination.*—The ratios of the intensities of emission for a number of wave-lengths are measured, and these ratios compared with the ratio of the integral luminosities of the radiation from the source, when observed through the red glass under test.

These measurements can be made in two ways:—

In one set of measurements the ratios of the intensities of radiation are measured with a spectrophotometer, and the ratio of the integral luminosities with a Lummer-Brodhun photometer having the red glass over the eyepiece. In the other set the ratio of the intensities are measured with a spectral photometer (Henning type), and the ratio of the integral luminosities with an optical pyrometer, either the disappearing "filament" or the polarising type, with the red glass over the eyepiece.

(2) *Indirect Determination.*—The results obtained by calculation from the

transmission curve of the red glass (from which the integral luminosities are calculated on the basis of Wien's law), and the sensibility curve for the eye are in close agreement with those obtained by direct experiment.

The procedure for obtaining the values of λ is laborious, and is resorted to only in the case of standard instruments for use at temperatures exceeding 1,500° C.

Foote adopts the indirect method, but develops the method of computation, so that the effective wave-length for a definite temperature is obtained.

His method of calculation is as follows :—

Let the transmission coefficient of the glass—*i.e.*, the ratio of energy transmitted to the incident energy—be denoted by k. Then $k = f(\lambda)$, where $f(\lambda)$ is an unknown function to be determined experimentally. And let the visibility curve for the average eye be presented by

$$V = F(\lambda).$$

It is not necessary to know the mathematical equations for these, as the graphic forms of the functions are quite convenient.

Now, according to Wien's law, the intensity at temperature T_1 is

$$E_{T_1} = c_1 \lambda^{-5} e^{-\frac{c_2}{\lambda T_1}}$$

and at T_2

$$E_{T_2} = c_1 \lambda^{-5} e^{-\frac{c_2}{\lambda T_2}}$$

so that

$$\frac{E_{T_1}}{E_T} = e^{\frac{c_2}{\lambda}\left(\frac{1}{T_2} - \frac{1}{T_1}\right)}$$

Since λ may have any arbitrary value, it can be chosen so as to give the ratio of E_{T_1} to E_{T_2} the same value as the ratio of the integral luminosities seen through the filter glass.

Let L_1 = luminosity at temperature T_1.

L_2 = luminosity at temperature T_2.

Then,

$$L_1 = \int_0^\infty E\, k\, V\, d\lambda = \int_0^\infty E(\lambda, T_1)\, k(\lambda)\, V(\lambda)\, d\lambda$$

$$L_2 = \int_0^\infty E(\lambda, T_2)\, k(\lambda)\, V(\lambda)\, d\lambda$$

$$\frac{L_2}{L_2} = \frac{\int_0^\infty E(\lambda, T_1)\, k\, V\, d\lambda}{\int_0^\infty E(\lambda, T_2)\, k\, V\, d\lambda}$$

L_1 and L_2 can be determined by graphical integration. Let the ratio be any definite number. If it is possible to choose λ in the relation $\frac{E_{T_1}}{E_{T_2}}$ that $\frac{E_{T_1}}{E_{T_2}} = \frac{L_1}{L_2}$. Call this value of λ, λ_m. By substituting in the above expressions we have

$$\text{Mean } \lambda_m = \frac{c_2\left(\frac{1}{T_2} - \frac{1}{T_1}\right)}{\log_e L_1 - \log_e L_2}$$

This is merely the mathematical form of the definition of effective wave-length proposed by Hyde, Cady, and Forsythe.

Instead, however, of referring to a given temperature interval T_1 to T_2, it may be referred to a definite temperature by letting the two temperatures approach one another.

Assuming T_1 and L_1 constant and dropping the suffixes, let T_2 and L_2 approach these values as their respective limits. Then

$$\lambda_m = \text{limit of } \frac{c_2\left(\frac{1}{T_2} - \frac{1}{T}\right)}{\log L - \log L_2}$$

becomes, when numerator and denominator have been separately differentiated with respect to T,

$$\lambda_m = \frac{-c_2\frac{1}{T^2}}{\frac{1}{L}\frac{dT}{dL}} = \frac{c_2 L}{T^2\frac{dL}{dT}}$$

but
$$L = \int_0^\infty E\,k\,V\,d\lambda$$

$$\frac{dL}{dT} = \frac{d}{dT}\int_0^\infty E\,k\,V\,d\lambda = \int_0^\infty k\,V\,d\lambda\frac{dE}{dT}$$

since only E is a function of T.

Again,
$$E = c_1\lambda^{-5}e^{-\frac{c_2}{\lambda T}}$$

$$\frac{dE}{dT} = c_1\lambda^{-5}e^{-\frac{c_2}{\lambda T}}\left[\frac{c_2}{\lambda}\frac{1}{T_2}\right]$$

$$\frac{dL}{dT} = \int_0^\infty k\,V\,d\lambda\,c_1\lambda^{-5}e^{-\frac{c_2}{\lambda T}}\left(\frac{c_2}{\lambda}\frac{1}{T_2}\right)$$

$$= \frac{c_2}{T^2}\int_0^\infty \frac{k\,V\,E\,d\lambda}{\lambda}, \text{ since } E = c_1\lambda^{-5}e^{-\frac{c_2}{\lambda T}}$$

$$\therefore\ \lambda_m = \frac{c_2 L}{T^2\frac{c_2}{T^2}\int_0^\infty \frac{k\,V\,E}{\lambda}d\lambda}\frac{L}{\int_0^\infty \frac{k\,V\,E}{\lambda}d\lambda}$$

$$\lambda_m = \frac{\int_0^\infty k\,V\,E\,d\lambda}{\int_0^\infty \frac{k\,V\,E}{\lambda}d\lambda}$$

This is the effective wave-length for a glass of transmission $k\,f(\lambda)$ for temperature T.

To find λ_m, therefore, it is necessary to plot the transmission curve, k, for the glass, the visibility curve, V, for the eye, the energy curve, E, of the source.

The product of corresponding ordinates would give a new curve, the area of which is the numerator of the fraction representing λ_m.

Similarly a curve obtained by dividing each ordinate of the previous

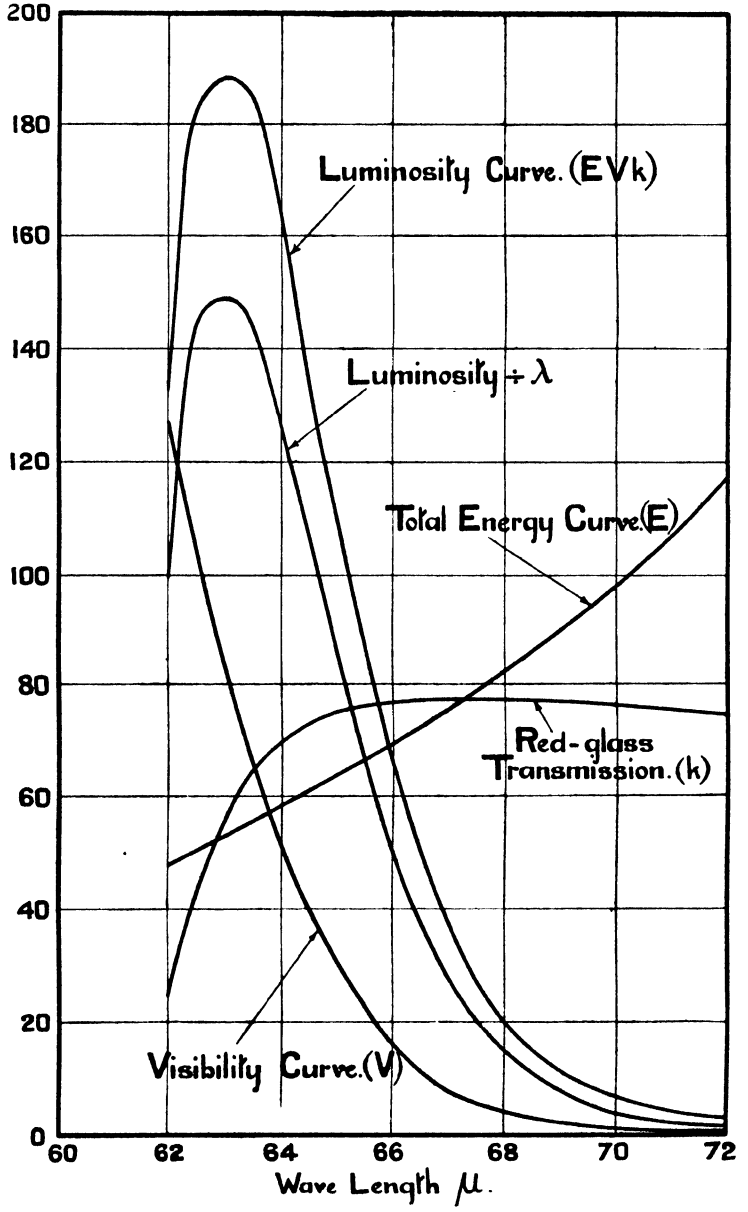


FIG. 79.—Typical curves for calculation of effective wave-length.

curve by its λ would give a curve the area of which is the denominator of the fraction.

A typical series is shown in Fig. 79.

But Foote points out that instead of plotting λ in terms of $E\,k\,V$ as ordinates, the ordinary luminosity curve, we may plot $\frac{V\,E\,k}{\lambda}$ as ordinates. Then the value of λ_m is that the value which corresponds to the centre of gravity of the curve with respect to the $\frac{E\,k\,V}{\lambda}$ axis.

Hence the true effective wave-length of a pyrometer glass is the wave-length corresponding to the centre of gravity of the curve $\varphi(\lambda) = \frac{E\,V\,k}{\lambda}$ plotted in terms of λ—that is, the luminosity at any wave-length divided by the wave-length and expressed in terms of the wave-length.

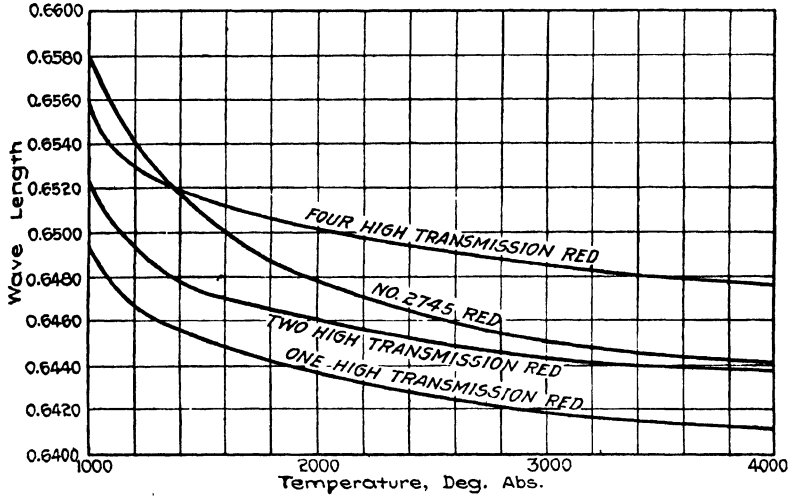


FIG. 80.—Effective wave-length *v s* temperature.

The value of L can be determined for various values of T, and hence a curve found for λ_m as a function of T.

In Fig. 80 is shown the results obtained for typical glasses employed for filter screens.

Effect of Change of Temperature of the Filter Glass on its Transmission Coefficient.—Another factor which influences the transmission coefficient of the red glass is its actual temperature.

Some observations have been made by Forsythe on the transmission curve for a specimen of red glass when maintained at two different temperatures, 20° and 80° C. The results are shown in Fig. 81. Curve A gives the transmission of the glass at 20°, while curve B is the corresponding one when its temperature is 80° C.

The transmission is shown to decrease with increasing temperature, the coefficient of change being greatest in the shorter wave-length. The change is such as to make the transmission band appear to shift to longer wave-lengths as the temperature is increased.

A test was made of the effect of this temperature shift of the transmission band on temperature measurement when the red glass was used as a filter screen before the eyepiece of a pyrometer. The temperature of a carbon filament lamp operated at a temperature of about 1,900° K.* was measured with the red glass temperature at 20° and 80° C., using a sector disc with a 2° angular opening, as this gives a larger effect than a sector disc of greater transmission. It was found that there was a decrease of about 5° C. in the apparent temperature obtained when the glass was heated to 80° over that obtained with a glass at room temperature. Hence it may be inferred that for all ordinary changes of room temperature the effect is negligible.

Spectroscopic Eyepiece.— Practically all modern optical pyrometers have red filter glasses for producing approximate monochromatic radiation, and, as shown above, it is possible to obtain the effective wave-length of such a glass, which is equivalent for the purposes of calculation to the case of perfect monochromatism.

The early forms of optical pyrometer of the polarising type had direct-vision prisms in place of filter glasses, but practical requirements demanded that the slit opening should be so wide that the spectral band transmitted was no better than that transmitted by a filter glass. If, however, the conditions of the experiment are such that narrower slits are possible, the system offers certain advantages. Mendenhall, in some of his work on the disappearing type of optical pyrometer, used a spectroscopic eyepiece. The fitment consists of a small auxiliary eyepiece, and a totally reflecting prism which slides in a side tube just below the lamp. The images of the comparison filament and of the hot surface are thrown in sharp focus across the middle of the spectroscope slit by means of an intermediate achromatic lens, the primary image of the hot surface having previously been brought into the plane of the comparison filament in the usual way.

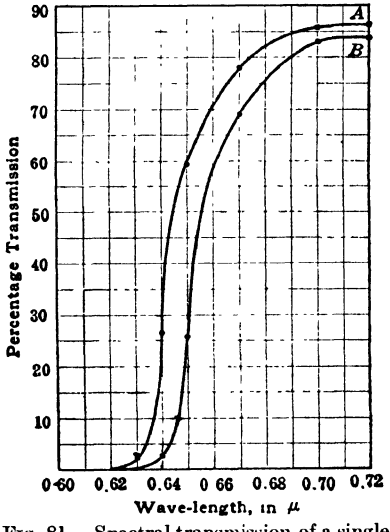


FIG. 81.—Spectral transmission of a single thickness of glass. F. — 4,512; A, at 20° C.; B at 80° C.

The eyepiece and ocular slit of variable width are movable with a

* The symbol K denotes the absolute thermodynamic scale of temperature.

micrometer screw, giving about 500 divisions for the visible spectrum, and it is easy to work with an ocular slit covering not more than 25 A.U. (0·0025 μ). The field then shows a central band due to the filament bounded by light from the hot object.

A comparative series of tests on the same conditions, employing in the one case a spectroscopic eyepiece and in the other a piece of red Jena glass having a maximum ordinate at $\lambda = 0{\cdot}652\ \mu$, is given below. The distribution of light in the transmission spectrum of the red glass was determined by spectrophotometric observations.

TABLE XXVII.

Temperature C. Red Glass.	Temperature C. Spectroscopic Eyepiece.
1,063	1,062
1,858	1,861
1,990	1,990
2,000	1,995
2,370	2,380

Absorption Devices.—The absorbing device sometimes used with the disappearing filament type of instrument consists of two black glass mirrors inclined at an angle of 45°. In this arrangement the beam of light from the hot body is reflected twice at an angle of 45° incidence and thereby weakened to about $\frac{1}{200}$ of its original intensity, thus allowing continuous observations to be made up to about 2,700° C. without risk of over-running the pyrometer lamp.

Another form of absorption device is a piece of neutral-tinted glass interposed in the path of the beam.

The use of a rotating sectored disc has already been mentioned in connection with the work of Mendenhall and Forsythe.*

Calculation of the Constant of an Absorption Glass.—It is assumed that the absorption glass cuts down the intensity of the light in the spectral band dealt with in the ratio of k to 1.

If T_1 is the observed temperature without absorption glass, and T_2 the apparent temperature of the same object with absorption glass—

* When using a rotating sector in conjunction with a "disappearing filament" type of pyrometer, for the determination of the temperature of lamp filaments, they found that if the sector was mounted near the lens with the opening of the sector parallel to the axis of the filament when passing the centre of the lens, the definition was bad. On the other hand, if the opening was perpendicular to the filament the definition was quite good.

The best position for the sector is near the lamp, since then the definition is practically independent of the position of the opening of the sector relative to the filament when crossing the field. This trouble was not encountered when taking the temperature of large objects.

By Wien's law $$E = \frac{c_1}{\lambda^5} e^{-\frac{c_2}{\lambda T_1}}$$

$$K E = \frac{c_1}{\lambda^5} e^{-\frac{c_2}{\lambda T_2}}$$

Hence $$\log_2 K = \frac{c_2}{\lambda}\left(\frac{1}{T_1} - \frac{1}{T_2}\right)^*$$

where c_2 is a numerical constant about 14,350 micron degrees; and λ for the usual red glasses 0·6 to 0·7 μ.

Hence $\left(\frac{1}{T_2} - \frac{1}{T_1}\right)$ is a constant quantity.

Rotating Sector Method of Reducing the Intensity by a Calculable Amount have been advocated by some observers for cutting down the intensity, since it is then possible to obtain the coefficient of transmission by actual measurement of the sector.

(1) THE SECTORS.—Mendenhall employed sectors 13·5 cms. in diameter with the disappearing filament type of instrument. With discs of this diameter it was found possible to cut radial openings as small as 3°, giving a factor of $\frac{1}{120}$.

The absence of any error due to diffraction was proved by comparing the effect of ten equal and separate openings with that due to a single opening of the same total area.

The range of temperature available with various-sized sectors is illustrated by the following example :—

A pryometer calibrated with full aperture had a scale covering the range up to 1,553° C. (melting-point of palladium); with a $\frac{1}{60}$ sector the range was from 1,755° to 2,482° C.; and with a $\frac{1}{180}$ sector the scale was extended to include the melting-point of tungsten (3,300° C. approx.).

For the very small apertures it is advisable to use a large disc; Mendenhall employed one of 27 cms. diameter with an opening of 1·7 mms. at its narrowest part, whilst sectors 35 cms. in diameter or bigger are desirable in precision work.

Table XXVIII. gives the transmission value of a number of sectors and the apparent temperatures T_2.

(2) SPEED OF ROTATION OF THE SECTORS.—Forsythe has investigated the speed necessary for rotating sectors, and his conclusions are :—

"The sector must rotate at such a speed that no flicker is noticeable. To accomplish this the alternations must be at least 30 to 40 per second. This is for the condition where the open and closed spaces of the sector are about equal in size. If there is a very great difference between the open and closed parts of the sector, as, for instance, in the case of the 2° sector with two 1° openings, the speed must be higher. If the motor available will not rotate the sectors fast enough when there is but one opening and

* This expression is also applicable for calculating the small absorption effect of a glass window closing a furnace.

TABLE XXVIII.—Temperature corresponding to Different Percentages of the Radiation from a Black Body at the Temperature of Melting Palladium (1,828° K.), using Red Glass with an Effective Wave-length which varies as is shown in Column 2.

$c_2 = 14{,}350\ \mu$ degrees.

Transmission of Sector.	λ_m.*	T_2 Deg K
0·749	0·6652	1,785
·499	·6653	1,727
·2443	·6655	1,632
·0830	·6657	1,509
·0336	·6658	1,426
·01668	·6659	1,356
·00542	·6662	1,267

one closed part, it is often a great help to make more open spaces. A good plan is to have six openings, which will reduce the necessary speed considerably. For a small sector having a 1° opening this is impossible without making the sector too large, because if the sector opening is too small there is danger of an error due to diffraction. In this case, with a sector 35 cms. in diameter, it is not necessary to have a motor that will rotate it something like 3,500 r.p.m.

"In Fig 82 are shown the values found for the transmission of a 180° sector as a function of the speed in alternation per second. This transmission was measured with the optical pyrometer. It can be seen, as shown in the curve, that the value found is constant and equal to the transmission of the sector for alterations above about 30 per second, but below that the transmission at first becomes smaller and then larger, and an apparent transmission of over 100 per cent. is obtained for a speed of alternations of about 1 per second. The transmission, of course, approximates 100 per cent. for zero speed.

"The values found for the transmission to alternations between 10 and 30 per second are due to a flicker which bothers the observer. It might be that another observer would get slightly different values for the transmission of such speeds. For speeds slower than 10 alternations per second the observer attempts to make the settings when the open part of the sector is passing before the opening. There is a very great flicker, and settings are attempted, using only the bright part. The value found for extremely low speeds is due to the apparent over-shooting of the brightness of the source when viewed only for a short time as compared with the pyrometer filament, that always has about the same brightness.

"If the sector has a long opening measured in the direction of the radius, care must be taken to always use about the same part of this opening. This

* Last digit in this column approximated. Sectors about 35 cms. in diameter.

is to avoid error due to the fact that the radial sides of the openings may not be straight or may not be in radial direction."

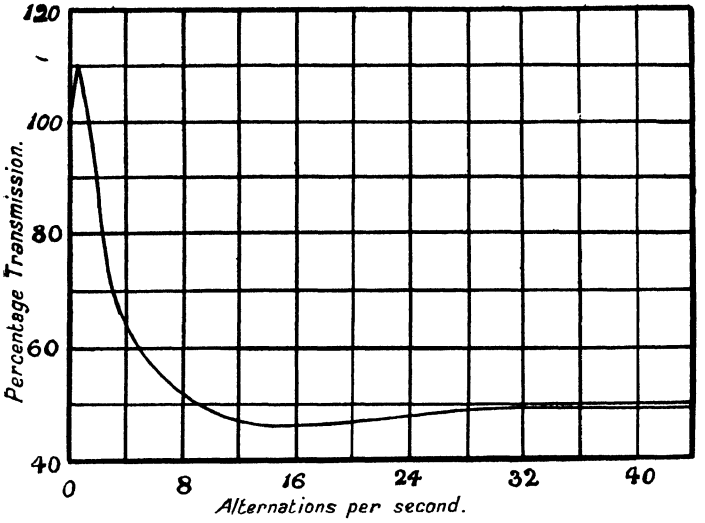


FIG. 82.—Relation between percentage transmission of rotating sector and the frequency of the alternations.

Absorption of Glass for Reducing the Intensity.—For most work the use of a neutral-tinted glass is to be preferred on account of its simplicity, but it has the disadvantage that the effective wave-length shift towards the green with increasing temperature. The best neutral glasses are far from being neutral. The transmission coefficient of the glasses obtainable varies considerably through the visible spectrum.

In Fig. 83 are shown some typical transmission curves for various absorbing glasses. The degree to which it is necessary for the absorbing screen

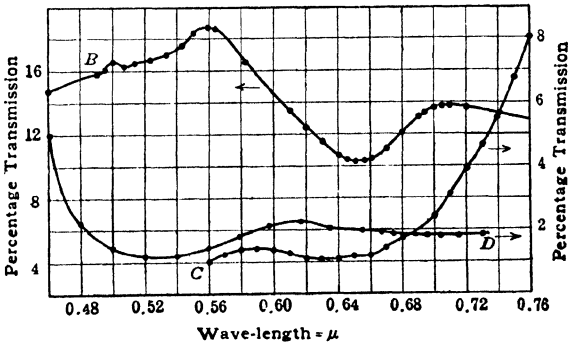


FIG. 83.—Spectral transmission of various absorbing glasses. Curve B, Jena absorbing glass 1·5 mms. thick. Curve C, Noviweld obtained from Corning Glass Works; shade about 6. Curve D, Leeds and Northrup absorbing glass made of purple and green glass.

to have a special transmission independent of the wave-length depends on the monochromatism of the filter glass. It is evident that if the red filter glass is absolutely monochromatic any absorbing glass will be satisfactory. If it transmits a band of appreciable width, then the colour differences are encountered, which renders the matching of the brightness extremely difficult. The total transmission of the absorbing screen when used in conjunction with a red glass in the eyepiece in the usual manner can be calculated for any black body of distribution by the following formula :—

$$\text{Total transmission coefficient} = \frac{\int_0^\infty E\, V\, k_R\, k_B\, d\lambda}{\int_0^\infty E\, V\, k_R\, d\lambda}$$

where E = black body energy for interval λ to $\lambda + d\lambda$ and V = visibility. k_R and k_B = spectral transmission of red and absorbing glasses respectively.

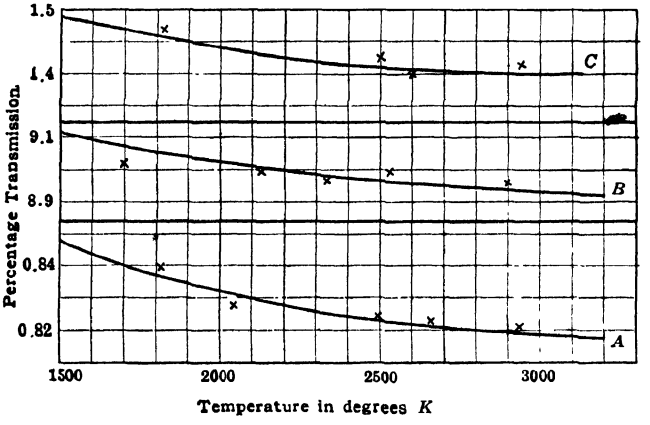


FIG. 84.—Total transmission of absorbing glasses, as a function of temperature when used with red glass No. 4,512, 5·8 mms. thick. Curve A, two pieces Jena absorbing glass. B, one piece Jena absorbing glass. C, Noviweld glass from Corning Glass Works. Crosses represent values of transmission obtained with optical pyrometer.

It is evident that if the spectral transmission of the absorbing glass is different for different wave-lengths, the total transmission will be a function of the temperature of the source under investigation.

In Fig. 84 is shown, as a function of the temperature of the source, the total transmission for red light of the absorbing glasses having the spectral transmission given by curves B and C, Fig. 83.

The data were obtained by Forsythe, who employed a double thickness of the red filter glass, whose spectral transmission is shown in Fig. 81.

Temperature Measurement in Terms of Total Intrinsic Brilliancy.—An empirical method of estimating temperatures which is occasionally used in connection with light sources, such as incandescent lamp filaments, is one developed by Rasch.

He proposed the relationship

$$\log H = -\frac{A}{T} + B$$

for connecting the temperature T (abs.) of a " black body " and its total intrinsic brilliancy H.

It will be observed that this equation is merely Wien's law, in which monochromatic light is replaced by the total radiation visible to the normal eye.

This, of course, is a somewhat questionable assumption, but some support is given to it by the fact that Crova has shown, that for all ordinary light sources giving a continuous spectrum, there is one wave-length for which the monochromatic intensity is proportional to the total intensity. This wave-length is about 0·58 μ.

In order to test Rasch's equation it is necessary to measure the intrinsic brilliancy of a " black body "—*i.e.*, the candle-power per sq. mm. It is a difficult matter to do this with sufficient accuracy on the usual type of uniform temperature enclosure form of " black body," and the following indirect method was adopted by Nernst.

Nernst lamp filaments were measured, and the relation between the watts expended and the candle-power obtained was observed in the usual manner by photometric measurements.

A filament was then set up in front of a " black body " furnace, and at a series of steady temperatures the filament was brought to a temperature when it disappeared against the background—*i.e.*, emitted the same intensity of light.

From the watts expended in the filament the intrinsic brilliancy of the filament, and hence that of the furnace, was obtained.

The actual temperatures of the furnace were obtained by means of a Wanner pyrometer standardised by the melting-point of gold (1,064° C.), and assuming c_2 in Wien's equation to be 14,600.

Rasch's equation was verified within 10° over the temperature range from 1,400° to 2,300° C., and from the experiments the constants of the equation were obtained :—

$$T = \frac{11{,}230}{5{\cdot}367 - \log_{10} K}$$

where K is the intrinsic brilliancy in Hefner candles per sq. mm.

This equation requires a correction factor if employed for taking the temperature of surfaces which are not full radiators.

For example, tungsten has an emissivity of about 0·51 (of a " black body ") for light of $\lambda = 0{\cdot}56\ \mu$.

Hence, if H is the intrinsic brilliancy of a tungsten filament, and K that of a " black body " at the same true temperature, then H = 0·51 K.

Colour Match Method of Determining Filament Temperatures.—A method of estimating the temperature of lamp filaments which has come into extensive use in recent years is that based on colour matching. By the colour

temperature is meant the temperature of a full radiator when its radiation matches in colour the radiation from the incandescent metal. The relation between colour temperature and true temperature for tungsten has been determined by Hyde, Cady, and Forsythe, so that it is now possible to estimate the temperature of the filament of a tungsten lamp by matching its colour against that of a standard whose temperature is known.

In practice the comparison standard is not a "black body," but a combination of a vacuum lamp with a filter. This lamp is run at different voltages to give the desired colour for matching. The lamp filaments to be tested are compared by means of Lummer-Brodhun photometer head with the standard. It is advisable to make the intensities of the light from the lamps and the standard approximately equal to facilitate comparisons of the colours. In the table below are given some data by Hyde for commercial tungsten lamps in which the true temperature, the colour temperature, and the apparent or brightness temperature are compared with the lumens per watt. It might be remarked that the temperature scale is based upon the melting-point of gold as 1,063° C., and the value 14,350 for c_2 in Wien's equation. This gives the value 1,555 for the melting-point of palladium, whereas the value obtained by Day and Sosman was 1,550° C. The difference, however, is practically within the limit allowed for experimental error.

TABLE XXVIIIA.

Melting-point of Tungsten = 3,675° K.

Brightness temperature. ° K	True temperature. ° K.	Corrected for end effects and bulb absorptions.	
		Colour temperature, ° K.	Lumens per Watt.
1,600	1,701	1,714	0·78
1,650	1,758	1,775	1·04
1,700	1,816	1,837	1·40
1,750	1,874	1,898	1·81
1,800	1,932	1,960	2·31
1,850	1,990	2,021	2·90
1,900	2,049	2,082	3·56
1,950	2,108	2,144	4·35
2,000	2,167	2,205	5·26
2,050	2,227	2,266	6·30
2,100	2,287	2,327	7·45
2,150	2,347	2,380	8·69

Above table based on the following constants :—

Melting-point of gold, ... 1,336° K.
Melting-point of palladium, . . . 1,828° K.

These result in Wien's constant c_2 being equal to 14,350 $\mu \times$ deg.

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CHAPTER VIII.

DISTRIBUTION OF ENERGY IN THE HEAT EMISSION SPECTRUM OF THE METALS.

Distribution of Energy in the Heat Emission Spectrum of the Metals.—While Planck's formula is capable of representing with considerable accuracy the distribution of energy among the wave-lengths of the spectrum of a "full radiator," the corresponding problem for a metal has not yet been solved.*

A considerable amount of experimental data has been accumulated, which is of practical value, insomuch as that it permits of the calculation of the corrections to temperature observations on such surfaces when taken with an optical pyrometer calibrated under "black body" conditions.

Unfortunately, however, such corrections can only be regarded as approximations, since it has been shown that the slightest oxide film seriously affects the emissivity of a metallic surface.

The work done on this subject may be roughly grouped under two headings: the one in which experiments have been made with spectral bands of appreciable width, such as those obtained in practical forms of optical pyrometers, and over extended ranges of temperature; the other in which experiments have been made with almost monochromatic illumination for various wave-lengths in the spectrum, the investigation being usually confined to a few steady temperatures.

Emissivity of Iron Oxide.—When iron is heated in air to a temperature of about 800° C. its surface becomes covered with a brittle coating of oxide, apparently consisting of FeO and Fe_2O_3 in various proportions. In appearance the surface is silky and pitted with minute depressions, which produce the same effect as a collection of minute "black bodies," and consequently the surface has a high emissivity. Burgess and Foote have measured the emissivity of this oxide surface.

A small sample of the oxide was heated up on a platinum strip and its apparent temperature observed with a disappearing filament type of optical pyrometer, having a red glass with transmission band at $\lambda = 0{\cdot}65\ \mu$.

* Attempts have been made to apply a modification of Wien's form of equation to represent the distribution of energy in the heat spectra of the metals, such as—

$$E_\lambda = c_1 \lambda^{-\alpha} e^{-\frac{c'_2}{\lambda T}}$$

For platinum Paschen obtained the value 6·4 for α; Lummer and Pringsheim 6·0; while McCauley, in a detailed investigation, was unable to find any constant value of α, to satisfy the equation or a modified form of Planck's.

The true temperature was obtained by placing on the platinum strip minute specimens of NaCl, Na_2SO_4, and Au.

The table below gives the emissivity of the oxide surface at various temperatures.

TABLE XXIX.

Melting-point of	True temperature, °C.	Apparent temperature, °C.	Average deviation from mean.	Emissivity.
NaCl	801±1	801	±1·5	1·00
Na_2SO_4	884±1	882	±3	0·97
Au	1063±2	1,058	±2	0·94

The emissivity was calculated by the equation—

$$\frac{1}{T} - \frac{1}{S_\lambda} = \frac{\lambda}{\cdot 4343 c_2} \log E_\lambda,$$

where T is the true temperature,

S_λ is the observed temperature,

λ is the wave-length of light considered (measured in μ units),

The emissivity appears to decrease slightly with increasing temperature, which is the case also with nickel and other oxides.

The authors ignore the observation at 801° C., and by extrapolation —assuming a straight line—obtain the following corrections to reduce apparent to true temperatures :—

Observed temperature, °C., .	600	700	800	900	1000	1100	1200
Correction, °C., . . .	0	0	+1	+2	+4	+6	+10°

Emissivity of Copper and Cuprous Oxide.—Burgess investigated the emissivity of a clear copper surface and one of the oxides, employing the disappearing filament type of pyrometer with red ($\lambda = 0{\cdot}65\ \mu$) and green ($\lambda = 0{\cdot}55\ \mu$) glasses.

The copper was contained in shallow crucibles of magnesia and graphite, about 8 cms. inside diameter. These were heated in a gas furnace, and by regulating the gas and air supply, it was possible to obtain either the clear metal surface or the oxide surface. The crucible was set in the furnace so that the flames could not play on the surface, and also in such a position as to avoid direct radiation from the walls of the crucible into the pyrometer.

In the case of the rough oxide surface diffuse reflection from the surface might vitiate the observations. But when sighting on the mirror-like surface of the molten metal only specular reflection was possible, and there could

be no error due to this cause, unless the image of some hot object was actually visible in the telescope.

Temperatures were measured by means of a thermoelement bent into the form of a crook.

From the observations the following equations were deduced, in which t is the true temperature and s the apparent.

Clear Molten Copper Surface.

Red light ($\lambda = 0{\cdot}65\ \mu$)

$$t = 1{\cdot}515\ s - 359$$

Green light ($\lambda = 0{\cdot}55\ \mu$)

$$t = 1{\cdot}515\ s - 477$$

Hence at the melting-point the apparent temperature, with the red glass, is too low by 130°.

The green glass gives a temperature 78° higher than the red glass throughout the range.

Burgess states that in deducting the equations a slight allowance was made for the fact that the optical readings would tend to be too high on account of the slightest traces of impurity on the copper surface.

The maximum difference between the observed and computed values of the temperature over the range 1,073° to 1,200° C. was about 13°.

Cuprous Oxide Surface.—The formation of an oxide film caused an apparent increase of 100° in the temperature of the molten copper when observed with the red glass, and 35° in the case of the green glass.

The smaller increase with the green glass is due to the fact that molten copper radiates strongly in the green. This greenish appearance persists in the case of incandescent solid copper as may be observed by adjusting the gas feed to remove surface oxidation.

The relation between the apparent and true temperatures, in the case of the oxide, is not quite linear. This can be seen by a consideration of the data in Table XXX., which refer to the red light of wave-length $\lambda = 0{\cdot}65\ \mu$.

TABLE XXX.

Molten copper.		Cuprous oxide.	
Pyrometer reading, °C	True temperature, °C.	Pyrometer reading, °C.	True temperature, °C.
950	1,082	900	903
975	1,118	950	958
1,000	1,156	1,000	1,020
1,025	1,193	1,050	1,087
1,050	1,231	1,100	1,159
		1,150	1,233

TABLE XXXI.—Emissivities.

Molten copper.			Cuprous oxide.		
Temperature, °C.	$\lambda = 0{\cdot}65\ \mu$.	$\lambda = 0{\cdot}55\ \mu$.	Temperature, °C.	$\lambda = 0{\cdot}65\ \mu$.	$\lambda = 0{\cdot}55\ \mu$.
1,075	0·17	0·47	1,000	0·80	—
1,125	0·15	0·38	1,100	0·60	0·68
1,175	0·14	0·32	1,200	(0·49)	(0·49)
1,225	0·13	0·28			

Emissivity of Solid and Liquid Gold.—Gold is one of the metals which does not oxidise appreciably when heated.

Both copper and gold emit greenish or bluish light at high temperatures. Stubbs and Prideaux made a study of the emissivity of gold. The radiation of the various wave-lengths was measured by means of a König spectrophotometer and direct comparison made with the radiation from a " black body " at the same temperature.

The metal was contained in a silica capsule of 4·5 cms. diameter and 6 mms. deep. The " black body " was placed in exactly the same position for the second experiment. It consisted of a cylindrical graphite block, 11 cms. long, 5 cms. in diameter, in the centre of which a hole 12 mms. in diameter by 9 cms. deep was bored.

True temperatures were obtained by means of thermocouples.

In the case of the gold the two couples dipped into the metal, one on either side of the field of view. Owing to the shallowness of the depth of immersion an error of the order of 6° at 1,000° C. was introduced in the observed readings. A correction was applied, this being determined by observing the apparent freezing-point. Two couples were also embedded in the graphite. The black body conditions were sufficiently perfect to make it impossible to distinguish the white thermocouple when it projected into the central hole.

Impurities or Inequalities in the Gold Surface.—Any slight surface film present was found to produce an increase in the red radiation in which the gold spectrum was weak.

The impurities were got rid of in the case of the molten surface by the application of borax.

The solid gold surface proved to be more difficult to obtain free from oxide.

It was found that a surface turned flat, treated with four grades of fine emery powder and then with jeweller's rouge, gave an apparently perfect mirror. On heating, however, a conspicuous red film was produced. This film could be removed by repeatedly treating the surface with borax at a temperature near the melting-point. Although a clear, solid gold surface was obtained when the liquid solidified, it was generally uneven owing to

contraction, crystallisation, etc., and consequently reflected heat from the furnace walls into the spectrophotometer.

Occasionally by very slow cooling an area could be obtained which was free from unevenness.

The following values were obtained for the emissivity of molten gold at the temperature of its freezing-point :—

TABLE XXXII.—Emissivity of Gold in the Molten State.

Wave-length,	0·7014	0·6712	0·6409	0·6149	0·5895
Emissivity, .	0·184	0·203	0·232	0·263	0·304
Wave-length,	0·5649	0·5418	0·5186	0·4961	0·4750
Emissivity, .	0·347	0·390	0·434	0·473	0·503

For solid gold at various temperatures the values in Table XXXIII. were obtained. The data are shown graphically in Fig. 85.

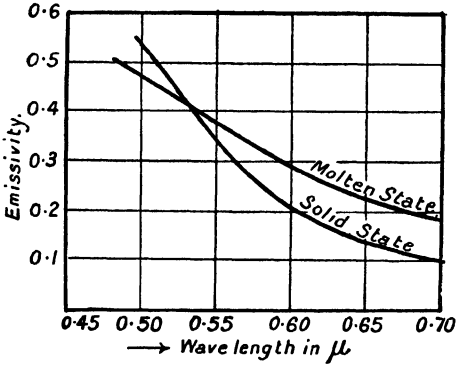


Fig. 85.—Diagram to illustrate emissivity of gold.

Stubbs and Prideaux observed that in passing from the solid to the molten state a sharp discontinuity occurred in the emissivity wave-length relationship, the relative emissivity increasing in the red and decreasing in the violet. Roughly the emissivity for red light of the solid gold is only about three-fifths that of molten gold.

For the limited range of temperature investigated (110° C. in the case of molten state) no change of the relative emissivity of either molten or solid gold with temperature was observed.

TABLE XXXIII.—Emissivity of Gold in the Solid State.

Wave-lengths.	Temperature, °C.				Mean emissivity.
	949°.	1040°.	1061°.	1046°.*	
0·7014	[0·164]	[0·134]	0·103	0·103	0·103
0·6712	[0·146]	0·114	0·114	0·116	0·114
0·6409	[0·169]	0·144	0·143	—	0·143
0·6149	[0·198]	0·172	0·171	0·178	0·175
0·5895	0·241	0·229	0·221	—	0·229
0·5649	0·315	0·291	0·289	0·361	0·301
0·5418	0·379	0·371	0·366	—	0·371
0·5186	0·520	0·465	—	0·516	0·494
0·4961	0·595	0·492	—	0·541	0·531

From the above values of the emissivities the "black body" or true temperatures corresponding to various values of the apparent temperatures can readily be calculated from the relationship :—

$$\frac{1}{T} - \frac{1}{S_\lambda} = \frac{\lambda}{c_2} \log_e \frac{E_\lambda'}{E_\lambda}$$

where $\frac{E_\lambda'}{E_\lambda}$ is the emissivity for wave-length λ.

The data below give the apparent temperatures by Wien's equation for various wave-lengths corresponding to a true temperature of 1,063·2° C.

TABLE XXXIV.—True Temperature, 1,063·2° C.

Wave-length in μ.	Apparent temperature, °C.	
	Solid state.	Molten state.
0·7014	891·5	931
0·6409	925·5	956·5
0·5895	964	982
0·5418	1,000	1,003
0·4961	1,025·5	1,019

Solid and Molten Copper and Silver.—An investigation on the same lines as the above described in the case of gold was carried out by Stubbs for the metals silver and copper.

Copper.—The metal was contained in a silica pot and heated in a closed furnace with a hydrogen atmosphere, the observations being taken through a glass window (microscope cover glass).

* Data given in this column refer to a surface naturally crystallised from the molten state. Values enclosed in brackets [ ] were obtained with a surface having a slight film over it.

The block of copper (4·2 cms. diameter) was turned up to a flat surface, rubbed smooth with emery paper, and polished with metal polish. The use of rouge was avoided as it was found to tarnish on heating. No trace of filming was observed, and the surface showed no deterioration until a temperature of about 10° from the melting-point had been attained, when recrystallisation rapidly set in, and this produced stray reflection of light from the furnace walls into the photometer, owing to the roughening of the surface.

A perfect mirror of molten copper, free from film, was obtained without difficulty.

The emissivities for the solid and molten copper for various wave-lengths are shown in Fig. 86. The values are for a temperature of 1,010° C. for solid copper and 1,130° C. for molten copper. As in the case of gold, there is a discontinuity at the melting-point, but of smaller magnitude.

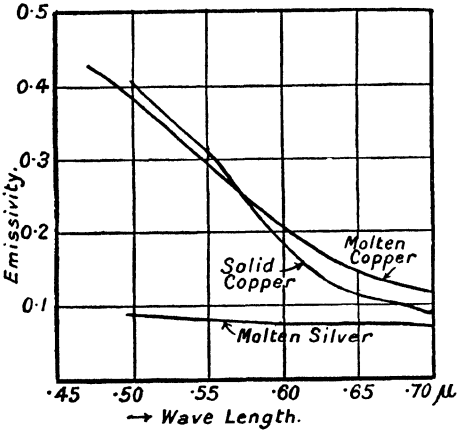


FIG. 86.—Diagram showing emissivities of solid and molten copper.

The values differ markedly from those obtained by Burgess described above.

This may be due to the fact that the experimental conditions in Burgess' work were less favourable, and that the red glass of his pyrometer transmitted a comparatively wide spectral band (100 μ), while the width of the band in the photometer employed by Stubbs and Prideaux was 8 μ.

Silver.—It was unnecessary to take the extreme precautions for the exclusion of oxygen in the case of silver as for copper. A satisfactory reducing atmosphere was produced by placing a small quantity of powdered graphite in the furnace below the crucible containing the silver. The solid metal surface lost its polish on heating, so that no measurements could be made of its true emissivity.

The emissivity of the molten surface for various wave-lengths is shown in Fig. 86.

There appeared to be a slight increase in the relative emissivity with

temperature, but owing to the small magnitude of the coefficient the authors are in some doubt as to its real nature.

In Table XXXV. the apparent temperatures corresponding to the various wave-lengths at the melting-points of the metals are given.

TABLE XXXV.

Wave-length in μ.	Copper, m.p. 1083° C. Apparent temperature. (Solid.)	Copper, m.p. 1083° C. Apparent temperature. (Liquid.)	Silver, m.p. 961° C. (Liquid). Apparent temperature.
700	896	917	792
650	924	942	804
600	966	973	816
550	1,007	1,003	831
500	1,028	1,026	845

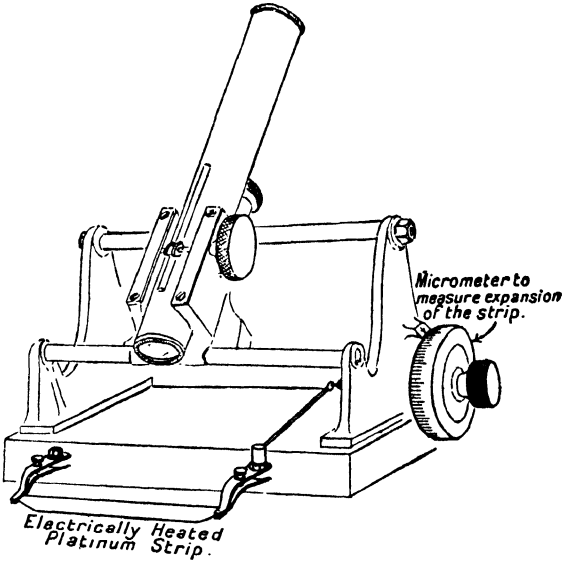


FIG. 87.—Illustration of Joly's meldometer.

Emissivity of Polished Platinum.—The permanency of a polished platinum surface greatly simplifies the study of the emissivity of the metal at high temperatures.

Holborn and Kurlbaum, and Waidner and Burgess have independently investigated the difference between the apparent and true temperatures for approximately monochromatic radiation of a platinum surface. The former employed a small box of platinum, with a thermocouple in the interior, to give the true temperature, the apparent temperature being obtained by means of an optical pyrometer.

The latter worked with a Joly meldometer (Fig. 87).

The apparent temperature of the strip was determined with a "disappearing filament" type of optical pyrometer. This was calibrated under "black-body" conditions by comparison with a thermocouple up to 1,150° C., which temperature, at the time (1904), marked the upper limit of reliable gas thermometry work.

The thermo-electric formula was extrapolated to about 1,350° C., and beyond this point the calibration of the optical pyrometer was extended by means of Wien's law.

True temperatures were obtained by calibrating the strip by melting-points of pure metals and salts.

The electric contact micrometer permitted of accurate determinations of lengths corresponding to the melting-temperatures of minute specimens heated on the strip.

In the observations of the "apparent temperature" the current through the strip was regulated to keep the length of the strip constant at a measured value.

The following "fixed points" were assumed for the calibration of the strip :—

TABLE XXXVI.

Melting-point.	Value accepted by W. and B. °C.	Value on the Day and Sosman scale. °C.
Palladium, . . .	1,500	1,549
Gold, ...	1,064	1,063
Sodium chloride, . .	782	801
Potassium bromide, . .	723	730

The apparent temperature corresponding to the melting-point of platinum was obtained by increasing the temperature of the strip until it fused.

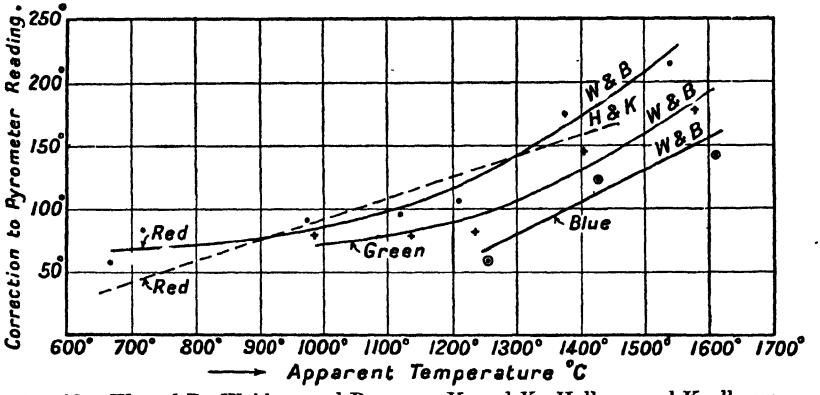


FIG. 88.—W. and B., Waidner and Burgess ; H. and K., Holborn and Kurlbaum.

For this melting-point Waidner and Burgess assumed the value 1,780° C., which. according to Day and Sosman, is 25° too high.

In Table XXXVII. and Fig. 88 the data have been recalculated on the basis of the standard scale of temperature referred to in Chap. I.

The curves given in Fig. 88 differ considerably from the original of Waidner and Burgess, in which the lines terminate at the temperature of the melting-point of palladium.

TABLE XXXVII.

RED LIGHT $\lambda = 0{\cdot}651\ \mu$.

Apparent temperature, °C.	True temperature, °C.	Difference, °C.
1,541	1,755 *	214
1,374	1,549 †	175
1,209	1,315	106
1,119	1,215	86
973	1,064	91
717	801	84
666	723	57

GREEN LIGHT $\lambda = 0{\cdot}550\ \mu$.

Apparent temperature, °C.	True temperature, C.	Difference, °C.
1,577	1,755 *	178
1,403	1,549 †	146
1,233	1,315	82
1,136	1,215	79
985	1,064	79

BLUE LIGHT $\lambda = 0{\cdot}474\ \mu$.

Apparent temperature, °C.	True temperature, °C.	Difference, °C.
1,612	1,755 *	143
1,426	1,549 †	123
1,256	1,315	59

(Day and Sosman's values.)

The values for red light obtained by Holborn and Kurlbaum are shown by the dotted line in Fig. 88.

Distribution of Energy in the Spectra of Platinum, Palladium, and Tantalum.—McCauley has investigated the distribution of energy in the heat spectra of platinum, palladium, and tantalum over a wide range of temperature.

* Melting-point of platinum. † Melting-point of palladium.

The experiments were made on electrically heated strips 3·5 cms. long, 0·05 mm. thick, by 7 mms. wide, folded into wedge-shaped filaments with 12° angular opening.

The " true temperature " was deduced from observations of the radiation from the interior of the wedge, using a disappearing filament type of optical pyrometer.

The distribution of energy was obtained with the usual spectro-bolometric arrangement.

With tantalum great precautions had to be taken to obtain the highest vacuum in the enclosure containing the filament. The slightest trace of residual gas would cause the resistance to increase rapidly and the metal would become brittle, losing its metallic appearance.

If the vacuum was satisfactory the metal after heating remained bright and ductile except for a slight flaking off at the highest temperatures.

The spectral energy curves for platinum, palladium, and tantalum were perfectly continuous and showed no bands of selective emission. They resembled generally those of a " black body," but no modifications of Wien's or Planck's formulæ were found capable of resembling the curves over the range. Taking the general form of Planck's equation—

$$E = c_1 \lambda^{-a} \frac{1}{e^{\frac{c_2}{\lambda T}} - 1}$$

and determining a mean value of a from the data of a given isothermal curve, McCauley found that the computed emission for palladium was in general from 4 to 7 times smaller than the observed value at 6 μ. The agreement was better for shorter wave-lengths and correspondingly worse for longer ones.

For all three metals the emission diminishes more rapidly than that of a " black body " at the same temperature in the infra red.

The wave-length of maximum emission shifts much more slowly towards the shorter wave-lengths for increasing temperature than for a " black body," especially at the higher temperatures. The product $\lambda_m T$ increases with temperature, and the constant value for platinum found by Lummer and Pringsheim is probably in error. Their value of $\lambda_m T = 2{,}620$ is correct only in the neighbourhood of 2,000° abs.

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Emissivity of Polished Platinum.

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CHAPTER IX.

HIGH TEMPERATURE MELTING-POINTS AND BOILING-POINTS.

For temperature measurements beyond 1,600° C. it is necessary to employ some type of pyrometer based on the laws of radiation. Hence it is necessary either to make the experimental arrangements such that "black body" conditions are obtained, or determine the emissivity of the material by experiment, so as to correct "apparent temperatures" to "true temperatures."

A practical difficulty frequently encountered is the prevention of chemical reaction between the material and the container, since in the case of very high temperatures the range of substances capable of being used in the manufacture of crucibles, etc., is a limited one.

The researches described below illustrate the procedure which has been followed in certain cases and may serve as a guidance in analogous determinations.

Melting-points of Refractory Oxides.—Kanolt has redetermined the melting-points of lime, magnesia, alumina, and chromium oxide.

An Arsem graphite spiral furnace was employed for heating and temperatures measured with a disappearing filament type of optical pyrometer.

The Arsem furnace is designed for working *in vacuo;* in this case, however, it was found that the vaporisation of some of the oxides at high temperatures made observations impossible under reduced pressure conditions. Consequently the furnace had to be rearranged so as to permit of working with atmospheric pressure inside.

To diminish heat loss from the resistor the Arsem furnace is provided with a shield consisting of a cylindrical-shaped box of graphite filled with powdered magnesia or graphite. The shield surrounds the heater without being in actual contact with it.

Kanolt modified the standard form by substituting a smaller heater and adding a second shield—placed within the first—filled with powdered graphite.

The refractory oxide was contained in a crucible with re-entrant tube (see Fig. 75), or was formed into a long narrow crucible which could be carried from the top of the furnace.

Except in the case of lime, the material itself was not directly under observation, consequently to determine the melting-point a heating up curve was taken and the halt at the melting observed, the rate of heating being of the order of 100° C. per minute.

The accuracy of the method was checked by observations with samples taken to temperatures just below and just above the temperature at which the halt occurred and noting the change in appearance when cold.

Most oxides react with carbon at high temperature to form carbides, the only exception being the oxide of magnesium (MgO), which, however, is slowly decomposed by carbon with the formation of carbon monoxide and magnesium vapour. In consequence of this the volatilisation after fusion is very rapid.

Some difficulty was encountered in the early experiments owing to the formation of smoke which interfered with the temperature observations; this was overcome by the usual method of passing a stream of gas into the interior of the furnace.

Lime (CaO).—Two methods were employed in the examination of this oxide. In the first the material was in the form of a long closed tube supported from the upper end, and observations were made by sighting into the interior on the bottom surface. To clear away fog a gentle stream of hydrogen was passed into the tube.

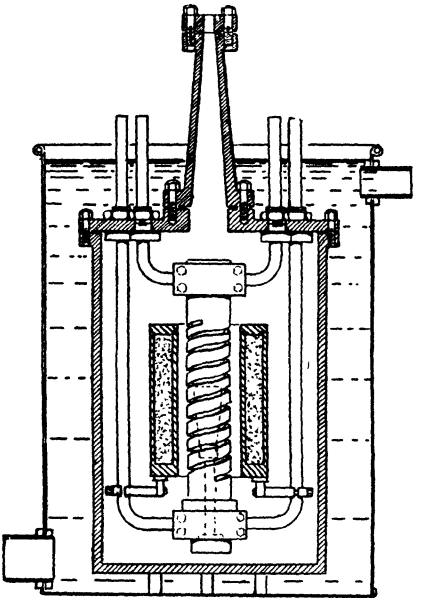


FIG. 89.—Arsem furnace.

It was observed that the parts melted were perfectly white, while the upper portions, which had been submitted to a lower temperature, were grey. The explanation suggested by Kanolt is, that the grey material is calcium carbide, produced by the reaction of the lime and the carbon "spluttered" on to the tube. At higher temperatures any carbide formed would react with the lime, forming carbon monoxide and calcium vapour, consequently the grey appearance would be confined to the lower temperature zone.

In the second method crucibles of tungsten were employed.

By moulding powdered tungsten and then heating rapidly to high temperatures, it is possible to manufacture hard, porous, metallic crucibles. The lime, when melted, was absorbed by the porous material; this, however, did not interfere with the observations.

The value 2,570° C. was found for the melting-point.

Magnesia (MgO).—This oxide was melted in a graphite crucible with re-entrant tube.

After fusion the magnesia was a colourless, fairly transparent, solid of compact crystalline structure.

The value 2,800° C. was obtained for the melting-point, with an average deviation of 13° from the mean.

Alumina (Al_2O_3).—Alumina reacts with carbon to form a carbide, but since the reaction takes place very slowly the melting-point could be determined with graphite containers. After melting the material was white, but on prolonged exposure to high temperatures it became grey.

The same values were obtained with both graphite and tungsten crucibles, the melting-point being 2,050° C.

Alumina is not so volatile as most oxides at high temperatures, and experiments could be made in a vacuum of two millimetres of mercury.

Chromium Oxide (Cr_2O_3).—With this oxide both tungsten and graphite crucibles were tried.

In the case of the tungsten crucibles the melted oxide soaked into the porous tungsten to a considerable extent, while with the graphite crucibles *in vacuo*, vigorous reduction of the oxide occurred on melting.

The value obtained by both methods was 1,990° C.

TABLE XXXVIII.—MELTING-POINTS OF REFRACTORY OXIDES (*Kanolt*).

Substance.	Melting-point, °C.
Lime,	2,570
Magnesia,	2,800
Alumina,	2,050
Chromium oxide,	1,990

TABLE XXXVIIIa.—MELTING POINTS OF COMMON REFRACTORY MATERIALS.

Material.	Temperature, °C.
FIRE BRICKS—	
Fireclay,	1,500-1,750
Silica,	1,700-1,750
Magnesia,	2,150
Bauxite,	1,600-1,800
Chromite,	2,050
CLAYS AND SANDS—	
Kaolin, $Al_2O_3\ 2SiO_2(2H_2O)$,	1,740
Fireclays,	1,400-1,740
Bauxite clays,	1,800
Bauxite, $Al_2O_3(2H_2O)$,	1,820
Chromite, $FeO\ .\ Cr_2O_3$,	2,180
Silica,	1,750
Silica sands,	1,700-1,750
MISCELLANEOUS—	
Coal ash,	1,100-1,500
Alundum cements,	1,750-2,000

Softening Points of Coal Ash.—Coal ash is a complex mixture of oxides and silicates, and has no definite melting point. It is, however, of considerable technical importance to have data concerning the clinkering tendency of various samples, and the subject has received detailed study by Messrs. Fieldner and Hall.

They accepted as criterion of the clinkering tendency the value of the " softening " or flowing temperature of the ash in the form of a cone.

These cones were made by grinding the ash in an agate mortar with 10 per cent. dextrin solution into a plastic mass. This material was pressed into a shaped groove in a brass mould, the surface of which had been previously moistened with paraffin oil to prevent sticking. The cones were then dried and mounted on a base of kaolin and alumina. In the test the temperature of the furnace was raised at a rate of 10° to 15° per minute

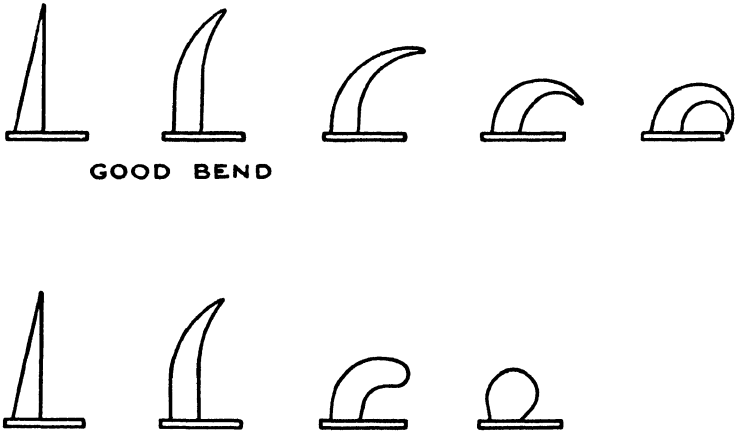


FIG. 90.—Typical coal ash cones.

up to a point not less than 200° C. below the probable softening point and then at a much slower rate.

The softening point was taken as the temperature when the apex of the cone had bent over to touch the base, or failing to bend, had fused down to a lump or ball. The sketch in Fig. 90 shows the appearance of two typical cones at the initial and final deformation points and at several intermediate points of deformation.

The nature of the atmosphere proved to be the most important factor influencing the softening point. The highest softening points were obtained in air or a strongly reducing atmosphere of carbon monoxide, since the latter prevented the iron oxide from acting as a fluxing agent by reducing it to metallic iron before the softening of the ash began. The lowest softening temperatures were obtained in those atmospheres of mixed gases in which reduction of ferric oxide proceeded mainly to ferrous oxide—the most active

phase of iron as regards slag formation at lower temperatures. Such was the case with the atmosphere within the molybdenum furnace. The variations in softening temperatures due to different atmospheres ranged from 14° to 500° C.

The molybdenum* furnace employed is illustrated in Fig. 91.

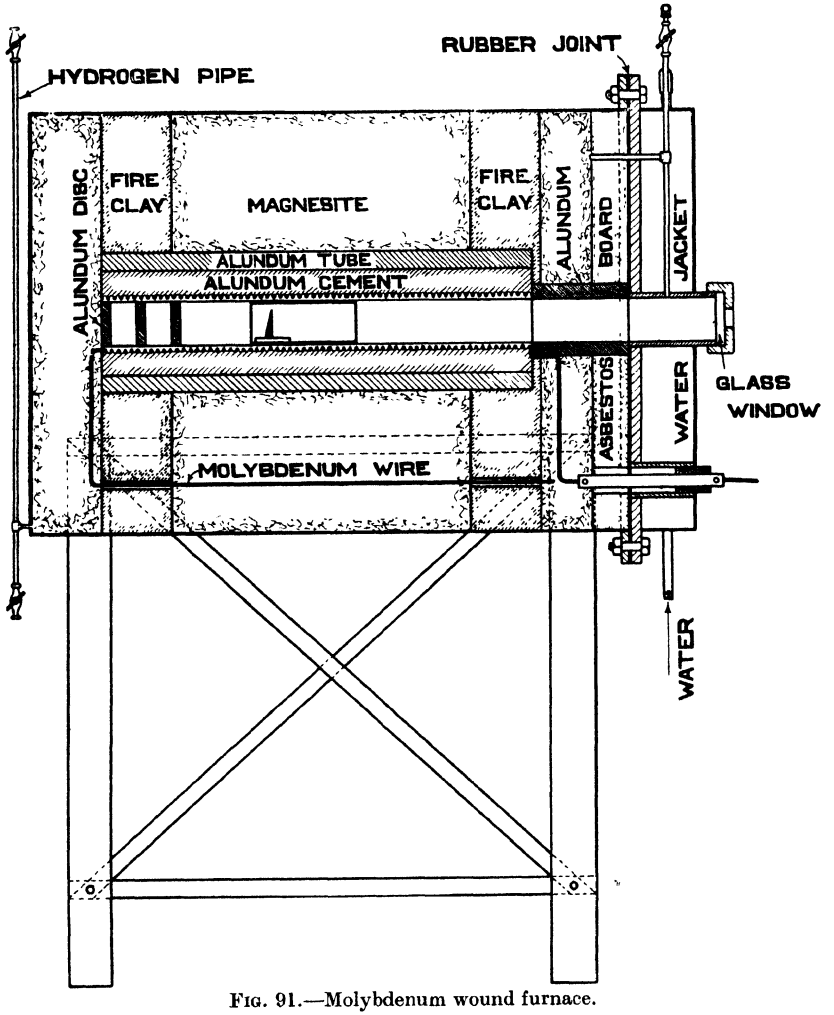


FIG. 91.—Molybdenum wound furnace.

The furnace was operated with a hydrogen atmosphere; similar tests were carried out in an atmosphere of air obtained in a platinum-wound furnace and in an atmosphere of CO with a graphite spiral furnace.

* Molybdenum has a melting point of 2,840° K. $\pm$ 40° according to Pirani and Alterthum. *Zeit. Elektrochem.*, **29**, p. 5, 1923.

Melting-points of the Elements of the Iron Group—Nickel, Cobalt, Iron, Manganese, and Chromium—also of Vanadium and Titanium.—Burgess has devised a valuable instrument, which he terms a *micropyrometer*, for the determination of the melting-points of minute specimens of materials.

The apparatus is somewhat similar to a Joly meldometer, with a microscope pyrometer.

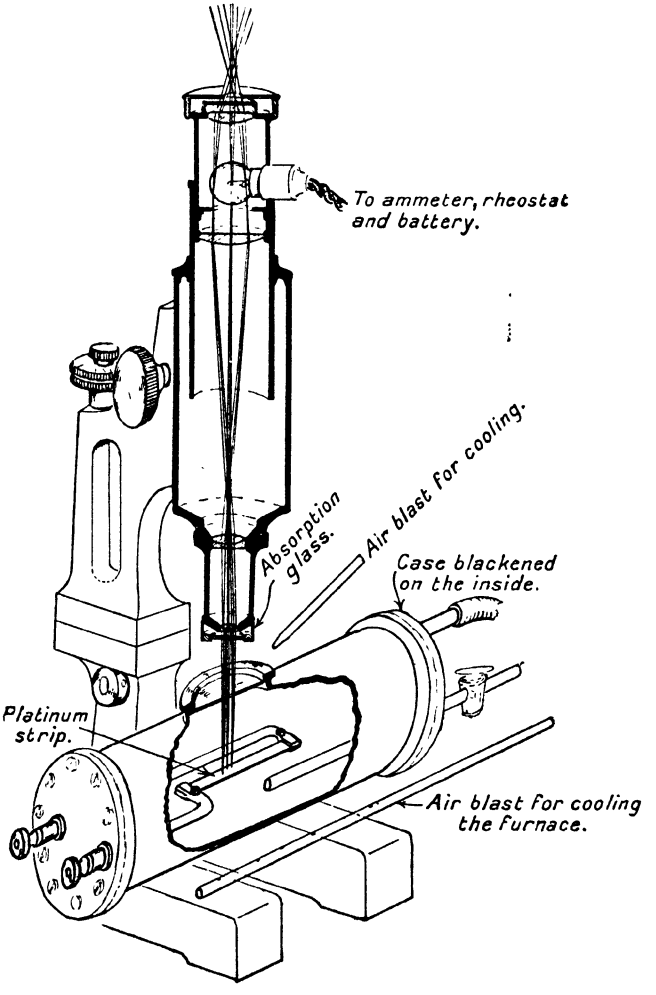


FIG. 92.—Burgess' micropyrometer.

Fig. 92 illustrates the essential features of the instrument.

Within the Huyghens eyepiece of an ordinary microscope a small incandescent lamp is mounted. In series with the lamp there is an ammeter and rheostat operated in precisely the same manner as in the case of a

disappearing filament type of optical pyrometer. The eyepiece of the microscope is fitted with a piece of good red filter glass.

For temperatures exceeding 1,400° C. an absorption glass is placed between the microscope objective and the furnace window.

The tip of the filament of the lamp is set to the same brightness as the platinum strip viewed from above at the instant of melting of the metallic or other specimen on which the microscope is focussed. The eye of the observer sees the specimen, the platinum strip, and the lamp filament all in focus at once.

*Calibration of the Pyrometer.**—The most convenient method of calibration is to observe the lamp currents at the known melting-points of two or more pure substances, such as gold, nickel, and palladium, and from the equation expressing the relation between temperature and current (in lamp), the temperature of melting of any specimen may be computed. For moderate temperature intervals the equation $\log c = a + b \log T$ may be used, where c is the current, T the absolute temperature, b a constant very nearly unity.

The melting-points of nickel and palladium were taken for calibration purposes.

The accuracy of the equation was checked by extrapolating to the melting-point of platinum, which could be directly observed by matching the lamp and strip at the instant the latter burnt out. The value 1,755° C. $\pm$ 5 was obtained from six observations.

An atmosphere of pure hydrogen was maintained in the enclosure, to prevent oxidation of the metal under test.

For those metals for which the melting is sharp, such as nickel, cobalt, and iron, a precision of 1° to 2° was possible with only a few thousandths of a milligram of material.

Iron (purity 99·98 per cent. Fe).—Pure electrolytic iron from three sources was tested. There appeared to be no systematic difference either among the several samples or for different-sized pieces, and the mean value 1,533° C. $\pm$ 1 was obtained for the melting-point.

The melting and freezing-points of iron, *in vacuo* and in hydrogen, were also taken in the Arsem furnace (Fig. 89). Four observations *in vacuo* gave 1,531°, 1,531°, 1,529°, 1,527° C., and two in hydrogen gave 1,523°, 1,527° C.

Cobalt (purity 99·95 per cent. Co).—Samples from three sources were tested. Mean value 1,477° C. $\pm$ 2.

Day and Sosman employed the same method for cobalt as that described for nickel.† They found the value 1,490° C. in a nitrogen atmosphere.

Burgess and Waltenburg suggest that Day and Sosman's higher value might be caused by some oxidation of the powdered cobalt.

Chromium (98 per cent. ? Cr).—Two different samples gave values varying from 1,536° C. to 1,513° C.

Manganese (97·5 ? Mn).—Melts were taken both on platinum and on nickel strips using gold (1,063° C.) and palladium as calibration points.

* Melting-point determinations made by Burgess and Waltenberg. † Page 84.

Those on nickel were generally 10° to 20° lower than on platinum, due, apparently, to evaporation of the nickel.

The mean value 1,254° C. was obtained for the impure samples of manganese available.

Vanadium (about 97·5 per cent. Va).—None of the samples investigated melted sharply, the substance being quite viscous and showing evidences of incipient melting many degrees below the temperature at which the melting was complete. In some samples evidence of melting was apparent as low as 1,500° C., and melting was complete at about 1,720° C.

The authors estimate the melting-point of pure vanadium to lie about 1,720° C.

Titanium.—The melting-points were taken on an iridium strip. Some samples of colloid titanium melted at 1,450° to 1,500° C.; other samples showed no signs of melting when tested on a platinum strip.

Two samples from different sources gave the values 1,787° C. and 1,800° C., the melting-points being fairly sharp.

TABLE XXXIX.—Melting-points of Elements of Atomic Weight 48 to 59 (*Burgess* and *Waltenberg*).

Metal.	Melting-point, °C.	Purity.	Probable melting-point of pure element, °C.
Nickel,	1,452 * / 1,449 †	$99{\cdot}83_5$	$1{,}452 \pm 3$
Cobalt,	$1{,}477 \pm 2$ / $1{,}478 \pm 1$ ‡	$99{\cdot}95_1$	$1{,}478 \pm 5$
Iron,	$1{,}533 \pm 1$ / 1,528 §	$99{\cdot}98 \pm 0{\cdot}01$	$1{,}530 \pm 5$
Manganese,	1,255	97·98	$1{,}260 \pm 20$
Chromium,	1,520	98·99	1,520 to > Fe ?
Vanadium,	1,720	97·98	$1{,}720 \pm 30$
Titanium,	$1{,}794 \pm 12$	99·9 +	$1{,}795 \pm 15$

Melting-points of the Metals of the Platinum Group.—(*a*) *Platinum.*—The determination of the melting-point of this metal has been the object of numerous investigations. The favourite procedure has been to determine the relationship between the E.M.F. and the temperature of a thermo-element of which platinum was one component, and then obtain the value of the melting-point by extrapolation of this formula.

It is, for example, a comparatively simple matter to determine the E.M.F. at the instant when the circuit breaks for a couple of platinum *v.* platinum 10 per cent. rhodium.

The uncertainty arises in the extrapolation of the formula over large

* Assumed value on platinum strip; also observed value on iridium strip.
† Crucible melts in electric furnace.
‡ Crucible melts in electric furnace; also on iridium strip.
§ Five samples agreeing to within 3°.

intervals of temperature, and the values for the melting-point obtained by various observers differ by as much as 145° C.

When the gas thermometer scale was carried to 1,550° C. by Day and Sosman and the E.M.F. temperature relationship of couples was determined with considerable accuracy in terms of it, the extrapolation over the 200° C. to the platinum melting-point could be made with greater confidence than had previously been the case.

The method employed by Day and Sosman was to heat up the thermo-element slowly until the platinum arm melted. The couple was enclosed within a glazed Marquardt porcelain tube inserted into a carbon tube furnace. A stream of carbon monoxide around the outside of the porcelain tube protected the furnace from oxidation, while a current of dry air through the inside prevented contamination of the wires by reducing gases.

Both wires were enclosed in capillaries, leaving about 2 mms. exposed near the junction. It was this projecting portion that melted, the point being marked by a halt of about one minute in the gradual rise in temperature of the thermoelement (measured by the E.M.F. generated). This halt preceded the formation of a globule and the interruption of the circuit.

The mean value 1,752° C. was obtained for the melting-point.

Another method for the determination of the melting-point of platinum is to measure the temperature interval between the melting-points of palladium and platinum by means of optical pyrometers calibrated on the basis of Wien's law.

Several observers have employed this method with various forms of experimental arrangements.

The values obtained for the interval are in close agreement. Nernst and Wartenberg gave the value 204° C.; Holborn and Valentiner, 207° C.; Waidner and Burgess, 207° C. Hence the probable mean is 206° C. Accepting the value 1,553° C. for the palladium point, we obtain the value 1,759° C. for platinum, with a probable error of $\pm$ 5° C.

It will be observed that this figure is in fair agreement with the one obtained by extrapolation of the E.M.F. temperature relationship by Day and Sosman.

(*b*) *Rhodium and Iridium.*—The other metals of the group have not received the careful study given to platinum. Some experiments have been made by Mendenhall and Ingersoll, in which a Nernst glower was ingeniously used as the source of high temperature heat supply.

The apparatus employed is shown diagrammatically in Fig. 93. The metal to be investigated was in the form of a minute globule and placed on the glower, whose temperature could be varied by controlling the current through it. The globule was observed by means of a microscope,. By careful manipulation of the current through the glower it was possible to maintain one part melted and the other part solid in the case of the metals gold and platinum.

The apparent temperature of the glower was obtained by focussing an

image across the slit of a Martens-König spectrophotometer, the image being more than sufficient to fill the aperture.

The radiation from a Nernst glower departs considerably from that corresponding to a "full radiator," consequently Wien's law is not applicable. The authors based the extrapolation of the temperature scale on an empirical equation of the same form as Wien's, namely :—

$$E_{(\lambda T)} = c_1 \lambda^{-\alpha} e^{-\frac{c_2}{\lambda T}}$$

where $E_{(\lambda T)}$ is the energy of wave-length λ at temperature T.

Taking logarithms,

$$\log E_{(\lambda T)} = \log c_1 - \alpha \log \lambda - \frac{c_2}{\lambda T} \log e$$

Now c_1 has been found by experiment for the radiating surfaces hitherto studied to lie between 500,000 and 2,000,000. Hence, for wave-lengths near unity (1μ), the term $\alpha \log \lambda$ in the above equation is small compared with $\log c_1$, so that any variation with temperature in the value of α (which

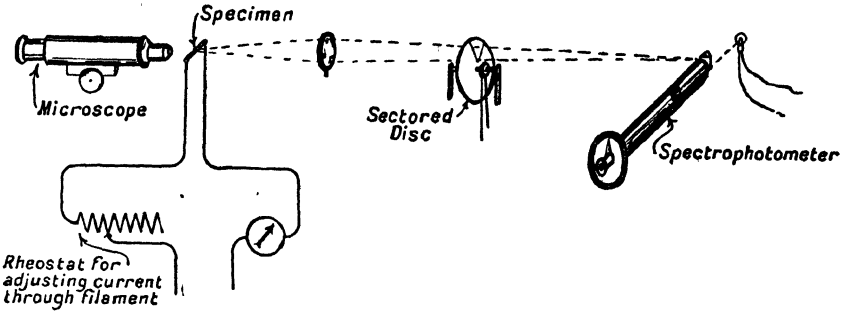


FIG. 93.—Diagram of apparatus employed by Mendenhall and Ingersoll in their use of the Nernst glower for melting-point determinations.

in the case of α "full radiator" is numerically equal to 5) will not exert much influence.

Hence a relationship of the form

$$\log E_{\lambda T} = \kappa_1 + \frac{\kappa_2}{T}$$

may be taken as a basis for extrapolation as in the case of a "full radiator."

Standardisation of the Spectrophotometer.—From the above it will be observed that two calibration points are sufficient for obtaining the constants of the equation. For this purpose the melting-points of gold and platinum were selected, the standardisation being effected by melting globules of these metals on the glower in exactly the same way as that followed in the case of the samples for test. The value 1,065° was taken for the melting-point of gold, but in the case of platinum at that time the two values 1,745° and 1,789° had been put forward without decisive proof in favour of either.

TABLE XL.

Substance.	Melting-point, °C.	Method.	Melting-point, of platinum on scale employed, °C.	Observer.
Silicon, . .	1,430			Tone.
,, . .	1,438±8	Optical	1,755	M. and I.*
Palladium, . .	1,541	Wanner pyrometer	1,745	Nernst and Wartenburg.
,, . .	1,582	Thermoelectric	1,789	Holborn and Valentiner.
,, . .	1,554±5	Optical	1,755	M. and I.
,, . .	1,549	Thermoelectric	1,755	Day and Sosman.
Rhodium, . .	1,921±5	Optical	1,755	M. and I.
Iridium, . .	1,950			Violle, 1,879°.
,, . .	2,200–2,300			Weyde, 1,879°.
,, . .	2,314±10		1,755	M. and I.
Temperature † of glower at normal brilliancy, ° C.	1,900–2,200	Maximum energy curve	1,745	Lummer and Pringsheim.
,, ,,	2,100	Efficiency	1,745	Ingersoll.
,, ,,	1,530	Thermoelectric		Hartman.
,, ,,	2,100	Optical	1,755	M. and I.
MgO, . . .	1,910	Wanner pyrometer		Goodwin and Mailey.
,, . . .	1,980–2,020	Optical	1,745	M. and I.
Melting-point of glower material, ° C.	2,380	,,	1,745	,,

* Mendenhall and Ingersoll.

† **On the temperature of normal brilliancy of the glower.**—The temperature of a 0·8 amp. 110 volt glower 1·04 mms. diam. was found to be 2,100° C., while that of one 1·30 mms. diam. was about 200° lower.

Lummer and Pringsheim's value was obtained from measurement of the wave-length of maximum energy and applying Wien's law, making the assumption that the radiating properties of the glower material were intermediate between those of platinum and a "full radiator."

Ingersoll assumed it to be a "full radiator."

Hartmann used thermocouples of wires of various sizes and extrapolated. Mendenhall and Ingersoll showed that Hartmann's value was too low, by placing small bits of platinum wire on the glower and noting that it melted at temperatures far below normal brilliancy, hence the temperature of normal brilliancy must be higher than 1,755°.

It was observed that it was not possible to melt platinum in the form of fine wire or strip hung over the glower. Hence the probable explanation of Hartman's result is that area of the glower in contact with the platinum wire was maintained at a lower temperature by the conduction of heat along the wire.

This method of employing progressively thinner wires and extrapolating the results to obtain the temperature of flames, etc., is one liable to serious errors. For example, the value 1,675° C. has been given as the temperature of a candle flame, yet it is possible to melt very fine strip platinum in almost any part of the flame. This, however, cannot be regarded as decisive proof that the temperature of the flame exceeds the melting-point of platinum, since the reducing gases present may deteriorate the platinum and affect its melting-point.

Change of Radiating Power of the Metals at the Melting-point.—Mendenhall and Ingersoll state that gold shows a marked increase of radiating power on melting, while palladium, platinum, rhodium, and iridium exhibit a similar effect, but to a smaller extent.

Silicon shows a very marked decrease of radiating power on melting.

With rhodium a change occurs at about 1,100° C., which exhibits a decided increase of radiating power as the temperature falls; a slight rise in temperature is sufficient to reverse the effect.

As previously shown the value 1,759° is the probable one, and the data given by Mendenhall and Ingersoll have been interpolated to refer to this value in Table XL.

As a check point on the line between the melting-points of gold and platinum the melting-points of palladium was determined and found to be 1,555° C., which is in good agreement with the accepted value.

A further indirect check on the work was obtained by the use of two different wave-lengths, and it was found that the melting-points agreed to within 10°.

Generally the wave-length 0·606 μ was adopted for the observations.

An experimental detail which required careful attention was the thermal contact between the globule and the filament. It was observed that the first melts were not so reliable as subsequent ones when the globules had effected good contact. Errors amounting to 100° to 200° were possible from this cause. The effect was studied by taking globules of varying size until ultimately the melting-point was found to be independent of the diameter. The limiting value of the diameter was of the order of 0·05 mm. In cases where it was not possible to maintain the globule partly molten and partly solid the melting-point and not the solidifying-point was accepted owing to the considerable super-cooling which occurred.

The method, of course, is only applicable to metals which draw into clear metallic beads and which give consistent readings for successive melts: oxidisable metals cannot be studied under the same conditions.

The most serious criticism of the work is that no attempt was made to ascertain the purity of the metals used.

The iridium, it is stated, might possibly contain traces of ruthenium.

Their value for MgO differs considerably from that given by Kanolt (2,800°).

The Melting-points of Tungsten and Tantalum.—The extensive use of these metals in incandescent lamp filament manufacture, furnace windings, etc., has naturally resulted in attention being directed to their melting-points.

Many of the published values are based on extrapolations which have no theoretical foundation, and consequently such values have to be regarded as being more or less in the nature of estimates.

Pirani determined the relationship between true temperature, apparent temperature, and electrical energy supply in the case of tungsten and tantalum wires heated up to 1700° C.

The true temperature was obtained by means of a thermocouple inserted between twisted filaments, while the apparent "black body" temperature was determined by sighting a Wanner optical pyrometer on the same filaments.

From the observations he found that the energy varied as the mth power of the absolute temperature,

$$i.e., \quad W = e\,i = A\,T^m$$

where e is the applied voltage,

i is the current,

T the absolute temperature,

$$\text{so that } \log e\,i = A' + m \log T.$$

This linear relationship between log E and log T was found to hold over a range of 500° C.

To obtain the melting-point it was necessary to extrapolate over 1,300° C. The values obtained were

3,250° C. for tungsten and
3,000° C. for tantalum.

It is doubtful whether a thermocouple as disposed in these experiments would give the true temperatures. Further, m decreases slightly with the temperature.

To allow for these errors Pirani applied a correction of the order of 200° C. to the above results.

Wartenberg used tungsten as the anode, and with the discharge from a Wehnelt cathode raised it by bombardment to the melting-point. He measured both the apparent temperature and the reflecting power of the surface.

If A is the absorbing and R the reflecting power, then

$$A = 1 - R.$$

So that if S is the apparent temperature and T the true temperature, then by Wien's law—

$$\frac{1}{S} - \frac{1}{T} = \frac{c_2}{\lambda} \log \frac{A}{\log e}$$

where λ is the wave-length of the radiation transmitted by the optical pyrometer, and c_2 the constant in Wien's equation.

The method was tested by him in the case of several metals up to a temperature of 2,400° C.

The value obtained for the melting-point of tungsten was 2,930° C.

Ruff attempted a direct determination of the melting-point of tungsten, employing a carbon tube furnace mounted *in vacuo*.

The tube had a longitudinal slit to permit of observations on the metal in the interior under approximate " black body " conditions.

The tungsten was in the form of a cone, and the value 2,650° C. was obtained for its melting-point.

A determination by a similar method by Forsythe gave the value 2,974° C. for the melting-point.

There is but little doubt that these figures are in error owing to the fact that tungsten is attacked by carbon at high temperatures.

Tantalum could not be studied in the carbon tube furnace owing to

its reaction with the incandescent carbon, and the specimens tried had the appearance of cinder when taken out of the furnace.

Both Mendenhall and Worthing have devised methods whereby "black body" conditions are obtained and the incandescent metal is not in contact with any substance which reacts chemically with it.

Worthing's Determination of the Tungsten Melting-point.—He employed a hollow, cylindrical tungsten filament perforated with small holes. This was mounted in a large lamp bulb.

Determinations of the brightness were made by sighting on a hole and on the adjacent surface. The ratio of the latter brightness to the former when corrected for (1) the difference in temperature between the interior and the surface; (2) for the departure from "full radiation" of that from the interior due to the presence of the hole; (3) for the lack of symmetry in the temperature distribution over the filament, gives the emissive power for the metal at that temperature.

A linear relation was obtained between the emissive power and the true temperature over the range 900° to 2,900° C.; the values at these two temperatures being 0·467 and 0·406 respectively for $\lambda = 0{\cdot}666\,\mu$. The corresponding corrections to convert apparent to true temperatures are 33° and 375° C.

Assuming that the linear relationship between emissive power and temperature for solid tungsten continues to hold up to the melting-point this occurs at 3,360° C.

The apparent temperature (for red radiation) of the melting-point is 2,870° C., and the emissivity 0·390. The values are stated to be of a preliminary nature only.

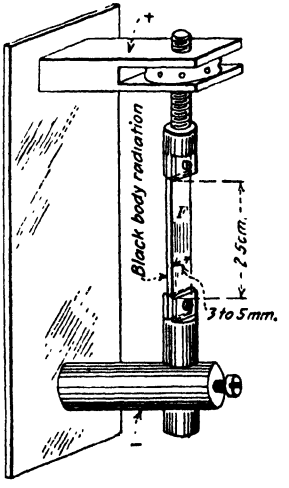


FIG. 94.—Wedge opening used by Mendenhall for true-temperature measurements.

Mendenhall and Forsythe's Determination of the Melting-points of Tungsten, Tantalum, and Molybdenum.—Mendenhall's method of obtaining "black body" conditions is to fold on itself a sheet of the metal and observe the radiation emitted from the narrow wedge opening.

The arrangement of the apparatus is shown in Fig. 94, where F is a flat conducting ribbon, heated by a longitudinal electric current, as shown, and folded on a line parallel to the length so that the resulting cross-section perpendicular to the current flow is a very narrow V—say with about 10° angular opening. If the ribbon is of uniform thickness and width, it will be raised to a uniform temperature by a given current, except near the ends. The inside of the V might be then expected to be in close approximation to a black body since it has but a small opening and uniformly heated walls; and if this were so, observations on it with an optical pyrometer would give

the true temperature of the inside walls. The outside of the ∨ will give radiation characteristics of the material of the ribbon.

The questions arise :

(1) How closely does the radiation from the inside of the ∨ approximate to that of a black body at the temperature of the inside walls ?

(2) How much real temperature difference is there between the inside and outside surfaces of the wall of the ∨ ?

The first of these two questions is answered by considering the building up of radiation within the ∨ opening by multiple reflection. In Fig. 95 a ∨ opening is formed by bending a specular reflecting sheet. Points A, B, C, D, E, and F are points of reflections for a ray which may be imagined as entering at P. If the material of the ∨ is radiating, in consequence of its temperature, for any range of wave-lengths, the brightness of the point F, as viewed from Q, may be considered as made up of various components : first, that due to the natural radiation from F ; second, that due to the natural radiation from E reflected at F ; third, that due to the natural radiation from D which is twice reflected at E and at F, etc. Limiting ourselves to a small wave-length interval, remembering according to Kirchhoff's law that the reflection factor r is equal to $1 - e$, and representing

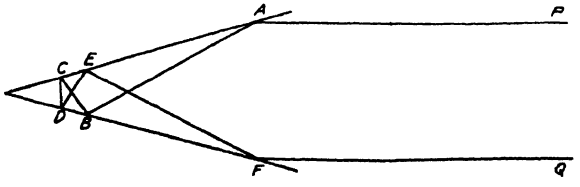


FIG. 95.—Diagram showing how radiation issuing from a narrow V builds up towards black-body radiation.

by b' the spectral brightness of a black body at the temperature of the material of the ∨, and by b'' the corresponding spectral brightness of the point F as viewed from Q, we have

$$b'' = e\,b' + r\,e\,b' + r^2 e\,b' + \ . \ . \ . \ r^n e\,b'$$
$$= e\,b^1\,(1 - r^n).$$

With a ∨ opening of 10°, as suggested by Mendenhall, n will be equal to 18. Thus with r equal to 0·7 (which is roughly the value for the material used originally by Mendenhall) b''/b is found to be 99·8 per cent.—that is, the radiation from the ∨ cavity may be said to be 99·8 per cent. black, a satisfactory approach to black-body radiation.

The second question relating to the temperature difference between the inside and the outside of the ∨ opening was settled by computing the difference in temperature from the known dimensions, the electrical input, and the thermal conductivity of the material. For the platinum wedges used, Mendenhall found a difference of the order of a few tenths of a degree. His results on platinum agreed quite well with the previously mentioned results by Holborn and Kurlbaum and by Waidner and Burgess. In

applying the $\vee$ method to tungsten, there is a difficulty in constructing a suitable $\vee$, so Mendenhall and Forsythe employed two separate sheets arranged to form a $\vee$. There was, however, a tendency for the two sheets to separate and leave a gap between the parts.

In a paper entitled "The True Temperature Scale of Tungsten and its Emissive Powers at Incandescent Temperatures," *Phys. Rev.*, p. 377, 1917, Mendenhall and Forsythe have summarised previous work on the subject.

The table below gives a series of values for the apparent temperature S, the emissivity E for wave-length $\lambda = 0{\cdot}665\ \mu$, and the difference between true temperature (T) and apparent temperature (S).

TABLE XLI.—TEMPERATURE RELATION OF TUNGSTEN ON BASIS OF $c_2 = 14{,}350\ \mu$ AND THE MELTING-POINT OF GOLD = 1,336° K.

Apparent temp. S. $\lambda = 665$.	Emissivity E.	Difference T-S.	ΔT in case $\frac{\Delta e}{e} = +{\cdot}01$.
1,200	·457	56	−·7
1,400	·451	76	1·0
1,600	·446	102	1·3
1,800	·440	132	1·7
2,000	·434	168	2·2
2,200	·428	208	2·7
2,400	·422	254	3·3
2,600	·416	306	3·9
2,800	·410	366	4·6
3,000	·403	433	5.4
3,176 m.p.	·398	498	6·2

The Melting-point of Tungsten according to Various Observers.*

	Apparent temperature for $\lambda = 0{\cdot}665$.
Mendenhall and Forsythe,	3,174° K.
Langmuir,	3,187
Worthing,	3,174
Luckey,	3,169
Average,	3,176° K.
Hence true temperature,	3,675° K. = 3,402° C.

TABLE XLII.—MELTING-POINT OF TANTALUM.

Observer.	Date.	Method.	Value, °C.
Waidner and Burgess,	1907	Extrapolation	2,900
Pirani,	1910	„	3,000
„	1911	Apparent temperature and reflecting power	2,700 †
Forsythe,	1911	Wedge method	2,800

* Forsythe and Worthing, 1924, give the melting point of tungsten as 3,655° K.

† Corrected to palladium 1,549° instead of 1,575° C., and $c_2 = 14{,}500$ instead of 14,200.

The Temperature of the Electric Arc.—The temperature of the positive crater of the electric arc represents the highest terrestrial temperature, and the estimation of its value has been a frequent subject for investigation.

The theory of the mechanism of the arc which has received the greatest support up to the present is that the arc is produced by carbon vapour volatilised from the electrodes, which are supposed to be in a state of incipient fusion, the surface being covered by a layer of viscous carbon from which the vapour boils.

Variations in Temperature of the Arc with Change in the External Conditions.—I. Influence of Current Density.—As far back as 1878 it was observed by Rossetti that the brightness of the arc did not depend on the value of the current. Since the brightness is a function of the temperature it would follow from this observation that the temperature would be independent of the current.

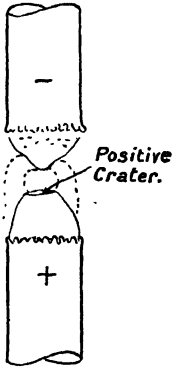


FIG. 96.

Violle varied the current from 10 to 400 amperes, and found that the brightness of the positive crater was independent of the power expended in the arc. In these experiments a larger-sized electrode was used for the higher energies, and consequently the experiments of Violle do not necessarily prove that for a given size of electrode the temperature is constant.

Wilson and Gray, Wanner, and Waidner and Burgess made further investigations of the same point.

Wilson and Gray and Wanner conclude from their observations that doubling the current through the arc had no influence on the temperature. It should be remarked, however, that their measurements were not particularly concordant, and errors of the order for 100° C. were possible.

Waidner and Burgess found that the temperature was a function of the current when the potential difference was constant and the arc was burning normally.

The change is comparatively small, since doubling the current caused an increase of 70° only, from 3,420° to 3,490° C.

The observations were made with a disappearing filament type of optical pyrometer, which had the advantage of only requiring a small area to sight on, and consequently the wandering of the brightest spot of the crater could easily be followed.

Reich using a pyrometer of the polarising type found the value 3,430° C. for the temperature of the positive crater, and 2,870° C. for the cathode, the temperature of both poles being independent of current when this was varied from 3 to 12 amps. He believed that the change observed by Waidner and Burgess might have been due to the increased brilliancy of the gases in the arc with larger currents.

Lummer, in 1913, described experiments in which the current was varied

from 10 to 68 amperes, and the length from 1 mm. to 18 mms. without apparent effect on the temperature.

The explanation of these effects is not difficult, since increase in current merely involves a larger area covered by the arc, while the small increase of temperature observed by Waidner and Burgess may be caused by superheating of the viscous layer—the vapour still maintaining the temperature of the normal boiling-point—or to the fact that with the smaller current the area heated is reduced, and consequently there is a greater tendency to cool the crater by thermal conduction to the colder parts of the carbon.

II. Influence of Pressure.—If the theory advanced is correct, that the arc temperature corresponds to the boiling-point or the sublimation temperature of carbon, we should expect the temperature to depend upon the pressure of the atmosphere surrounding the arc. Thus the temperature would be raised when the pressure is raised, and lowered if the pressure is lowered, assuming, of course, that carbon obeys the laws found to hold for other substances.

Lummer's experiments show that this is the case. At 0·1 atmosphere pressure the temperature is 3,670°C., at 1 atmosphere 3,930° C., and at 22 atmospheres 5,730° C.

III. Influence of Impurities.—Wanner observed that cored* carbon gave an arc temperature about 170° C. lower than that of retort carbon.

Waidner and Burgess found that homogeneous carbons prepared for optical projection purposes gave temperatures of the order of 40° below those obtained with very pure graphite. The difference would probably be still greater for the commercial carbons which contain salts.

Determinations of the Temperature of the Positive Crater under Normal Conditions.—Determinations of the temperature of the arc afford a severe test of the validity of the various laws of radiation, owing to the wide ranges of temperature which have to be covered by extrapolation.

It is generally assumed that carbon radiates as a "full radiator," and this assumption is probably not wide of the mark; in any case the temperature obtained would represent the lower limit if carbon radiates as a "grey body." †

(*a*) **Estimations based on Wien's Law.**—Wanner in 1900 calibrated an optical pyrometer of his design (Chap. VII.) under "full radiator" conditions up to 1,100° C., and verified the linearity of the relationship between $\log \tan\varphi$ and $\frac{1}{T}$.

He then determined the temperature of the hottest portion of the positive crater, using red ($\lambda = 0{\cdot}6563\ \mu$) and green ($\lambda = 0{\cdot}5461\ \mu$) radiation.

* The material generally employed for coring is very finely ground carbon, of approximately the same composition as the carbon rod itself, mixed to a paste with a solution of potassium silicate. The composition and the percentage of the silicate used influence considerably the length of the arc.

† One with a constant coefficient of emissivity over the entire spectrum range.

The results obtained with two different grades of carbon are shown below :—

	Cored carbons, °C.	Retort carbons, °C.
Red light, . . .	3,450	3,600
Green light, . . .	3,430	3,620

Féry employed a Le Chatelier form of optical pyrometer and obtained the value 3,870° C. with red light and 3,900° C. with green light. These values appear to be abnormally high ; this may be due to the fact that the red glass screen transmitted a wide band and at high temperatures the short wave-lengths would have a disturbing effect on the extrapolation of the low temperature calibration curve.

Waidner and Burgess determined the arc temperature with three different types of optical pyrometers with the results given below.

Pyrometer.	Temperature, °C.
Holborn-Kurlbaum,* . .	3,420
Le Chatelier, . . .	3,450
Wanner,†	3,410

The determinations above described, with instruments whose calibrations are based on Wien's law, are probably the ones upon which reliance should be placed.

(*b*) **Estimations based on the Fourth-power Law of Radiation.**—Féry employed one of his early types of total radiation pyrometers in the determination of the temperature of the positive crater.

In this method the image of the crater was focussed by means of the fluorite objective of the telescope on to an iron constantan thermo-junction.

The instrument was calibrated up to 1,500° C. on a " full radiator " and its indications shown to comply with the fourth-power law.

The value 3,490° C. was obtained for the temperature of the positive crater.

(*c*) **Estimations based on the Displacement Law $\lambda_m T$ = Constant.**—This law which connects the wave-length of maximum energy with the temperature has a sound theoretical foundation, but is difficult of practical application, owing to the fact that the energy curve does not possess a well-defined maximum.

Lummer and Pringsheim in 1901 utilised this law to estimate the limiting temperatures of a number of light sources. The value of the constant for a " full radiator " was found to be 2,940.

* Disappearing filament type. † Polarising type.

Hence as a maximum estimate of the temperature of the positive crater we have

$$T_{max.} = \frac{2,940}{0{\cdot}7} = 4,200° \text{ C. abs.}$$

It is probable that carbon approaches but is not a "full radiator"; the other extreme is represented by platinum, for which the constant is 2,630.

Hence $$T_{min.} = \frac{2,630}{0{\cdot}7} = 3,750° \text{ C. abs.}$$

Later determinations of the ordinate of maximum energy by Abney and Festing and by Very have given the value 0·73 μ for λ_m.

Hence the limits become

$$T_{max.} = 4,025° \text{ C. abs.} \equiv 3,750° \text{ C.}$$
$$T_{min.} = 3,600° \text{ C. abs.} \equiv 3,330° \text{ C.}$$

(*d*) **Estimations based on Various Empirical Methods of Extrapolating the Temperature Scale.**—Le Chatelier (1892) determined the relationship between the intensity of red light and temperature over the range 700° to 1,800° C., using his optical pyrometer for the purpose.

He deduced the relationship

$$I = 10^{6{\cdot}7}\, T^{-\frac{3210}{T}}$$

Extrapolating this equation to obtain the arc temperature he found the value 4,130° C.; a result which is probably too high.

Violle (1893 and 1895) described an ingenious method based on the extrapolation of the specific heat-temperature line for carbon.

In this method a small button of carbon from the end of the positive crater was dropped into a calorimeter and its total heat observed.

Assuming the validity of the linear variation of specific heat with temperature, which had been experimentally verified up to a temperature of 1,000° C., he deduced the value 3,600° for the temperature of the arc.

Wilson and Gray employed a differential method in which the radiation from the positive crater was balanced against that from a platinum surface at a known temperature.

The radiation was received on the thermojunction of a radio-micrometer.

The relation between the radiation from polished platinum and platinum covered with copper oxide was ascertained, and it was then assumed that carbon obeyed the same law as that found for copper oxide.

From the ratio of the projected areas emitting radiation the temperature of the radiator could be calculated.

For the arc temperature the value 3,330° C. was obtained.

It might be remarked that their scale of temperature was in error, according to present standards, by about 20° at the melting-point of gold.

Petavel, in his study of the luminous emission from the incandescent

platinum, obtained the following relationship between temperature and intrinsic brilliancy :—

$$(t - 400) = 889{\cdot}6 \sqrt[6{\cdot}9]{b}$$

where t is temperature in ° C., b the intrinsic brilliancy per sq. cm.

In the case of the positive crater he found for b the value 11,000 candles per cm.^{2} Hence $t = 3{,}830°$ C., assuming that carbon obeyed the same law as platinum.

Summarising the results we have the following series of values for the temperature of the crater :—

TABLE XLIII.

Observer.	Date.	Temperature, °C.	Method.
Le Chatelier, . . .	1892	4,100	Intensity red light.
Violle, ...	1893	3,600	Specific heat carbon.
Wilson and Grey, . .	1895	3,330	Total radiation.
Petavel, ...	1898	3,830	Luminosity.
Wanner, ...	1900	3,430-3,630	Wien's law. Different carbons.
Lummer and Pringsheim, .	1901	3,480-3,930	$\lambda_m T = C$.
Very, ...	1899	3,330-3,730	$\lambda_m T = C$.
Féry, ...	1902	3,490	Fourth-power law.
,, ...		3,880	Wien's law.
Waidner and Burgess, .	1904	3,400-3,450	Wien's law.
Reich, ...	1906	3,430	Wien's law.

Boiling-points of the Metals.—With a few exceptions metals boil at an extremely high temperature, and in most cases vigorous sublimation occurs at temperatures below the boiling-point which renders observations of the transition points very indefinite.

Experiments on the boiling-points of metals have been described by Féry, Wartenberg, and Greenwood.

Greenwood employed a carbon tube furnace with the metal contained in a crucible suspended from the top of the furnace. Temperature observations were taken with a polarising type of optical pyrometer sighted on the side of the crucible, while visual observations of the surface of the metal were made through a window closing the top of the furnace.

It was observed that the surface of the metal during the heating at first remained perfectly still, but on approaching the boiling-point a slight agitation was seen, which rapidly became vigorous. In most cases the difference between the temperatures indicated when a gentle agitation was first apparent, and when the ebullition was so vigorous that globules of metal were projected to a height of over 10 cms., did not exceed 100° C.

By accepting as the " boiling-point " that temperature at which ebullition first became decided, quite concordant results were obtained in different experiments.

Hence the " boiling-point " determined by these experiments may be defined as the temperature at which vaporisation becomes sufficiently vigorous to cause a decided projection of drops from the surface.

This definition is, however, somewhat arbitrary, since the temperature of ebullition when hydrogen was passed through the furnace was from 50° C. to 100° C. lower than when the nitrogen was used. It would seem that the dislodging of the heavy vapour above the surface of the metal, by the diffusion of hydrogen through the crucible, is apt to mask the true effect.

The non-carburisable metals were contained in graphite crucibles, while the metals which combine with carbon were contained in a carbon crucible " brasqued " with fused magnesia. Electrically shrunk magnesia was powdered and kneaded with a solution of magnesium chloride. By the use of a wooden former a uniform 2 mms. thick lining was obtained. The crucible was dried at 200° C., and then heated gradually in a carbon tube furnace to drive off the HCl which was copiously evolved during the heating.

TABLE XLIV.

I. Non-carburisable Metals.

Metal.	Boiling point, °C.	Authority.
Copper,	2,100	Féry.
,,	above 2,200	Wartenberg.
,,	2,310	Greenwood.
Tin,*	above 2,200	Wartenberg.
,,	2,275	Greenwood.
Silver,	2,070	Wartenberg.
,,	1,955	Greenwood.
Lead,	1,580	Wartenberg.
,,	1,525	Greenwood.
Bismuth,	1,550	Barns.
,,	1,420	Greenwood.
Antimony,	1,500–1,700	Biltz and Meyer.
,,	1,440	Greenwood.
Magnesium,	1,100	,, †
,,	1,120	,,

II. Carburisable Metals.

Aluminium,	1,800	Greenwood.
Manganese,	1,900	,,
Chromium,	2,200	,,
Iron,	2,450	,,

* It is interesting to note that tin remains in the molten stage over a temperature range exceeding 2,000° C.

† Thermocouple determination. Temperature remained steady while the metal distilled into the upper portion of the crucible.

The temperature was allowed to fall somewhat, and the charge of metal introduced.

Using this method the linings remained perfectly intact and coherent after heating to 1,800° C., and could be used up to 2,500° C.

At temperatures above 1,700° C. some trouble was caused by the interaction of the magnesia and the carbon, with the formation of a dark grey sublimate. This, however, was not sufficiently energetic to materially interfere with the observations of the metal surface except at the high temperatures required in the case of iron.

In the case of aluminium the ebullition occurred quite suddenly owing to the formation of an oxide film and its disruption.

With manganese and chromium no tenacious film was obtained, but failures were caused by the corrosive action of the metal on the magnesia lining.

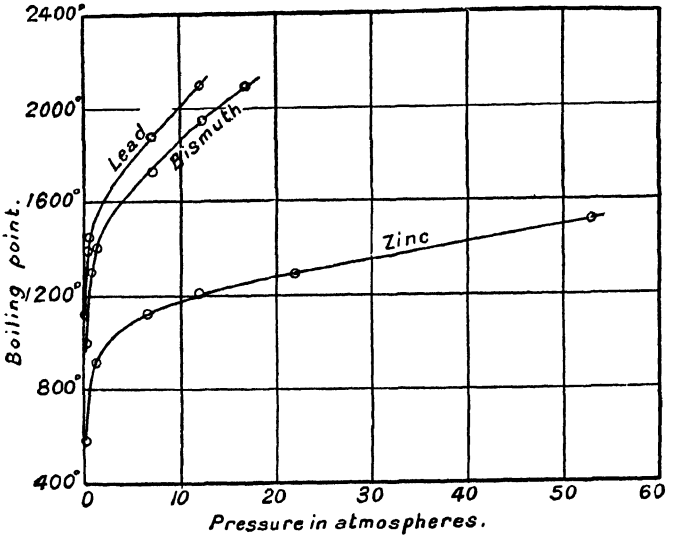


FIG. 97.—Boiling-points of the metals at different pressures.

Boiling-points at Different Pressures.—By enclosing the furnace in a steel bomb observations could be made under several atmospheres pressure.

At first considerable difficulty was caused by the convection effects in the column through which the surface was observed; this trouble was reduced by prolonging the furnace tube by a chimney up to the window.

The sharpness of the observations was not so satisfactory as at atmospheric pressure owing to the clouds of sublimed vapour obscuring the metal surface.

It was possible, however, to decide the temperature at which globules began to be thrown up.

Zinc exhibited a somewhat abnormal behaviour, the character of the distillation, particularly at the higher pressures, having more the appearance of a very rapid volatilisation than an actual ebullition.

The results are shown graphically in Fig. 97.

Furnace for High Temperature Melting-points in Air.—For the determination of the melting-points of certain substances, for example the platinum group, it is essential to employ an oxidising, or at least a neutral, atmosphere.

There is a considerable advantage in using a furnace in preference to a strip for heating purposes, particularly if it is practicable to arrange diaphragms so that approximate "black body" conditions are obtained in the interior.

The furnace described below was designed by Dr. Harker in 1905 for the determination of the melting-point of platinum by the thermoelectric method. It should, however, be possible to so modify it that melting-point determinations could be carried out under "black body" conditions, and an optical pyrometer employed for the temperature observations.

It is a well-known fact that most oxides, when heated to redness, conduct electricity fairly well, and this phenomenon has found practical application in the Nernst lamp.

The resistor element of the furnace illustrated in Fig. 98 is a tube of "rare earths" of a composition which has a high specific electrical conductivity.

The preliminary heating of the material to the temperature (1,000° C.) at which it has a reasonably low resistance, is effected by a nickel wound tube which encloses the resistor element, but is separated from it by a layer of powdered zirconia.

The resistor tube A is about 10 mms. internal diameter by 70 mms. long. It is made of a mixture of zirconia (ZrO_2) and 10 per cent. yttria and erbia mixture bound with about 5 per cent. of gum tragacanth. The mixture is moulded and baked at a high temperature. This causes a shrinkage of about 40 per cent. in the volume; consequently the admixture of a considerable proportion of hard burnt material is advisable to reduce the shrinkage.*

The current is led in by platinum flexibles autogenously welded to thick leads of platinum or nickel. The tube is sunk below the level of the surrounding furnace to permit of the upper electrode being heated to the temperature necessary for obtaining good electrical conductivity in the material. The tube B is of hard porcelain of 30 to 40 mms. inside diameter and wound with nickel wire.

To start up the furnace, about 200 watts are supplied to the nickel spiral—for half an hour or so—until the interior is red hot. The zirconia tube, with a resistance in series, is then switched on to a 200 to 500 volt circuit.

To maintain the tube at about 2,000° C. a current of the order of 2 amps.

* In the manufacture of refractory bricks it is the standard practice to add a certain amount of "grog," or hard burnt material, to reduce shrinkage.

is required, with a fall of potential of 60 to 80 volts between the electrodes. Temperatures much in excess of 2,000° C. cannot be obtained, since the material softens about this temperature.

All solid electrolytic conductors have a negative temperature coefficient of resistance, hence a very large ballast resistance is necessary in series with the tube, and normally a voltage drop of 20 to 25 per cent. occurs in this resistance.

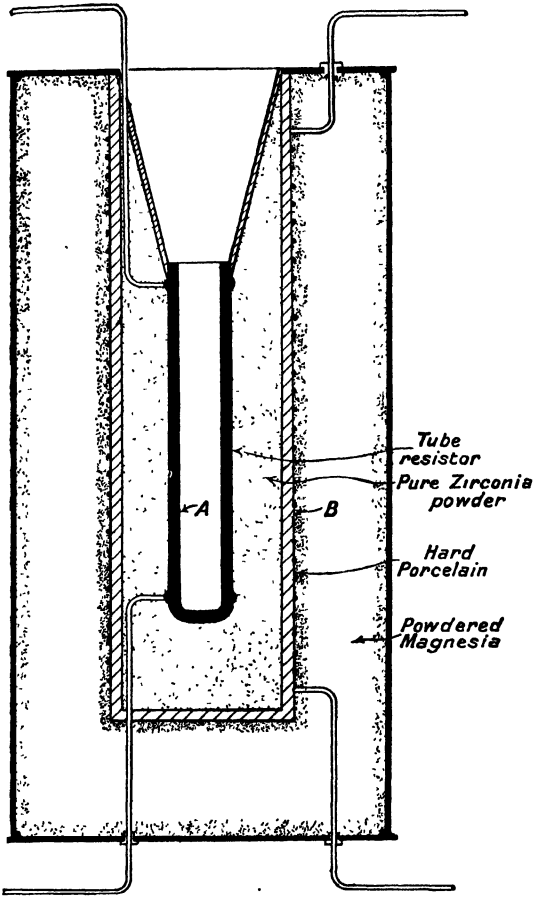


FIG. 98.—Illustration of a furnace for high temperature melting-points in air.

A furnace of the dimensions given above requires—for maintaining a steady temperature of about 1,700° C.—about 150 watts expended in the nickel winding and 140 watts in the tube itself.

The resistance of the tube when at room temperature is of the order of 1,000 megohms, but from 400° C. upwards decreases with great rapidity.

The practical difficulty with this type of furnace is the electrodes, the

temperature of which must not rise beyond the melting-point of platinum, and with the large sizes this point is a particularly troublesome one. In such cases it is advisable to construct the resistor in the form of a reel, the electrode wires being wound around the wider parts at the ends, and thus kept relatively cool by conduction losses.

It should be remarked that furnaces of this type cannot be operated at low temperatures, since the current tends to flow along a hot streak and not distribute itself uniformly over the cross-section of the tube. This effect is observed when the furnace has been operated at higher temperatures and then the energy supply is gradually cut down. It is, of course, due to the instability caused by the negative temperature coefficient of resistance.

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APPENDIX I.

Specifications of Sulphur Boiling-point Apparatus.—The following specifications proposed by Mueller and Burgess as the result of their experiments are primarily directed to be of assistance in obtaining standard practice in resistance thermometer calibration :—

" 1. *Boiling Apparatus.*—The boiling tube is of glass, fused silica, or similar material, and has an internal diameter of not less than 4 nor more than 6 cms. The length must be such that the length of the vapour column, measured from the surface of the liquid sulphur to the level of the top of the insulating material surrounding the tube, shall exceed the length of the thermometer coil by at least 20 cms.* Heating is by any suitable heater at the bottom of the tube, and the arrangement must be such that the heating element, and all conducting material in contact with it, terminate at least 4 cms. below the level of the liquid sulphur. If a flame is allowed to impinge directly on the tube the heat insulation must extend at least 4 cms. below the level of the liquid sulphur. There should be a ring of insulating material above the heater, fitting the tube closely, to prevent superheating of the vapour by convection currents outside the tube. Above the heater the tube is surrounded with insulating material, not necessarily in contact with it, and of such character as to provide heat insulation equivalent to a thickness of not less than 1 cm. of asbestos. The length of this insulated part has already been specified. Any device used to close the top of the boiling tube must allow a free opening for equalisation of pressure.

" 2. *Purity of Sulphur.*—The sulphur should contain not over 0·02 per cent. of impurities. It should be tested to determine whether selenium is present.

" 3. *Radiation Shield.*—The radiation shield consists of a cylinder open at both ends, and provided with a conical umbrella above. The cylindrical part is to be 1·5 to 2·5 cms. larger in diameter than the protecting tube of the thermometer, and at least 1 cm. smaller than the inside diameter of the boiling tube. The cylinder should extend 1·5 cm. or more beyond the coil at each end. The umbrella should fit the thermometer tube closely, should overhang the cylinder, and be separated from the latter by a space 0·5 to 1·0 cm. high. The inner surface of the cylinder must be a poor reflector, such as sheet-iron, blackened aluminium, asbestos, or a deeply corrugated surface.

* This length was arrived at as follows :—The minimum distance from the liquid surface to the bottom of the shield was taken as 6 cms. ; excess length of shield over length of thermometer coil, 6 cms. : distance available for displacing thermometer, 6 cms. ; minimum distance from top of shield to level of top of insulation, 2 cms.

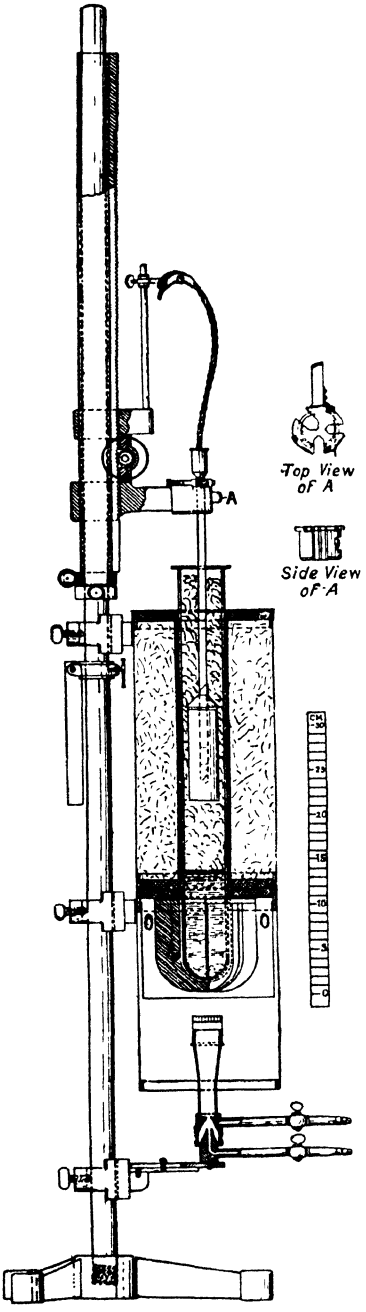


FIG. 99.—Sulphur boiling-point apparatus employed by Mueller and Burgess.

"4. *Procedure.*—The sulphur is brought to boiling,* and the heating is so regulated that the condensation line is sharply defined and is 1 cm. or more above the level of the top of the insulating material. The thermometer, enclosed in its shield, is inserted into the vapour, taking care to have the thermometer coil properly located with respect to the shield, and the thermometer and shield centred in the boiling tube. After putting the thermometer into the vapour, time must be allowed for the line of condensation again to reach its proper level. Simultaneous readings of the temperature and barometric pressure are then made. In all cases care should be taken to prove that the temperature is not affected by displacing the thermometer 2 or 3 cms. up or down from its usual position.

"5. *Computations.*—Temperatures † are calculated from the pressure by use of the formula

$$t = 444{\cdot}60^\circ + 0{\cdot}0910\,(p - 760) - 0{\cdot}000049\,(p - 760)^2.$$

If necessary, account should be taken of any difference in pressure between the levels at which the thermometer bulb and the open end of the barometer respectively are located. Pressures are to be expressed in the equivalent millimetres of mercury at 0° and under standard gravity ($g = 980{\cdot}665$)."

* If the sulphur has been allowed to solidify in the bottom of the tube, it must be melted from the top downwards, to avoid breaking the tube. A better procedure is that recommended by Rothe—namely, on completing work with the apparatus, it is turned so that the tube makes an angle of 30° or less with the horizontal, so that the sulphur on solidifying extends along the sides of the tube, in which position it may be melted down with less danger of breaking the tube. Even when the procedure recommended is followed, breakage of tubes may be reduced by carefully melting the sulphur from the top downwards over a Bunsen burner before applying heat to it in the apparatus.

† International agreement has not yet been arrived at as to the value to be ascribed to the sulphur boiling-point.

APPENDIX II.

TABLES.

TABLE XLV.—Boiling-point of Water at Different Pressures.

Pressure.	Temp. °C.	Diff. pr. 1 mm.	Pressure.	Temp. °C.	Diff. pr. 1 mm.
730	98·8802		750	99·6310	
731	·9182		751	·6681	
732	·9561		752	·7051	
733	·9939	0·0378	753	·7421	
734	99·0318		754	·7791	0·0369
735	·0695		755	·8160	
736	·1073		756	·8529	
737	·1449		757	·8897	
738	·1826		758	·9265	
739	·2202		759	·9633	
740	·2577		760	100·0000	
741	·2953		761	·0367	
742	·3327		762	·0733	
743	·3702		763	·1099	
744	·4075		764	·1465	
745	·4449	0·0373	765	·1830	0·0365
746	·4822		766	·2194	
747	·5194		767	·2559	
748	·5567		768	·2923	
749	·5938		769	·3286	
750	·6310		770	·3649	

TABLE XLVI.—Boiling-point of Sulphur at Different Pressures. Also the Corresponding Values of the Function

$$\left\{\left(\frac{t}{100}\right)^2-\left(\frac{t}{100}\right)\right\}.$$

Pressure.	Temp. °C.	$\left\{\left(\frac{t}{100}\right)^2-\left(\frac{t}{100}\right)\right\}$	Pressure.	Temp °C.	$\left\{\left(\frac{t}{100}\right)^2-\left(\frac{t}{100}\right)\right\}$
730	441·77	15·098	737	442·42	15·149
731	·86	·105	738	·52	·157
732	·96	·113	739	·61	·164
733	442·05	·120	740	·70	·171
734	·14	·127	741	·79	·178
735	·24	·135	742	·89	·186
736	·33	·142	743	·98	·193
737	·42	·149	744	443·07	·201

TABLE XLVI.—*Continued.*

Pressure.	Temp. °C.	$\{(\frac{t}{100})^2-(\frac{t}{100})\}$	Pressure.	Temp. °C.	$\{(\frac{t}{100})^2-(\frac{t}{100})\}$
744	443·07	15·201	757	444·26	15·294
745	·16	·208	758	·35	·301
746	·25	·215	759	·44	·308
747	·35	·222	760	·53	·315
748	·44	·229	761	·62	·322
749	·53	·237	762	·71	·329
750	·62	·244	763	·80	·336
751	·71	·251	764	·89	·343
752	·80	·258	765	·98	·351
753	·89	·265	766	445·07	·358
754	·98	·272	767	·16	·365
755	444·08	·280	768	·25	·372
756	·17	·287	769	·34	·379
757	·26	·294	770	·43	·386

Calculated from the formula

$$t = 444{\cdot}53 + {\cdot}0904\,(p - 760) - 0{\cdot}0000519\,(p - 760)^2.$$

TABLE XLVII.

pt. °C.	*t* °C.	Difference for 1° *pt*	*pt.* °C.	*t* °C.	Difference for 1° *pt.*
−40	−39·18	0·975	270	277·38	1·075
−30	−29·43	0·978	280	288·13	1·079
−20	−19·65	0·981	290	298·92	1·083
−10	− 9·84	0·984	300	309·75	1·086
0	0·00	0·987	310	320·61	1·090
10	9·87	0·990	320	331·51	1·095
20	19·76	0·992	330	342·45	1·098
30	29·69	0·995	340	353·44	1·102
40	39·64	0·998	350	364·46	1·106
50	49·63	1·001	360	375·52	1·110
60	59·64	1·004	370	386·62	1·114
70	69·68	1·007	380	397·76	1·118
80	79·76	1·011	390	408·95	1·123
90	89·86	1·014	400	420·18	1·127
100	100·00	1·017	410	431·45	1·132
110	110·17	1·020	420	442·76	1·136
120	120·37	1·023	430	454·13	1·140
130	130·60	1·026	440	465·53	1·144
140	140·86	1·030	450	476·97	1·149
150	151·16	1·033	460	488·46	1·154
160	161·49	1·036	470	500·00	1·158
170	191·85	1·040	480	511·58	1·163
180	182·25	1·043	490	523·21	1·168
190	192·68	1·046	500	534·89	1·173
200	203·14	1·050	510	546·62	1·178
210	213·64	1·054	520	558·40	1·182
220	224·18	1·057	530	570·22	1·188
230	234·75	1·060	540	582·10	1·193
240	245·35	1·064	550	594·03	1·198
250	255·99	1·068	560	606·00	1·203
260	266·67	1·071	570	618·03	1·208

TABLE XLVII.—*Continued.*

pt. °C.	*t* °C.	Difference for 1° *pt.*	*pt.* °C.	*t* °C.	Difference for 1° *pt.*
580	630·11	1·213	800	910·76	1·352
590	642·24	1·219	810	924·28	1·359
600	654·43	1·224	820	937·87	1·367
610	666·67	1·230	830	951·54	1·374
620	678·97	1·235	840	965·28	1·383
630	691·32	1·241	850	979·11	1·390
640	703·73	1·247	860	993·01	1·399
650	716·20	1·253	870	1,007·00	1·407
660	728·73	1·259	880	1,021·07	1·416
670	741·32	1·264	890	1,035·23	1·424
680	753·96	1·271	900	1,049·47	1·433
690	766·67	1·277	910	1,063·80	1·441
700	779·44	1·283	920	1,078·21	1·450
710	792·27	1·290	930	1,092·72	1·460
720	805·17	1·296	940	1,107·31	1·469
730	818·13	1·303	950	1,122·00	1·479
740	831·16	1·310	960	1,136·79	1·490
750	844·26	1·316	970	1,151·69	1·499
760	857·42	1·323	980	1,166·68	1·508
770	870·65	1·330	990	1,181·76	1·519
780	883·95	1·337	1,000	1,196·95	1·529
790	897·32	1·344	1,010	1,212·24	1·541

TABLE XLVIII.—To calculate the Change in t for a given Small Change in δ.

t °C	Change in t for change of + 0·01 in δ.	t °C.	Change in t for change of + 0 01 in δ.
−40	+0·0056	450	+0·1575
−20	+0·0024	500	+0·200
0	+0·0000	550	+0·247
20	−0·0016	600	+0·300
40	−0·0024	650	+0·357
60	−0·0024	700	+0·420
80	−0·0016	750	+0·487
100	−0·0000	800	0·560
120	+0·0024	850	0·637
140	+0·0056	900	0·720
160	+0·0096	950	0·807
180	+0·0144	1,000	0·900
200	+0·0200	1,050	0·997
250	+0·0375	1,100	1·100
300	+0·0600	1,150	1·207
350	+0·0875	1,200	1·320
400	+0·1200		

Tables XLVII. and XLVIII. are based on data given by Dr. J. A. Harker, *Phil. Trans. Roy. Soc.*, Vol. **203, A. 369**, p. 343 (1904).

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